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ATLAS – An Integrated Structural Analysis and Design System

System Demonstration Problems

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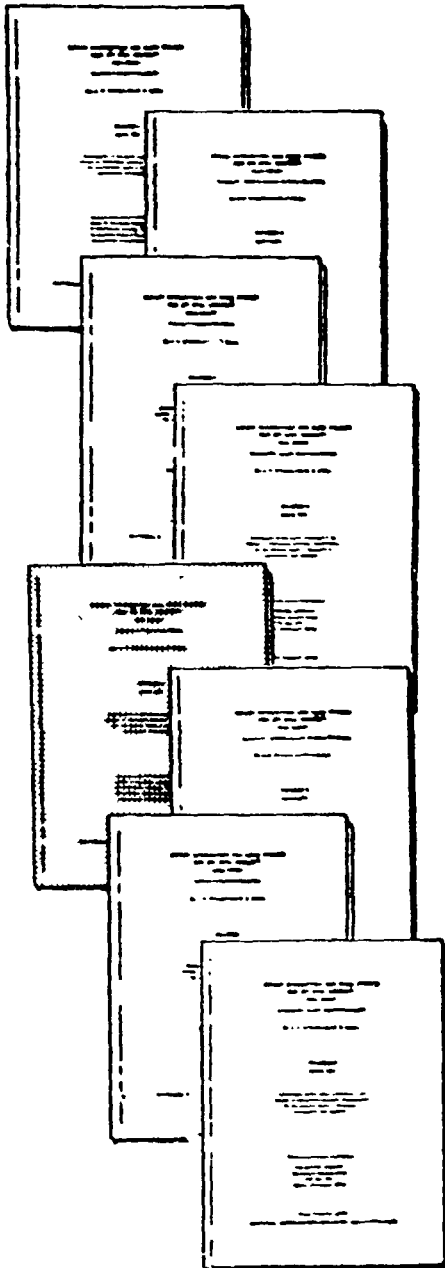
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Space Administration

1979



ATLAS SYSTEM DOCUMENTATION



VOLUME I

ATLAS User's Guide
NASA CR-159041

VOLUME II

System Design Document
NASA CR-159042

VOLUME III

User's Manual-Input and Execution Data
NASA CR-159043

VOLUME IV

Random Access File Catalog
NASA CR-159044

VOLUME V

System Demonstration Problems
NASA CR-159045

VOLUME VI

DESIGN Module Theory
NASA CR-159046

VOLUME VII

LOADS Module Theory
Boeing Commercial Airplane Company
D6-25400-0101

VOLUME VIII

SNARK User's Manual
Boeing Computer Services
BCS-G0686

FOREWORD

Development of the ATLAS integrated structural analysis and design system was initiated by The Boeing Commercial Airplane Company in 1969. Continued development efforts have resulted in the release and application of several extended versions of the system to aerospace and civilian structures. Those capabilities of the current ATLAS version developed under the NASA Langley Contract No. NAS1-12911 include the following: geometry control, thermal stress, fuel generation/management, payload management, loadability curve generation, flutter solution, residual flexibility, strength design of composites, thermal fully stressed design, and interactive graphics. The monitor of this contract was G. L. Giles. The inertia loading capability was developed under the Army Contract No. DAAG46-75-C-0072.

This document is one volume of a series of documents describing the ATLAS System. The remaining documents present details regarding the input data and program execution, data management, system design, and the engineering method used by the computational modules.

The key responsibilities for development of ATLAS have been within the Integrated Analysis/Design Systems Group of the Structures Research Unit of BCAC and the ATLAS System Group of the Boeing Computer Services Company (BCS) Integrated Systems and Systems Technology Unit. R. E. Miller, Jr. was the Program Manager of ATLAS until 1976 after which K. H. Dickenson assumed this position. The current ATLAS System is the result of the combined efforts of many Boeing engineering and programming personnel. Those who contributed directly to the current version of ATLAS are as follows:

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ABSTRACT

This document is one of a series of documents describing the ATLAS System for structural analysis and design. This volume describes a set of problems that demonstrate the various analysis and design capabilities of the ATLAS System proper as well as capabilities available by means of interfaces with other computer programs.

Input data and results for each demonstration problem are discussed. Results are compared to theoretical solutions or experimental data where possible. Listings of all input data are included.

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101. INTRODUCTION

This document describes the set of ATLAS System demonstration problems. A list of the problem decks and a brief description of each are presented in table 101-1.

The 200-series sections of this document discuss the problem used to demonstrate capabilities of the ATLAS System proper, whereas the 300-series sections discuss several analytical capabilities available to ATLAS users by means of interfaces with other computer programs.

The discussion of each demonstration problem is comprised of the following parts:

- Description of the analysis (model, loading, analysis performed, etc.)
- Presentation and discussion of results
- Listing of Control Program and input data

The features demonstrated by each deck are summarized in table 101-2. Reference 101-1 should be consulted for descriptions of system capabilities and input data formats.

Other documentation of ATLAS usage in production environments include that presented in references 101-2 through 101-7. The stress analysis of a large sports stadium (3400 nodes, 9600 elements, 20 000 freedoms, 70 million words of storage), and a detailed three-dimensional stress analysis of a gas turbine engine blade (3200 nodes, 350 solid elements, 9500 freedoms, 15 million words of storage) are described in references 101-2, 101-3 and 101-4, respectively, in terms of problem definition, solution approach, data management and cost. The automated strength resizing of an arrow-wing supersonic cruise aircraft (ref. 101-5) with approximately 20 000 design variables demonstrated the practicality of using ATLAS in the earliest stages of the interdisciplinary aeroelastic design process. Use of those methods implemented in ATLAS during its continued development to automate the strength/stiffness (flutter) aeroelastic design process for metallic and composite structural components are described in references 101-6 and 101-7.

Table 101-1. Description of Demonstration Decks

Deck Number	Document Section	Description
1	204	Substructured stress and vibration analyses of an SST
2	203	Non-substructured stress and vibration analyses of an SST
3	209	Fully stressed design and composite optimization
4	211	Flutter analysis of an SST
5	301	ATLAS to FLEXSTAB interface
6	301	FLEXSTAB to ATLAS interface
7	303	NASA-LaRC Configuration Program interface to ATLAS
8	206	Normal mode analyses of cantilever beams
9	302	ATLAS-NASTRAN interfaces
10	202	Stress, vibration and flutter analyses of a delta wing
11	201	Substructured stress and vibration analyses of a transmission tower
12	213	Stress analysis of a rotating disk
13	207	Frame buckling and superposition
14	212	Flutter analysis of a T-tail aircraft
15	205	Vibration analysis of the FIREBEE Drone
16	208	Fuel and payload management
17	210	Thermal fully stressed design

Table 101-2. Summary of Capabilities Demonstrated

CAPABILITY	DECK NUMBER																
	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17
<u>CONTROL PROGRAM PROCEDURES</u>																	
STATIC STRESS ANALYSIS, STRESS		x							x	x		x	x				
STATIC STRESS ANALYSIS, R-STRESS						x							x				
REDUCED STIFFNESS MATRIX, K-REDUCE				x				x		x				x	x		
REDUCED FLEXIBILITY MATRIX, F-REDUCE					x												
REDUCED STIFFNESS AND MASS MATRICES, REDUCE		x						x									
SUBSTRUCTURE PROCEDURES	x										x						
DESIGN, DESIGN			x														
<u>STRUCTURE DEFINITION</u>																	
GEOMETRY							x										
LOCAL ANALYSIS FRAMES												x		x	x		
SPECIAL MATERIALS												x		x	x		x
COMPOSITE MATERIALS			x														
BC SPECIFICATION	x	x	x	x	x	x		x	x	x	x	x	x	x	x	x	x
STIFFNESS ELEMENTS:																	
ROD					x	x			x		x			x	x		x
BEAM	x	x	x	x	x	x		x	x		x	x	x	x	x		
SPAR	x	x	x	x	x	x				x							
COVER		x	x	x	x	x				x							
PLATE									x						x		
GPLATE									x						x		
BRICK								x				x					
SPLATE					x	x			x						x		
CCOVER			x														
SUBSETS	x	x	x	x	x	x	x	x		x	x	x	x	x	x	x	x
SUBSTRUCTURES	x										x						
<u>STATIC LOADING</u>																	
NODAL LOADING	x	x	x						x		x	x	x				x
ELEMENT LOADING										x		x	x				
ROTATIONAL INERTIA LOADING												x					
THERMAL LOADING												x					x
SUPPORT DISPLACEMENTS													x				
SUPERPOSITION													x				
EXTERNAL NODAL LOADS MATRIX						x											
<u>WEIGHTS & DYNAMIC MODELING</u>																	
STRUCTURAL MASS	x	x						x		x	x						
NON-STRUCTURAL MASS																	
MASS ELEMENTS	x	x		x	x	x									x	x	
CONCENTRATED MASS					x			x						x	x		
FUEL																	x
PAYLOAD																	x
SUBSTRUCTURES	x										x						
FUEL AND PAYLOAD MANAGEMENT																	x
WEIGHT CALCULATION ONLY						x										x	x
REDUCED MATRIX CALCULATION																	
BY MASS PROCESSOR:																	
DIAGONAL					x			x		x							
NON-DIAGONAL				x				x			x			x	x		
ELEMENT MASS MATRICES	x	x						x									

Table continued on next page

Table 101-2. Summary of Capabilities Demonstrated (Cont'd.)

CAPABILITY	DECK NUMBER																
	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17
BUCKLING													x				
DESIGN																	
FULLY-STRESSED RESIZE			x														
THERMAL DESIGN																	x
COMPOSITE OPTIMIZATION			x														
HISTORY			x														x
UNSTEADY AERODYNAMICS & FLUTTER																	
DOUBLET LATTICE				x						x				x			
MACH BOX				x													
AF1														x			
RHO3				x													
RESIDUAL FLEXIBILITY				x													
FLUTTER				x						x				x			
PRINTED OUTPUT																	
MATERIAL DATA															x		
NODAL DATA	x	x	x	x	x		x	x	x	x	x	x	x	x	x	x	x
STIFFNESS DATA	x	x	x	x	x			x	x	x	x	x	x	x	x	x	x
BC DATA		x	x	x	x			x	x	x		x	x	x	x		
MASS																	
INPUT	x			x	x			x						x		x	
OUTPUT	x			x		x				x				x	x	x	
LOADS																	
INPUT										x		x					
OUTPUT	x	x				x						x	x				
DESIGN																	
INPUT				x													
OUTPUT				x													x
ADD/INTERPOLATE OUTPUT				x													
AF1																	
INPUT														x			
OUTPUT														x			
DOUBLET LATTICE																	
INPUT				x										x			
OUTPUT				x										x			
FLEXAIR OUTPUT				x													
FLUTTER																	
INPUT				x										x			
OUTPUT				x						x				x			
MACH BOX																	
INPUT				x													
OUTPUT				x													
RHO3																	
INPUT				x													
OUTPUT				x													
INTERACT DATA	x										x						
STRESSES:																	
ELEMENT	x	x				x			x	x	x	x	x				
PICK NODAL STRESSES													x				

Table continued on next page

Table 101-2. Summary of Capabilities Demonstrated (Cont'd)

CAPABILITY	DECK NUMBER																
	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17
PRINTED OUTPUT (Cont'd)																	
DISPLACEMENTS	x	x				x			x	x	x	x	x				
REACTIONS	x	x							x	x	x	x					
VIBRATION OUTPUT	x	x		x				x		x	x			x	x		
BUCKLING OUTPUT													x				
GRAPHICAL OUTPUT																	
STRUCTURAL GRID		x	x	x	x		x	x		x		x	x	x	x		x
MASS ELEMENTS				x	x											x	
STIFFNESS ELEMENT PROPERTIES		x															
ELEMENT STRESS CONTOURS										x							
STATIC DISPLACEMENTS												x					
VIBRATION MODE SHAPES		x						x		x					x		
BUCKLING MODE SHAPES													x				
MARGINS OF SAFETY:																	
STRENGTH			x														
THERMAL																	x
LOADABILITY DIAGRAMS																x	
ELEMENT STRESS VS. LOADCASE													x				
V-G AND V-F GRAPHS				x						x				x			
EXPLODED GEOMETRY PLOTS	x										x						
SYSTEM INTERFACES																	
ATLAS-NASTRAN									x								
ATLAS-FLEXSTAB					x	x											
ATLAS/LARC CONFIGURATION							x										

201. SUBSTRUCTURED STRESS AND VIBRATION ANALYSES OF A TRANSMISSION TOWER (DECK 11)

201.1 DESCRIPTION OF ANALYSES

The structure analyzed in this demonstration problem is a power transmission tower as shown in figure 201-1.

The structural model consists of four substructures as shown in figure 201-2. The interaction tree is shown schematically in figure 201-3. The legs of the tower were modelled with BEAM elements, the diagonals with ROD elements. Masses are obtained from the stiffness finite elements. All translational freedoms at the base are supported. Nodal loads are applied at the six hanger points.

The vibration analysis for natural frequencies and mode shapes is performed on the top level substructure using reduced stiffness and mass matrices. All translational freedoms (except TZ at the intersection of the bottom panel diagonals) are retained. The reduced mass matrices for the lowest level substructures are calculated directly by the Mass Processor.

To obtain an alternate solution, a NASTRAN (ref. 201-1) model of the same structure was made and analyzed. ROD and BAR elements were used for the structural model. All mass was specified as concentrated masses. The NASTRAN model was not substructured.

201.2 RESULTS

Nodal displacements, element stresses and reactions from the ATLAS analysis agree exactly with the corresponding quantities from the NASTRAN analysis.

Natural frequencies obtained from ATLAS are compared with the corresponding NASTRAN values in table 201-1.

...CONTINUED IN TABLE 201-1 BUT FILMED

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CORE 130K (OCTAL)

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* THIS EXAMPLE REPRESENTS AN ATLAS RUN TO PERFORM STRESS
* AND VIBRATION ANALYSES FOR A TRANSMISSION TOWER WHICH
* IS MODELED AS FOUR SUBSTRUCTURES, SS=1 TO 4. SS=5 IS
* FORMED BY INTERACTING SS=1 TO 4.
*
* THE EXECUTION SEQUENCE IS
*
* 1) READ INPLT ..... THE INPUT DATA ARE
*                        PREPROCESSED, AND WRITTEN
*                        ON THE DATA FILE. SS=1 TO 4
*                        ARE DEFINED AS STIFFNESS/MASS
*                        SETS 1 TO 4. SS=5 IS DEFINED
*                        AS SET=5 FOR VIBRATION
*                        ANALYSIS.
*
* 2) EXECUTE STIFFNESS, . COMPUTE ELEMENTAL STIFFNESSES
*    MASS                AND THE NON-DIAGONAL MASS
*                        MATRICES FOR THE RETAINED
*                        FREEDOMS FOR SETS 1 TO 4.
*
* 3) EXECUTE LOADS ..... PROCESS LOADS FOR
*                        SUBSTRUCTURES 1 AND 3. NO
*                        LOADS ARE APPLIED TO
*                        SUBSTRUCTURES 2 AND 4.
*
* 4) PERFORM SS-PERGE, .. FORM GROSS STIFFNESS AND LOAD
*    STIF,LOAD            MATRICES FOR SS=1 TO 4.
*
* 5) PERFORM SS-REDU, ... REDUCE GROSS STIFFNESS AND
*    STIF,LOAD            LOADS MATRICES FOR SS=1 TO 4.
*
* 6) PERFORM SS-MERGE, .. FORM GROSS STIFFNESS,LOADS
*    STIF,LOAD,MASS       AND MASS MATRICES FOR SS=5.
*
* 7) PERFORM SS-VSQL .... COMPUTE REDUCED STIFFNESS AND
*                        MASS MATRICES FOR SS=5 TO
*                        PERFORM SUBSEQUENT VIBRATION
*                        ANALYSIS.
*
* 8) EXECUTE MASS ..... COMPUTE MASS PROPERTIES FOR
*                        TOTAL STRUCTURE. (SET=5)
*
* 9) EXECUTE VIBRATION .. COMPUTE THE FIRST 5 FREQUEN-
*                        CIES AND MODES.
*
* 10) PERFORM SS-SSQL .... COMPUTE DISPLACEMENTS FOR
*                        SS=5.

```

```

C * 11) PERFORM ..... FROM THE DISPLACEMENT MATRI- *
C * SS-PARTITION CES FOR SS=5, EXTRACT DISPLA- *
C * CEMENTS AT RETAINED FREEDOMS *
C * FOR SS=1 TO 4. *
C *
C * 12) PERFORM SS-BACK .... PERFORM BACK SUBSTITUTION TO *
C * COMPUTE ALL DISPLACEMENTS AND *
C * REACTIONS FOR SS=1 TO 4. *
C *
C * 13) EXECUTE STRESS, .... COMPUTE ELEMENTAL STRESSES *
C * PRINT STRESSES, AND PRINT STRESSES, *
C * DISPLACEMENTS DISPLACEMENTS AND REACTIONS *
C * AND REACTIONS FOR SUBSTRUCTURES 1 TO 4 *
C *
C * 14) PRINT INPUT, ..... PRINT NOCAL AND STIFFNESS *
C * NOCAL AND INPUT DATA FOR SETS 1 TO 4 *
C * STIFFNESS *
C *
C * 15) EXECUTE GRAPHICS ... PLOT TOTAL STRUCTURE AND *
C * COMPONENT SUBSTRUCTURES *
C *
C * 16) PRINT INPUT, ..... PRINT INTERACT DATA FOR *
C * INTERACT ALL SUBSTRUCTURES. *
C *
C * 17) PRINT OUTPUT, ..... PRINT FREQUENCIES AND MODE *
C * VIBRATION SHAPES. *
C *
C * 18) ERROR PROCEDURE .... SAVE DATA FILES IF AN ERROR *
C * IS ENCOUNTERED DURING *
C * EXECUTION. *
C *
C *****
C USER COMMON (K)
C ----- 1) -----
C READ INPUT
C ----- 2) -----
C DO 10 K=1,4
C EXECUTE STIFFNESS (SET=K)
C EXECUTE MASS (SET=K,OPTION=3,CONDITION=1)
C 10 CONTINUE
C ----- 3) -----
C EXECUTE LOADS (SS=(1,3))
C ----- 4) -----
C PERFORM SS-MERGE (STIF,LOAD,SS=1 TO 4)
C ----- 5) -----
C PERFORM SS-RECU (STIF,LOAD,SS=1 TO 4)
C ----- 6) -----
C PERFORM SS-MERGE (STIF,LOAD,PASS,SS=5)
C ----- 7) -----
C PERFORM SS-VSCL (SS=5)
C ----- 8) -----
C EXECUTE MASS (SET=5,CONDITION=1)
C ----- 9) -----
C EXECUTE VIBRATION (STIF=KREDC05,MASS=PREDO05,NFREQS=5,SET=5)
C ----- 10) -----
C PERFORM SS-SECL (SS=5)
C ----- 11) -----
C PERFORM SS-PARTITION (SS=5)
C ----- 12) -----
C PERFORM SS-BACK (SS=1 TO 4)
C ----- 13) -----
C DO 20 K=1,4
C EXECUTE STRESS(SS=K)
C PRINT OUTPUT(STRESS,SS=K)
C PRINT OUTPUT(DISP,SS=K)
C PRINT OUTPUT(REACTIONS,ECCHK,SS=K)
C 20 CONTINUE
C ----- 14) -----
C DO 30 K=1,4
C PRINT INPUT (NOCAL,SET=K)
C PRINT INPUT (STIFFNESS,SET=K)

```



```

30 CONTINUE
C ----- 15) -----
EXECUTE EXTRACT(EXNAME=SS1,LSUB=KGRID,KSET=1,ESUB=E1,NSUB=N2)
EXECUTE EXTRACT(EXNAME=SS2,LSUB=KGRID,KSET=2,ESUB=E1,NSUB=N1)
EXECUTE EXTRACT(EXNAME=SS3,LSUB=KGRID,KSET=3,ESUB=E1,NSUB=N1)
EXECUTE EXTRACT(EXNAME=SS4,LSUB=KGRID,KSET=4,ESUB=E1,NSUB=N1)
EXECUTE GRAPHICS(IGNAME=GEOM,CFFLINE=CALCOMP,EXPLODE,TYPE=ORTH,
X          SIZE=(15,15),EXNAME=(SS1,SS2,SS3,SS4))
EXECUTE GRAPHICS(IGNAME=GEOM,EXPLODE,TYPE=ORTH,SIZE=(15,15),
X          TX=-250.,EXNAME=SS1,TX=0.,TY=100.,EXNAME=SS2,
X          TX=50.,TY=0.,EXNAME=SS3,TX=0.,TY=-250.,
X          EXNAME=SS4)
C ----- 16) -----
PRINT INPUT (INTERACT,NODE,SS=1 TO 5)
PRINT INPUT (INTERACT,CONN,SS=1 TO 4)
PRINT INPUT (INTERACT,RETA,SS=1 TO 4)
PRINT INPUT (INTERACT,BC,SS=1 TO 5)
PRINT INPUT (INTERACT,LOADS,SS=1 TO 5)
C ----- 17) -----
PRINT GLTPLT (VIBRATION)
ERRGR PROCEDURE
SAVE FILES
END CONTROL PROGRAM

```

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```

*/ ***** /
BEGIN NOCAL DATA /
  1 169.0 148.0 634.5 /
  2 169.0 150.0 634.5 /
  400 112.8 169.0 96.0 /
  1001 100.0 * 406.0 TO 1003 100.0 169.0 600.0 /
  101 100.0 100.0 0.0 TO 106 148.0 * 360.0 /
  401 * 238.0 *2 OF 8.0,7.0,6.0,5.0,4.0 /
  106 TO 406 148.0 190.0 ** /
  406 * 416 * 190.0 ** /
  RECDER FROM 101 /
  SET 2 /
*/ ***** /
  2 169.0 150.0 634.5 /
  300 * 225.2 56.0 /
  301 238.0 * 0.0 TO 306 190.0 * 360.0 /
  401 100.0 *3 CF 8.0,7.0,6.0,5.0,4.0 /
  306 TO 406 148.0 ** /
  406 * 416 148.0 190.0 600.0 ** /
  RECDER FROM 301 /
  SET 3 /
  1 169.0 148.0 634.5 /
  2 * 190.0 * /
  200 225.2 169.0 56.0 /
  2001 238.0 * 406.0 TO 2003 238.0 169.0 600.0 /
  201 * 100.0 0.0 * 206 190.0 148.0 360.0 /
  301 * 238.0 *2 OF 8.0,7.0,6.0,5.0,4.0 /
  206 TO 306 * 190.0 ** /
  306 * 416 148.0 190.0 600.0 ** /
  RECDER FROM 201 /
  SET 4 /
*/ ***** /
  1 169.0 148.0 634.5 /
  100 * 112.8 56.0 TO 106 148.0 * 360.0 /
  101 100.0 * 0.0 CF 8.0,7.0,6.0,5.0,4.0 /
  201 238.0 *3 TO 206 190.0 ** /
  106 TO 116 148.0 148.0 600.0 /
  206 * 216 190.0 ** /
  RECDER FROM 101 /
  END NOCAL DATA /
  BEGIN STRESS DATA /
  BEGIN PROPERTY DATA /
  P1 5.75 C. 0. 39.8 19.9 ** /
  P2 3.75 C. 0. 11.2 5.6 5.6 /
  P3 2.11 C. C. 3.6 1.8 1.8 2.11 0. 0. 3.6 1.8 1.8 111.0 /
  P4 2.11 2.11 /
  P5 1.15 ** /
  P6 3.25 3.25 /
  END PROPERTY DATA /
  BEGIN ELEMENT DATA /
  BEAM MP 101 102 400 P1 TO 105 106 400 BY 1 1 0 /
  * 401 402 400 P1 TO 405 406 400 BY 1 1 0 /
  * 101 107 406 P2 TO 115 116 406 ** /
  * 406 407 106 P2 TO 415 416 106 ** /
  * 416 2 116 P2 /
  * 116 1 416 P2 /
  * 402 400 403 P3 /
  * 102 400 103 P3 /
  ROD 401 400 P4 /
  * 101 400 * /
  * 403 400 * /
  * 103 400 * /
  * 403 103 P5 TO 416 116 /
  * 103 404 *2 115 416 BY 2 2 /
  * 404 105 *2 416 115 ** /
  * 1 2 P5 /
  * 1 416 * /
  * 1001 108 P6 TO 1003 116 BY 1 4 /

```

```

      *      *      408      *      *      416      **
      *      *      109      *
      *      *      409      *
      *      1002      113      *
      *      *      413      *
      *      1003      1      *
      *      *      2      *
END ELEMENT DATA
SET 2
*/ *****
BEGIN PROPERTY DATA
P3 2.11 C. C. 3.6 1.8 1.8 2.11 0. C. 3.6 1.8 1.8 111.0
P4 2.11 2.11
P5 1.15 **
END PROPERTY DATA
BEGIN ELEMENT DATA
BEAM ME 302 300 303 P3
BEAM 402 300 403 P3
ROD 301 300 P4
ROD 401 300 *
ROD 303 * *
ROD 403 * *
ROD 303 403 P5 TO 316 416
ROD 403 304 *2 415 316 BY 2 2
ROD 304 405 *2 314 415 **
END ELEMENT DATA
SET 3
*/ *****
BEGIN PROPERTY DATA
P1 5.75 C. 0. 39.8 19.9 **
P2 3.75 C. 0. 11.2 5.6 5.6
P3 2.11 C. C. 3.6 1.8 1.8 2.11 0. 0. 3.6 1.8 1.8 111.0
P4 2.11 2.11
P5 1.15 **
P6 3.25 3.25
END PROPERTY DATA
BEGIN ELEMENT DATA
BEAM ME 201 202 200 P1 TO 205 206 203 BY 1 1 0
* 301 302 200 P1 TO 305 306 200 BY 1 1 0
* 206 207 306 P2 TO 215 216 306 **
* 306 307 206 P2 TO 315 316 206 **
* 216 1 316 P2
* 316 2 216 *
* 202 200 203 P3
* 302 200 303 P3
ROD 201 200 P4
* 301 * *
* 203 * *
* 303 * *
* 203 303 P5 TO 216 316
* 303 204 * * 315 216 BY 2 2
* 204 305 * * 214 315 **
* 216 2 *
* 2001 208 P6 TO 2003 216 BY 1 4
* * 308 * * 316 **
* * 205 P6
* * 309 *
* 2002 212 *
* * 313 *
* 2003 1 *
* * 2 *
END ELEMENT DATA
SET 4
*/ *****
BEGIN PROPERTY DATA
P3 2.11 C. C. 3.6 1.8 1.8 2.11 0. C. 3.6 1.8 1.8 111.0
P4 2.11 2.11
P5 1.15 **
END PROPERTY DATA
BEGIN ELEMENT DATA
BEAM ME 102 100 103 P3
* 202 100 203 P3
ROD 101 100 P4

```

```

      *      201 100      *
      *      103 100      *
      *      203 100      *
      *      103 203      P5 TO 116 216
      *      203 104      *2 215 116 BY 2 2
      *      104 205      *2 114 215 **
ENC ELEMENT DATA
END STIFFNESS DATA
*/
BEGIN BC DATA
SET 1
  RETAIN TX TY TZ FCR 1001 TC 1003
  RETAIN TX TY FCR 400
  SUPPORT ALL FCR 101 401
SET 2
  RETAIN TX TY FCR 300
  SUPPORT ALL FCR 301 401
SET 3
  RETAIN TX TY TZ FCR 2001 TC 2003
  RETAIN TX TY FCR 200
  SUPPORT ALL FCR 201 301
SET 4
  RETAIN TX TY FCR 100
  SUPPORT ALL FCR 101 201
END BC DATA
*/
BEGIN MASS DATA
SET 1
  BEGIN CONCITION DATA
  STAGE 1 CCNCITION 1
  END CONCITION DATA
END MASS DATA
BEGIN MASS DATA
SET 2
  BEGIN CONCITION DATA
  STAGE 1 CCNCITION 1
  END CONCITION DATA
END MASS DATA
BEGIN MASS DATA
SET 3
  BEGIN CONCITION DATA
  STAGE 1 CCNCITION 1
  END CONCITION DATA
END MASS DATA
BEGIN MASS DATA
SET 4
  BEGIN CONCITION DATA
  STAGE 1 CCNCITION 1
  END CONCITION DATA
END MASS DATA
*/
BEGIN LOADS DATA
SET 1
  BEGIN NOCAL LCAC DATA
  CASE 1
  ORDER FX FY FZ
  1001 TC 1003 10000.0 ** 20000.0
  END NOCAL LCAC DATA
SET 3
  BEGIN NOCAL LCAC DATA
  CASE 1
  ORDER FX FY FZ
  2001 TC 2003 10000.0 ** 20000.0
  END NOCAL LCAC DATA
END LOADS DATA
*/
BEGIN SUBSET DEFINITION
SUBSETS OF STIFFNESS SET 1
E1 = ALL
E6 = E1
N1 = 1001 TC 1003
E5 = GPER IN N1

```

```

EXCLUDE E5 FRGM E6 /
N2 = ALL /
SUBSETS OF STIFFNESS SET 2 /
E1 = ALL /
N1 = ALL /
SUBSETS OF STIFFNESS SET 3 /
E1 = ALL /
N1 = ALL /
SUBSETS OF STIFFNESS SET 4 /
E1 = ALL /
N1 = ALL /
END SUBSET DEFINITION /
BEGIN INTERACT DATA /
  DEFINE SS 1 AS SET 1 STAGE 1 /
  DEFINE SS 2 AS SET 2 STAGE 1 /
  DEFINE SS 3 AS SET 3 STAGE 1 /
  DEFINE SS 4 AS SET 4 STAGE 1 /
  SS 5 /
  INTERACT 1 2 3 4 /
  BEGIN BC CHANGES /
    SS 5 /
    REFERENCE SS 1 /
    RETAIN TX TY FOR 102 TO 116 /
    *4 402 TO 416 /
    *4 1 2 /
    REFERENCE SS 3 /
    RETAIN TX TY FOR 202 TO 216 /
    *4 302 TO 316 /
  END BC CHANGES /
  DEFINE HIGHEST SS 5 AS SET 5 /
END INTERACT DATA /
END PROBLEM DATA /

```

**Table 201-1. Comparison of Natural Frequencies
for Transmission Tower**

(1) Mode Number	Frequency (Hertz)		(4)
	(2) NASTRAN	(3) ATLAS	$\frac{(3)-(2)}{(2)} \times 100$ (%)
1	7.783 87	7.813 51	0.4
2	7.851 53	7.855 62	0.4
3	10.293 9	10.834 7	5.3
4	10.294 0	10.834 8	5.3
5	10.320 3	10.862 8	5.3

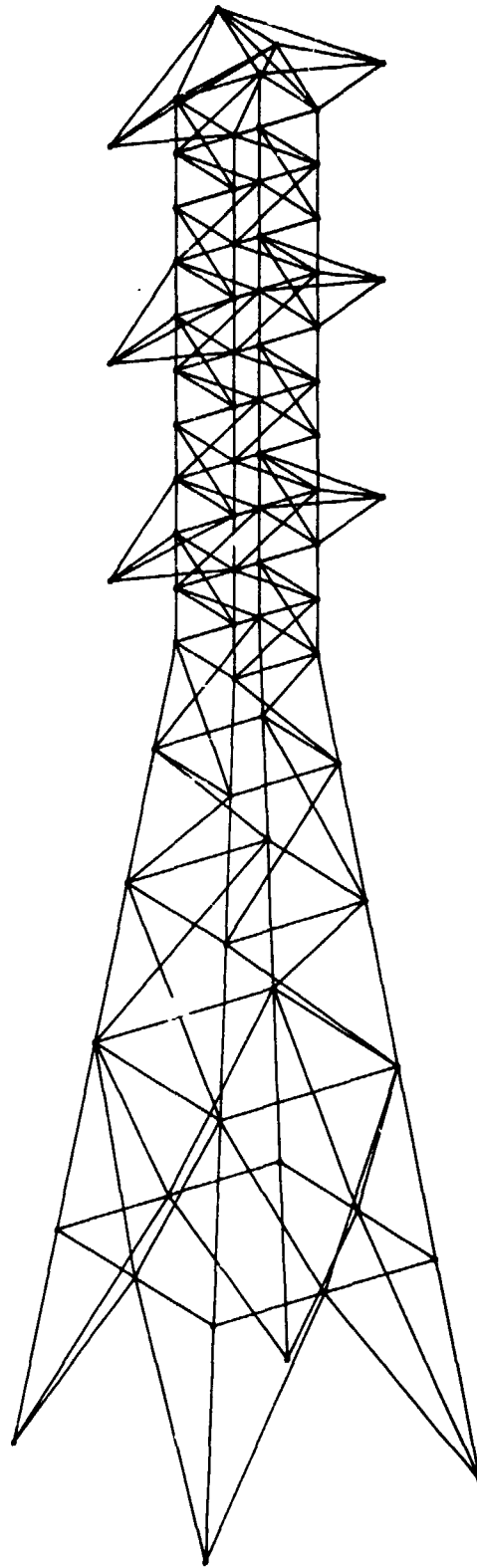


Figure 201-1. Transmission Tower

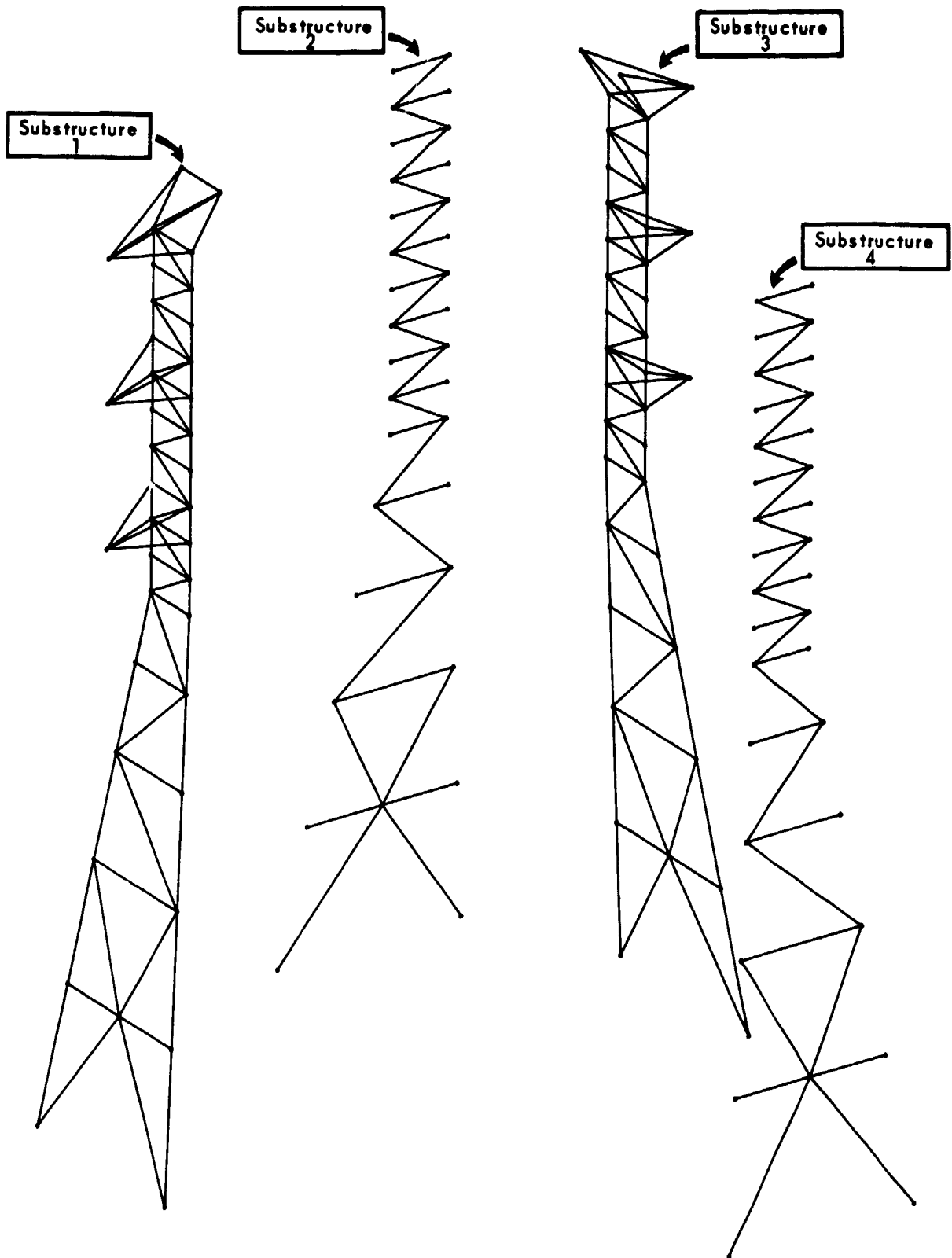


Figure 201-2. Substructure Models, Transmission Tower

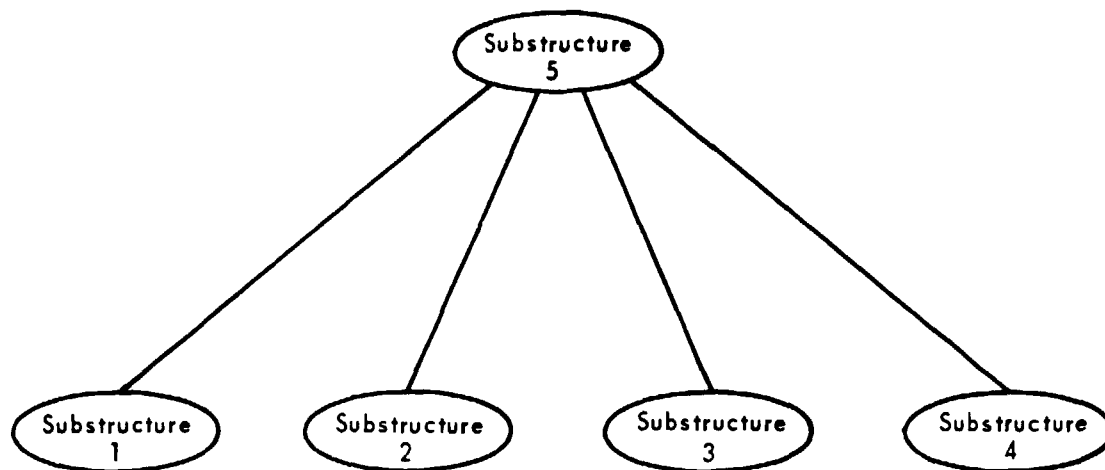


Figure 201-3. Substructure Interaction Tree, Transmission Tower

202. STRESS, VIBRATION AND FLUTTER ANALYSES OF A DELTA WING (DECK 10)

202.1 DESCRIPTION OF ANALYSES

Three analyses of a 45° delta wing are performed in this demonstration problem:

- Normal mode analysis for symmetric modes
- Flutter analysis using symmetric modes and DUBLAT aerodynamics
- Stress analysis of a cantilever wing subjected to pressure loading

The structure being analyzed is a small-scale structural model of a delta wing as described in reference 202-1. The ATLAS structural model is comprised of mid-surface nodes with SPAR and COVER elements. Because the structure is symmetric about the plane $Y=0$ only one-half of the structure is modelled. A plan view of the structural model is shown in figure 202-1. The same structural model is used for each of the three analyses.

202.1.1 Normal Mode Analysis

The mass model consists of the mass of the stiffness finite elements plus SCALAR mass finite elements representing the concentrated weights described in reference 202-1. A diagonal mass matrix is produced directly by the Mass Processor. The panels for which weights are calculated are shown in figure 202-2.

Boundary conditions are applied to the plane $Y=0$ to enforce symmetric behavior. Rigid body translation in the X-direction is eliminated by supporting TX at node 195. All Z-direction translational freedoms are retained.

The Vibration Processor is executed using reduced stiffness and mass matrices. All natural frequencies and mode shapes are calculated.

202.1.2 Flutter Analysis

The first seven vibration modes obtained in the first part of this demonstration problem are used together with DUBLAT aerodynamics to obtain flutter speeds. The Doublet Lattice box grid is shown in figure 202-3 along with a flow chart of the flutter analysis.

202.1.3 Stress Analysis

Pressure loading is applied as element loads uniformly distributed over each COVER. The pressure magnitudes vary from a maximum at $Y=16$ to a minimum at the wing tip. All freedoms are supported in the plane $Y=0$.

202.2 RESULTS

202.2.1 Normal Mode Analysis

The mass of the ATLAS model is compared to the experimentally obtained value in table 202-1. Natural frequencies of the five lowest symmetrical modes from ATLAS are compared with experimentally obtained values in table 202-2. The first mode shape along spar 2 from this analysis is compared to the shape given in reference 202-1 in figure 202-4.

202.2.2 Flutter Analysis

The results of the flutter analysis are presented as velocity vs. damping (V-g) and velocity vs. frequency (V-f) plots in figures 202-5 and 202-6.

202.2.3 Stress Analysis

Contour plots of upper surface stresses are presented in figure 202-7. Lower surface stresses are equal in magnitude and opposite in sign because of the structural symmetry and the loading antisymmetry about the wing mid-surface.

202.3 LISTING OF CONTROL PROGRAM AND DATA

BEGIN CONTROL PROGRAM DEMO10
PROBLEM 10(CENMU10 - STRESS/FLUTTER ANALYSES OF A DELTA WING)

PURPOSE THE PRINCIPAL ATLAS CAPABILITIES DEMONSTRATED BY THIS DECK ARE

1. NORMAL MODE ANALYSIS
2. PLOT OF VIBRATION MODE SHAPE
3. FLUTTER ANALYSIS - DUBLAT AERODYNAMICS
4. V-G AND V-F PLOTS
5. STRESS ANALYSIS
6. STRESS CONTOUR PLOTS

AUTHOR **F.P. GRAY**

CORE 130K (OCTAL)

METHOD THE SYSTEM IS EXECUTED TO DEMONSTRATE THE PROCEDURE TO OBTAIN STRESSES, DISPLACEMENTS, AND A FLUTTER SOLUTION FOR A DELTA WING.

```
*****
*
* THIS DECK DEMONSTRATES AN ATLAS ANALYSIS OF THE 45 DEGREE
* DELTA WING DESCRIBED IN NACA TN 3999.
*
* THE PROBLEM TO BE EXECUTED CONTAINS
*
*     117 STRUCTURAL NODES
*     154 SPAR ELEMENTS
*     102 COVER ELEMENTS
*
*****
```

READ INPUT

PRINT THE STIFFNESS AND LOADS INPUT DATA. PLOT GEOMETRY.

```

PRINT INPUT (NODAL,SUBSETS,N1=INPUT,N2)
PRINT INPUT (STIFFNESS,SUBSETS,E10,E20,E30)
PRINT INPUT (LOADS,STAGE=Z)
EXECUTE EXTRACT (EXNAME=NACA1,LSUB=KGRID,ESUB=E10,NSUB=N1)
EXECUTE GRAPHICS (IGNAME=PLANVIEW,OFFLINE=CALCOMP,TYPE=(ORTH,
X          POINT),LABEL=N,SCALE=.05,VIEW=100,EXNAME=NACA1)
EXECUTE EXTRACT (EXNAME=NACA2,LSUB=KGRID,ESUB=E25,NSUB=N25)
EXECUTE GRAPHICS (IGNAME=REARSPAR,TYPE=ORTH,LABEL=N+E,SCALE=.10,
X          VIEW=1000000,EXNAME=NACA2)

```

GENERATE THE REDUCED STIFFNESS MATRIX.

```
PERFORM K-REDUCE
PRINT INPUT(BC)
```

GENERATE AND PRINT THE DIAGONAL MASS MATRIX,PANEL WEIGHT MATRIX,AND WEIGHT STATEMENT.

```
EXECUTE MASS (OPTION=2)
PRINT OUTPUT(MASS,STATEMENT,SUMMARY,MDC=MDC****)
```

GENERATE AND PRINT THE MODES, FREQUENCIES, GENERALIZED MASS, AND
GENERALIZED STIFFNESS. PRODUCE MODE SHAPE PLOT.

```
EXECUTE VIBRATION(STIF=KRED,MASS=MDC001A,NMODES=7,SUBSETS=(N1,
X          N29))
```

```

PRINT OUTPUT(VIBRATION,SUBSETS=(N1,N29))
EXECUTE EXTRACT(EXNAME=SPAR2,LSUB=VMODE,VSET=1,NSUB=N29,MODE=3,
X      BSUB=ON2)
EXECUTE GRAPHICS(GNAME=MODES,TYPE=ORTH,SCALE=.1,VX=-1.,
X      VECTOR3=VMODE,VSCALE=60.,EXNAME=SPAR2)

C
C
C      GENERATE,PRINT,AND PLOT THE FLUTTER DATA.

EXECUTE INTERPOLATION(N1=(SURFSPLINE,CMOD),DOF=1000)
EXECUTE DUBLAT(COND=1,MACH=.5,KVAL=(35.0,14.2,5.0,2.2,1.0),
1      BREF=112.0)
EXECUTE ADDINT(ID=FCHCK,INT,DUBLAT,IGAIN=9,MACH=.5)
EXECUTE FLUTTER(GAFID=FCHCK)
PRINT OUTPUT(FLUTTER)
EXECUTE EXTRACT(EXNAME=FCASE1,LSUB=VGVF)
EXECUTE GRAPHICS(GNAME=FLUTTER,TYPE=GRAPH,SIZE=(10,10),
X      X=V,Y1=G,Y2=F,XMIN=J.,XMAX=3000.,Y1MIN=-.2,
X      Y2MIN=0.,Y1MAX=.1,Y2MAX=200.,EXNAME=FCASE1)

C
C
C      GENERATE AND PRINT THE ELEMENT STRESSES,NODAL DISPLACEMENTS,
      AND REACTIONS. PLOT STRESS CONTOURS.

PERFORM STRESS(STAGE=2,[K]=[S])
PRINT OUTPUT(STRESSES,STAGE=2)
PRINT OUTPUT(DISPLACE,STAGE=2)
PRINT OUTPUT(REACTIONS,STAGE=2,R3=R31,EQCHK)
EXECUTE EXTRACT(EXNAME=NACA3,LSUB=STRESS,ESUB=E10,NSUB=N1,
X      STAGE=2,BSUB=ON1)
EXECUTE GRAPHICS(GNAME=CONTOURS,TYPE=CONTOUR,SIZE=(15,15),
X      SCALAR=COVSIGMA1U,FLEV=-250.,LLEV=0.,
X      INTLEV=25.,EXNAME=NACA3)
EXECUTE GRAPHICS(GNAME=CONTOURS,TYPE=CONTOUR,SIZE=(15,15),
X      SCALAR=COVSIGMA2U,FLEV=-60.,LLEV=30.,
X      INTLEV=10.,EXNAME=NACA3)

C
C
C      INDEX THE RANDOM ACCESS FILES.

CALL PRNTCAT
INDEX FILES
END

```

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```

BEGIN NODAL DATA
  /* STRUCTURAL NODES
    15 196.0 0.0 0.0 2.72 TO 195 100.0 0.0 0.0 2.72 BY 15 /
    **2 -1 0.0 8.0 0.0 0.0 0 -1 0.0 8.0 0.0 0.0 0 0 /
        1 196.0 112.0 0.0 0.844 TO 193
        1 TO 13
        1 0 15
    **11 16
  /* AUXILIARY PANEL NODES
    310 196. 0. 0. TO 316 100. 0. 0.
    320 * 16. *2 326 * 16. 0.
    330 * 28. *2 336 112. 28. 0.
    340 * 40. *2 346 124. 40. 0.
    350 * 40. *2 354 124. 40. 0.
    360 * 56. *2 364 140. 56. 0.
    370 * 72. *2 374 156. 72. 0.
    380 * 88. *2 382 172. 88. 0.
    390 * 112. 0.
END NODAL DATA
BEGIN STIFFNESS DATA
BEGIN ELEMENT DATA
  /* RIB ELEMENTS
    SPAR M01 15.30 0.0254 .01905 TO 180,195 BY 15,15
    *2 14.29 0.0508 .03810 TO 179,194 **
    *2 13.28 0.1412 .12355 TO 178,193 **
    *2 12.27 0.0508 .03810 TO 162,177 **
    **9 0.0 -1,-1 010 .0 0 -16,-16 0,0,0
        *2 2.17 *2
  /* SPAR ELEMENTS
    SPAR 1 2 0.0695 0.201362 TO 3 4
    * 4 5 0.0695 0.474579 TO 14 15
    * 49 50 0.0701 0.477268 TO 59 60
    * 97 98 0.0718 1.498695 TO 104 105
    * 145 146 0.0720 0.205169 TO 149 150
    * 153 154 0.0706 0.039597 TO 194 195
    * 1 17 0.0706 0.039597 TO 177 193 BY 16 16
  /* COVER ELEMENTS
    COVER N1001 1 2 17 0.0696 0.0281 0. TO N1166 177 178 193
    BY N15 16 16
    COVER N1002 2 3 18 17 0.0696 0.0281 0. TO N1014 14 15 30 29
    **11 0 15 16 **3 0. 0. 0. 0 14 15 **3
END ELEMENT DATA
END STIFFNESS DATA
/*
BEGIN BC DATA
  STAGE 1
    RETAIN TZ FOR 1 TO 195
    SUPPORT TX FOR 195
    SUPPORT ASYM IN SURFACE 2 THROUGH 15
  STAGE 2
    SUPPORT ALL FOR 15 TO 195 BY 15
END BC DATA
/*
BEGIN MASS DATA
  BEGIN MASS ELEMENT DATA
    SCALAR F2 NODE002 2 .003
    SCALAR F2 NODE003 3 .003
    SCALAR F2 NODE004 4 .003
    SCALAR F2 NODE005 5 .008
    SCALAR F2 NODE006 6 .009
    SCALAR F2 NODE007 7 .012
    SCALAR F2 NODE008 8 .014
    SCALAR F2 NODE009 9 .017
    SCALAR F2 NODE010 10 .020
    SCALAR F2 NODE011 11 .022
    SCALAR F2 NODE012 12 .025
    SCALAR F2 NODE013 13 .058
    SCALAR F2 NODE014 14 .026
    SCALAR F2 NODE015 15 .013
    SCALAR F2 NODE017 17 .003
    SCALAR F2 NODE033 33 .003
    SCALAR F2 NODE049 49 .003
    SCALAR F2 NODE050 50 .008
    SCALAR F2 NODE051 51 .009

```

SCALAR	F2	NODE152	52	.012
SCALAR	F2	NODE053	53	.014
SCALAR	F2	NODE054	54	.017
SCALAR	F2	NODE055	55	.020
SCALAR	F2	NODE056	56	.022
SCALAR	F2	NODE057	57	.025
SCALAR	F2	NODE058	58	.058
SCALAR	F2	NODE059	59	.026
SCALAR	F2	NODE060	60	.013
SCALAR	F2	NODE065	65	.004
SCALAR	F2	NODE081	81	.004
SCALAR	F2	NODE097	97	.006
SCALAR	F2	NODE098	98	.014
SCALAR	F2	NODE099	99	.017
SCALAR	F2	NODE100	100	.020
SCALAR	F2	NODE101	101	.022
SCALAR	F2	NODE102	102	.025
SCALAR	F2	NODE103	103	.058
SCALAR	F2	NODE104	104	.026
SCALAR	F2	NODE105	105	.013
SCALAR	F2	NODE113	113	.006
SCALAR	F2	NODE129	129	.007
SCALAR	F2	NODE145	145	.008
SCALAR	F2	NODE146	146	.008
SCALAR	F2	NODE147	147	.010
SCALAR	F2	NODE148	148	.020
SCALAR	F2	NODE149	149	.010
SCALAR	F2	NODE150	150	.005
SCALAR	F2	NODE161	161	.008
SCALAR	F2	NODE177	177	.010
SCALAR	F2	NODE193	193	.298
SCALAR	F2	NODE194	194	.010
SCALAR	F2	NODE195	195	.2445

END MASS ELEMENT DATA
 BEGIN CONDITION DATA
 STAGE 1 CONDITION 1
 PANEL DATA 1 CONDITION 2
 END CONDITION DATA
 BEGIN PANEL DATA 1
 1 315 316 326 325 TO 6 BY 1 -1 **3
 **2 6 10 10 10 10 0 6 0 **5
 19 353 354 364 363 TO 22 **
 **1 4 10 10 10 10 0 4 0 **5
 27 372 374 382 381 TO 28 BY 1 -2 -2 -1 -1
 29 380 382 390
 END PANEL DATA
 BEGIN LABEL DATA
 LEVEL1 ** TOTAL WING STRUCTURE *
 EK10 ** COVER MATERIAL *
 EK30 ** RIB MATERIAL *
 LEVEL2 ** SPAR MATERIAL *
 EK21 ** SPAR 1 (FS) *
 EK22 ** SPAR 2 *
 EK23 ** SPAR 3 *
 EK24 ** SPAR 4 *
 EK25 ** SPAR 5 (RS) *
 END LABEL DATA
 END MASS DATA
 BEGIN LOADS DATA
 STAGE 2
 LOAD CASE 10 AIRLOAD **PRESSURE LOAD ON ENTIRE WING SURFACE*
 BEGIN ELEMENT LOAD DATA
 CASE AIRLOAD
 DIRECTION GLOBAL 0. 0. 1.
 1014 TO 1168 BY 14 .2
 1013 TO 1167 BY 14 .15
 1012 TO 1166 BY 14 .10
 **10 -1 0 -15 0 0 -.01
 1001 .005
 END ELEMENT LOAD DATA
 END LOADS DATA

```

BEGIN SUBSET DEFINITION
SUBSETS OF STIFFNESS SET 1
*/ SUBSETS OF ALL STRUCTURAL NODES AND ELEMENTS
  E1 = ALL
  N1 = ALL
  N2 = 300 TO 400
  EXCLUDE N2 FROM N1
*/ SUBSET OF ALL COVER ELEMENTS
  E10 = COVERS
*/ SUBSETS OF ELEMENTS FOR THE WING SPARS
  N21 = 1 TO 193 BY 16 194 195
  E21 = IN N21
  E22 = SLAB X 124.0
**3 1 0 0 0 2440
  N25 = NODES IN E25
*/ SUBSET OF ALL WING SPARS
  E20 = E21 U E22 U E23 U E24 U E25
*/ SUBSET OF ALL SPAR ELEMENTS
  E100 = SPARS
*/ SUBSET OF ALL WING RIBS
  E30 = E100
  EXCLUDE E20
*/ RETAINED NODES ON SPAR 2
  N29 = 45 TO 60
*/ BOUNDARY SUBSET FOR STRESS CONTOUR PLOTS
  ON1 = 1 TO 15, 30 TO 195 BY 15, 194, 193 TO 17 BY -16
*/ SUBSET FOR MODE SHAPE PLOT
  ON2 = 49 **11+1
END SUBSET DEFINITION
BEGIN FLUTTER DATA
CASE 1 ** NACA DELTA WING *
  ALTITUDE 500.0
END FLUTTER DATA
*/
BEGIN DUBLAT DATA
BEGIN GEOMETRY DATA
LIFTING SURFACE DATA
PANEL WING1 100.0 196.0 100.0 196.0 0. 16.0 0. 0.
  CHORD DIV 0. 0.1 0.2 0.3 0.4 0.5 0.6 0.7 0.8 0.9 1.0
  SPAN DIV 0. 1.0
PANEL WING2 100.0 196.0 190.0 196.0 16.0 112.0 0. 0.
  CHORD DIV 0. 0.1 0.2 0.3 0.4 0.5 0.6 0.7 0.8 0.9 1.0
  SPAN DIV 0. 0.1 0.2 0.3 0.4 0.5 0.57 0.64 0.7 0.75 0.8
    0.85 0.88 0.92 0.95 0.98 1.0
END GEOMETRY DATA
BEGIN SUBSET DATA
SUBSETS OF BOXES
  SUBSET SS 1 TO 170
END SUBSET DATA
BEGIN MODAL DATA
  USE CMOD WITH LIFTING SURFACE SS
END MODAL DATA
END DUBLAT DATA
END PROBLEM DATA

```


**Table 202-1. Mass Comparison for
Delta Wing**

Experimental (ref. 202-1)	185.330 kg (408.583 lb)
ATLAS	185.298 kg (408.514 lb)

**Table 202-2. Comparison of Natural Frequencies
for Symmetric Modes of Delta Wing**

(1) Mode	Frequency (Hertz)		(4)
	(2) Experimental (ref. 202-1)	(3) ATLAS	$\frac{(3)-(2)}{(2)} \times 100$ (%)
1	43.3	47.7	10.2
2	88.8	91.4	2.9
3	122.8	127.5	3.8
4	164.2	169.0	2.9
5	179.7	191.4	0.9



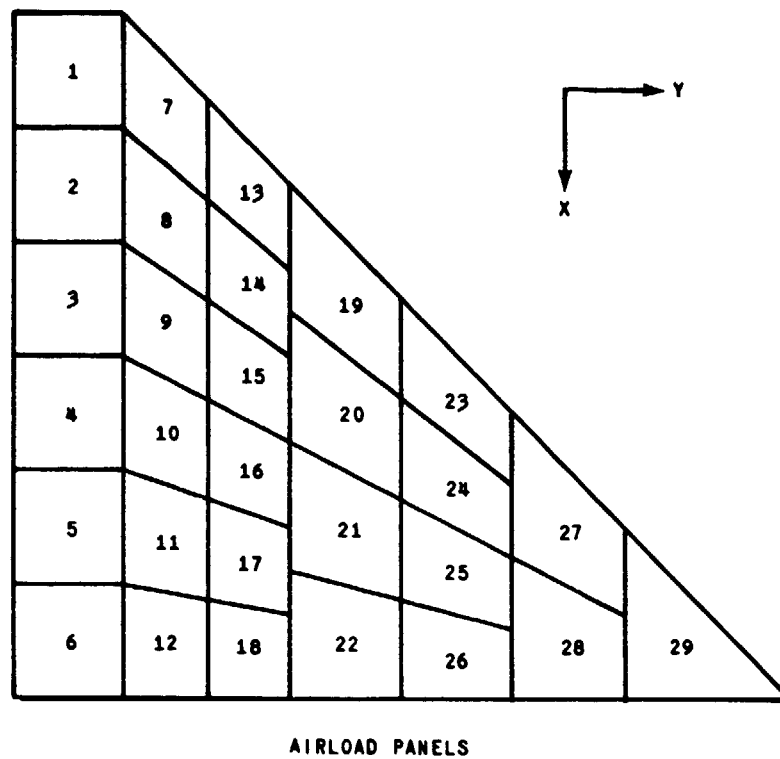


Figure 202-2. Delta Wing Weights Panels

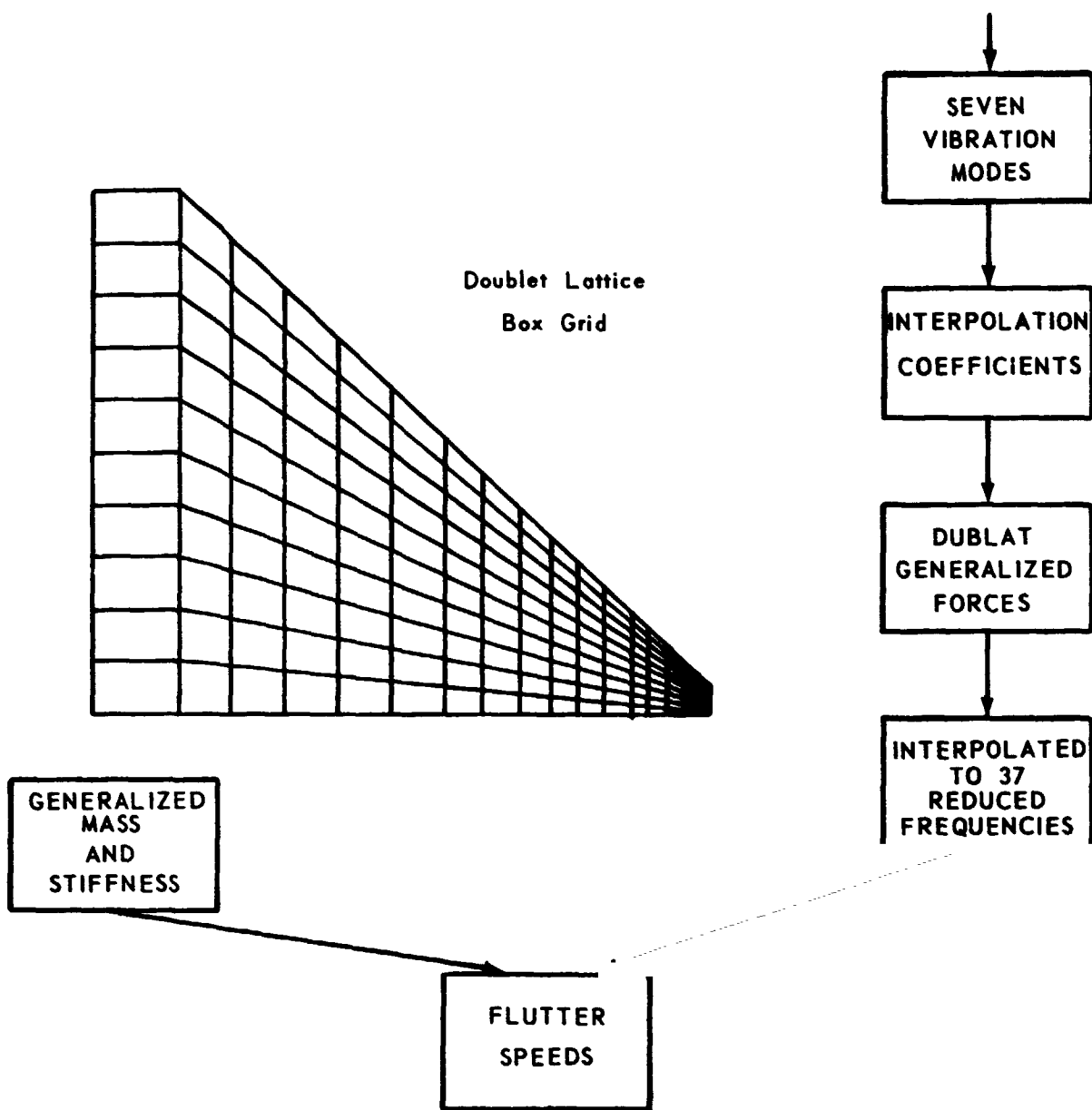


Figure 202-3. Flutter Analysis of Delta Wing

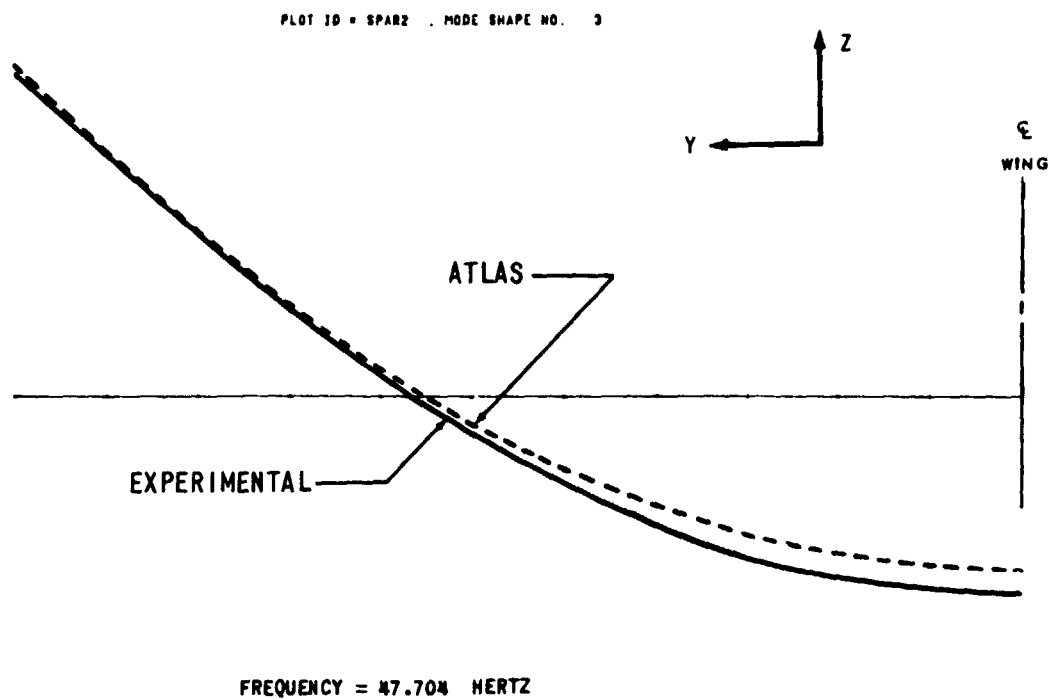


Figure 202-4. First Flexible Mode Shape along Spar 2 of Delta Wing

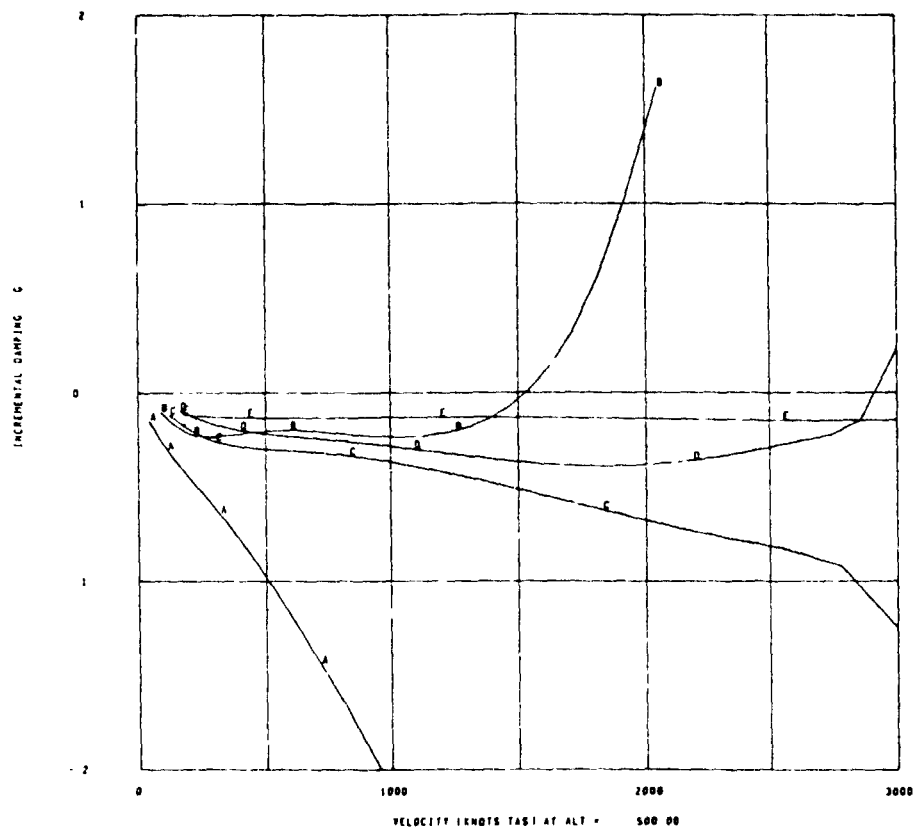


Figure 202-5. Flutter V-g Plot, Delta Wing

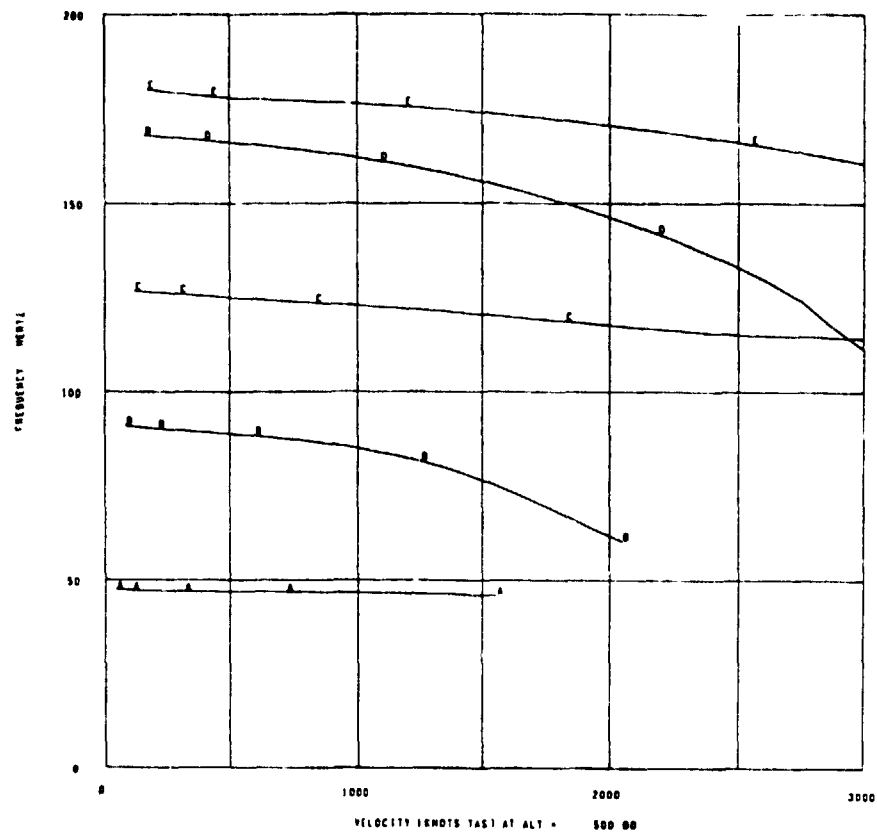
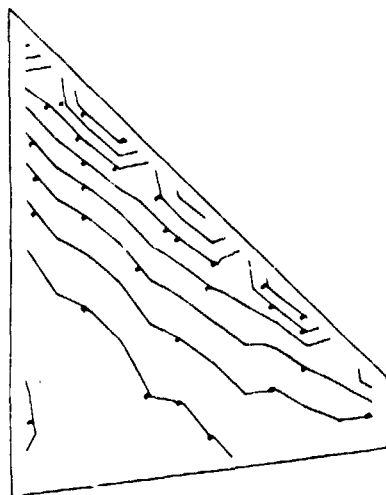
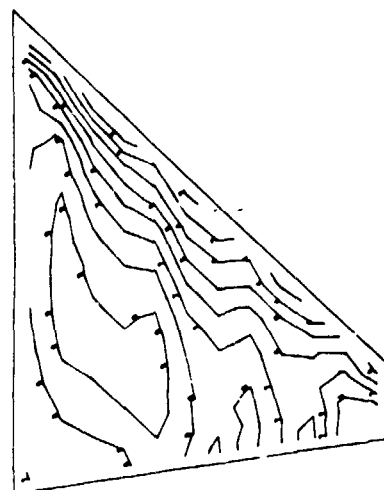


Figure 202-6. Flutter V-f Plot, Delta Wing



SIGMA1U



SIGMA2U

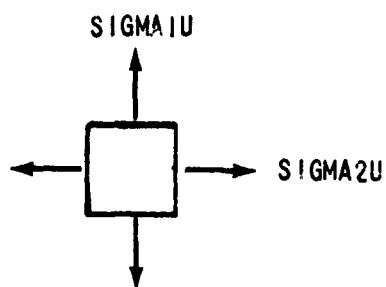


Figure 202-7. Delta Wing Upper Surface Stress Contours - Pressure Loading

203. STRESS AND VIBRATION ANALYSES OF AN SST AIRCRAFT (DECK 2)

203.1 DESCRIPTION OF ANALYSES

An SST aircraft is analyzed to obtain symmetric vibration modes and stresses due to pressure loads applied to the wings. Because of structural symmetry only one half of the aircraft is modelled.

The stiffness finite element model is shown in figure 203-1. Mid-surface nodes with SPAR and COVER elements are used for the wing, wing fin and horizontal tail. The body is modelled with BEAM elements the properties of which are shown in figure 203-2. Mass is obtained from the stiffness finite elements.

203.1.1 Vibration Analysis

Symmetric boundary conditions are applied in the plane $Y=0$. The degrees of freedom retained in the normal mode analysis are shown in figure 203-3. Rotational degrees of freedom are retained only at control surfaces. Rigid body translation in the X-direction is eliminated by supporting TX at the aftmost body node. The pitching and Z-translation rigid body modes are included in the analysis.

The analysis is performed using a reduced stiffness matrix and a reduced mass matrix obtained by Guyan reduction of the merged elemental mass matrices.

203.1.2 Stress Analysis

Symmetric boundary conditions are applied in the plane $Y=0$. Rigid body motions are eliminated by supporting X and Z-direction translations and rotation about the Y axis at the aftmost body node. The pressure loading is simulated with nodal loads.

203.2 RESULTS

Natural frequencies of the first eight modes are given in table 203-1. The third mode shape is shown in figure 203-4; this is the first flexible mode.

203.3 LISTING OF CONTROL PROGRAM AND DATA

```

C BEGIN CONTROL PROGRAM DEM002
C PROBLEM 10IDEM002 - STRESS/VIBRATION ANALYSES OF AN SST)
C
C PURPOSE      THE PRINCIPAL CAPABILITIES DEMONSTRATED BY
C               THIS DECK ARE
C               1. STRESS ANALYSIS
C               2. NORMAL MODE ANALYSIS
C               3. ELEMENT PROPERTY PLOTS
C               4. VIBRATION MODE SHAPE PLOTS
C
C AUTHOR       R.A. SAMUEL
C
C CORE         150K (OCTAL)
C
C METHOD        THE RESULTS OBTAINED FROM THIS DECK SHOULD BE THE
C               SAME AS THOSE FROM DECK DEM001.
C
C READ INPUT
C PRINT INPUT (NDOAL)
C PRINT INPUT(STIFFNESS)
C EXECUTE EXTRACT(EXNAME=GEOM,LSUB=KGRID,ESUB=E1,NSUB=N1)
C EXECUTE GRAPHICS(GNAME=GEOMETRY,OFFLINE=CALCOMP,TYPE=ORTH,
X             POINT),SIZE=(20.,20.),RZ=30.,RX=0.,RY=20.,
X             EXNAME=GEOM)
C EXECUTE EXTRACT(EXNAME=PROPS,LSUB=KPROP,ESUB=E2,NSUB=N2)
C EXECUTE GRAPHICS(GNAME=BODY,TYPE=ORTH,SIZE=(10,10),
X             SCALAR=BWIZ(1),SSCALE=.002,EXNAME=PROPS)
C EXECUTE GRAPHICS(GNAME=BODY,TYPE=ORTH,SIZE=(10,10),
X             SCALAR=BMA(1),SSCALE=5.,EXNAME=PROPS)
C PERFORM REDUCE
C PRINT INPUT(BC)
C EXECUTE VIBRATION (STIF=KRED,MASS=MRED,NFREQS=8)
C PRINT OUTPUT (VIBRATION)
C EXECUTE EXTRACT(EXNAME=MODE3,LSUB=VMODE,VSET=1,MODE=3,BSUB=ON1)
C EXECUTE GRAPHICS(GNAME=VMODES,TYPE=ORTH,SIZE=(20,20),
X             RX=0.,RZ=20.,RY=20.,VECTOR2=VMODE,VSCALE=100.,
X             EXNAME=MODE3)
C PURGE FILES(STIFRNF,MERGRNF,MASSRNF,MULTRNF,CHOLRNF,VIBRRNF)
C PERFORM STRESS(STAGE=2)
C PRINT INPUT(BC,STAGE=2)
C PRINT OUTPUT(LOADS,STAGE=2)
C PRINT OUTPUT(STRESS,STAGE=2)
C PRINT OUTPUT(DISP,STAGE=2)
C PRINT OUTPUT(REACTIONS,STAGE=2,EQCHK)
C END CONTROL PROGRAM

```

*/ MODE2 /
BEGIN NODAL DATA

*/
*/ BODY NODES
*/

1	20.	0.	0.		TO	25	9.	0.	0.	BY	2
27	1060.	0.	0.	30.0	TO	45	1780.	0.	0.	BY	2
**1	200	0.	65.	0.	0	200	0.	65.		**	
45					TO	55	2180.	0.	0.	BY	2
**1	200				0	200	0.	65.		**	
55					TO	63	2500.	0.	0.	BY	2
**1	200				0	200	0.	65.		**	
65	2580.	0.	0.		TO	77	3060.	0.	0.	BY	2
79	3140.	0.	0.	3.0							
**1	200	0.	65.	**							
81	3220.	0.	0.	6.5							
**1	200	0.	65.	**							
83	3300.	0.	0.	7.0							
**1	200	0.	65.	**							
85	3380.	0.	0.	2.0							
**1	200	0.	65.	**							
87	3460.	0.	0.								
89	3540.	0.	0.								

*/
*/ WING NODES
*/

427	1060.	65.	0.	30.0	TO	435	1380.	180.	0.	17.5	BY	2
435					TO	445	1780.	180.	0.	27.5	BY	2
445					TO	455	2180.	180.	0.	25.0	BY	2
455					TO	463	2500.	180.	0.	13.0	BY	2
635	1380.	180.	0.	17.5	TO	641	1620.	265.	0.	10.0	BY	2
641					TO	655	2180.	265.	0.	22.5	BY	2
655					TO	663	2500.	265.	0.	12.5	BY	2
841	1620.	265.	0.	10.0	TO	847	1971.	380.	0.	9.0	BY	2
847					TO	855	2291.	380.	0.	17.0	BY	2
855					TO	863	2611.	380.	0.	10.0	BY	2
1047	1971.	380.	0.	9.0	TO	1051	2205.	455.	0.	8.5	BY	2
1051					TO	1059	2525.	455.	0.	15.0		
1059					TO	1063	2685.	455.	0.	8.0		
1251	2205.	455.	0.	8.5	TO	1254	2409.	538.	0.	6.5		
1254					TO	1259	2609.	538.	0.	11.0		
1259					TO	1263	2769.	538.	0.	5.5		
1454	2409.	538.	0.	6.5	TO	1456	2545.	594.	0.	5.0		
1456					TO	1459	2665.	594.	0.	7.5		
1459					TO	1463	2825.	594.	0.	3.5		
1656	2545.	594.	0.	5.0	TO	1658	2710.	680.	0.	3.0		
1658					TO	1663	2910.	680.	0.	3.0		
1858	2710.	680.	0.	3.0	TO	1860	2875.	765.	0.	1.5		
1860					TO	1863	2995.	765.	0.	2.5		

*/
*/ WING TRAILING EDGE NODES
*/

3001	2500.	65.	0.	13.5	TO	3005	2580.	65.	0.	1.0	BY	2
3101	2500.	180.	0.	13.0	TO	3105	2580.	180.	0.	1.0	**	
3201	2500.	265.	0.	12.5	TO	3205	2580.	265.	0.	1.0	**	
3305	2830.	538.	0.	1.0	TO	3605	3045.	765.	0.	1.0		

BY 100 OF 56. 88. 85.

*/
*/ WING FIN NODES
*/

REC	WINGFIN	0.	594.	0.	1.	594.	0.	0.	-1.	0.		
2056	2545.	.1	0.	3.5	TO	2456	2830.	100.	0.	2.5	BY	200
2058	2625.	.1	0.	3.5	TO	2458	2842.	100.	0.	3.0	**	
2061	2745.	.1	0.	4.0	TO	2461	2859.	100.	0.	3.0	**	
2063	2825.	.1	0.	4.0	TO	2463	2870.	100.	0.	3.0	**	

*/
*/ HORIZONTAL TAIL NODES
*/

RESUME GLOBAL												
279					TO	679	3365.	200.	0.	2.0	BY	200
281					TO	681	3388.	200.	0.	2.5	**	
283					TO	683	3412.	200.	0.	2.5	**	
285					TO	685	3435.	200.	0.	1.0	**	

END NODAL DATA

BEGIN STIFFNESS DATA

BEGIN PROPERTY DATA

P1 .05 1. *(WING FIN SPARS AND RIBS)
P2 2. 0. 0. .2 .2 .2 *(WING FIN ATTACHMENT BEAMS - TYPE 1)
P3 10. 0. 0. 100. 100. 100. *(WING FIN ATTACHMENT BEAMS - TYPE 2)
P4 .15 .50 *(CONTROL SURFACE RIBS)
P5 0. *2 100. 100. 0. 10. *(BEAMS AT 455 RIB TO PICK UP SPARS)

END PROPERTY DATA

BEGIN ELEMENT DATA

*/

*/ WING FRONT SPAR

*/

SPAR	M5	N2003	227	425	.12	2.						
*2		N2205	429	431	.12	2.	TO	N2605	433	435	+	
							BY	N200	2	2		
*2		N2805	435	637	.12	2.						
*2		N3007	637	635	.12	2.	TO	N3207	639	641	+	
							BY	N200	2	2		
*2		N3407	641	843	.12	2.						
*2		N3609	843	845	.12	2.	TO	N3809	845	847	+	
							BY	N200	2	2		
*2		N4009	847	1045	.12	2.						
*2		N4211	1049	1051		**						
*2		N4411	1051	1253		**						
*2		N4613	1253	1254		**						
*2		N4713	1254	1455		**						
*2		N4815	1455	1456		**						
*2		N4915	1456	1657		**						
*2		N5017	1657	1658		**						
*2		N5117	1658	1855		**						
*2		N5219	1859	1860		**						

*/

*/ WING REAR SPAR

*/

SPAR	M5	N5603	263	463	.40	12.						
*2		N5605	463	663	.40	12.						
*2		N5607	663	863	.34	12.						
*2		N5609	863	1063	.34	12.						
*2		N5611	1063	1263	.30	8.						
*2		N5613	1263	1463	.30	8.						
*2		N5615	1463	1663	.30	4.						
*2		N5617	1663	1863	.30	4.						

*/

*/ WING INTERMEDIATE SPARS

*/

SPAR	M5	N2203	229	425	.20	2.	TO	N3603	243	443	+	
							BY	N200	2	2		
*2		N3803	245	445	.36	2.						
*2		N4803	255	455	.60	12.						
*2		N5003	257	457	.24	12.	TO	N5403	261	461	+	
							BY	N200	2	2		
*2		N3005	437	637	.20	2.	TO	N3605	443	643	+	
							BY	N200	2	2		
*2		N3805	445	645	.36	2.						
*2		N4005	447	647	.20	4.	TO	N4605	453	653	+	
							BY	N200	2	2		
*2		N4805	455	655	.60	12.						
*2		N5005	457	657	.24	12.	TO	N5405	461	661	+	
							BY	N200	2	2		
*2		N3607	643	843	.20	2.	TO	N3807	645	845	+	
							BY	N200	2	2		
*2		N4007	647	847	.20	4.	TO	N4607	653	853	+	
							BY	N200	2	2		
*2		N4807	655	855	.20	8.						
*2		N5007	657	857	.20	10.	TO	N5407	661	861	+	
							BY	N200	2	2		
*2		N4209	849	1049	.20	4.	TO	N4609	853	1053	+	
							BY	N200	2	2		
*2		N4809	855	1055	.20	8.						
*2		N5009	857	1057	.20	10.	TO	N5409	861	1061	+	
							BY	N200	2	2		
*2		N4611	1053	1253	.12	4.	TO	N4811	1055	1255	+	
							BY	N100	1	1		

*2	N4911	1056	1256	.06	4.	TO N5511	1062	1262	+	
						BY N100	1	1		
*2	N4813	1255	1455	.12	4.					
*2	N4913	1256	1456	.06	4.	TO N5513	1262	1462	+	
						BY N100	1	1		
*2	A5015	1457	1657	.06	2.	TO N5515	1462	1662	+	
						BY N100	1	1		
*2	N5217	1659	1859	.06	2.	TO N5517	1662	1862	+	
						BY N100	1	1		
*/ WING IN-BOARD SPARS										
SPAR	M5	N2001	27	227	1.00	10.	TO N3601	43	243	+
							BY N200	2	2	
*2		N3801	45	245	1.80	10.	TO N4601	53	253	+
							BY N200	2	2	
*2		N4801	55	255	3.00	60.				
*2		N5001	57	257	1.20	60.	TO N5401	61	261	+
							BY N200	2	2	
*2		N5601	63	263	2.00	60.				
*/ WING RIBS										
SPAR	M5	N6001	227	229	.25	4.	TO N6035	261	263	+
							BY N2	2	2	
*2		N6109	436	437	.30	4.	TO N6135	461	463	+
							BY N2	2	2	
*2		N6215	641	643	.20	3.	TO N6235	661	663	+
							BY N2	2	2	
*2		N6425	1051	1053	.20	4.				
*2		N6425	1053	1054	.20	4.	TO N6435	1062	1063	
*2		N6625	1456	1457	.12	2.	TO N6635	1462	1463	
*2		N6833	1860	1861	.30	1.4	TO N6835	1862	1863	
*/ WING COVERS										
COVER	M5	N7003	229	429	227	.06				
*2		N7203	229	429	431	.06				
		N8603	243	443	445	245	BY N200	2	*=3	+
*2		N8803	245	445	447	247	.12	.00		
		N9603	253	453	455	255	BY N200	2	*=3	
*2		N9803	255	455	457	257	.10	.14		
*2		N10003	257	457	459	259	**			
*2		N10203	259	459	461	261	.26	.14 .22	.00	
*2		N10403	261	461	463	263	**			
*2		N7805	437	637	435	.06				
*2		N8005	437	637	639	439	.06			
		N9605	453	653	655	455	BY N200	2	*=3	+
*2		N9805	455	655	657	457	.10	.14		
*2		N10005	457	657	659	459	**			
*2		N10205	459	659	661	461	.26	.14 .22	.00	
*2		N10405	461	661	663	463	**			
*2		N8407	643	843	641	.06				
*2		N8607	643	843	845	645	.06			
		N9607	653	853	855	655	BY N200	2	*=3	+
*2		N9807	655	855	857	657	.10	.08		
*2		N10007	657	857	859	659	**			
*2		N10207	659	859	861	661	.30	.14 .20	.00	
*2		N10407	661	861	863	663	**			
*2		N9009	849	1049	847	.06				
*2		N9209	849	1049	1051	851	.06			
		N9609	853	1053	1055	855	BY N200	2	*=3	+
*2		N9809	855	1055	1057	857	.10	.08		
*2		N10009	857	1057	1059	859	**			
*2		N10209	859	1059	1061	861	.30	.14 .20	.00	
*2		N10409	861	1061	1063	863	**			
*2		N9411	1053	1253	1051	.30	.14 .22	.12		
*2		N9611	1053	1253	1254	1054	.30	.14 .22	.12	+
		N10511	1062	1262	1263	1063	BY N100	1	*=3	
*2		N9713	1255	1455	1254	.30	.14 .22	.12		
*2		N9813	1255	1455	1456	1256	.30	.14 .22	.12	+
		N10513	1262	1462	1463	1263	BY N100	1	*=3	

*2		N9915	1457	1657	1456		.08						
*2		N10015	1457	1657	1658	1458	.08						
		N10515	1462	1662	1663	1463		BY	N100	1	TO	*	
		N10117	1659	1859	1658		.08						
*2		N10217	1659	1859	1860	1660	.08				TO	*	
		N10517	1662	1862	1863	1663		BY	N100	1	TO	*	
*/													
*/ WING IN-BOCY COVERS													
*/													
	COVER	M5	N7001	27	227	229	29	.30				TO	*
			N8601	43	243	245	45		BY	N200	2	TO	*
*2			N8801	45	245	247	47	.60				TO	*
			N9601	53	253	255	55		BY	N200	2	TO	*
*2			N9801	55	255	257	57	.70					
*2			N10001	57	257	259	59	.70					
*2			N10201	59	259	261	61	1.30	.70	1.10	.00		
*2			N10401	61	261	263	63		**				
*/													
*/ WING FIN SPARS													
*/													
	SPAR	M5	N11001	2056	2256		P1						
*2			N11003	2256	2456		*						
*2			N11201	2058	2258		*						
*2			N11203	2258	2458		*						
*2			N11501	2061	2261		*						
*2			N11503	2261	2461		*						
*2			N11701	2063	2263		*						
*2			N11703	2263	2463		*						
*/													
*/ WING FIN RIBS													
*/													
	SPAR	M5	N12001	2256	2258		P1						
*2			N12003	2258	2261		*						
*2			N12005	2261	2263		*						
*2			N12201	2456	2458		*						
*2			N12203	2458	2461		*						
*2			N12205	2461	2463		*						
*/													
*/ WING FIN COVERS													
*/													
	COVER	M5	N13001	2056	2256	2258	2058	.05					
*2			N13003	2058	2258	2261	2061	*					
*2			N13005	2061	2261	2263	2063	*					
*2			N13201	2256	2456	2458	2258	*					
*2			N13203	2258	2458	2461	2261	*					
*2			N13205	2261	2461	2463	2263	*					
*/													
*/ WING FIN ATTACHMENT BEAMS													
*/													
	BEAM	Z5	N20001	1456	2056	1463	P2						
*2			N20003	1458	2058	1463	*						
*2			N20005	1461	2061	1463	*						
*2			N20007	1463	2063	1461	*						
*2			N21001	1456	1456		P3						
*2			N21003	1458	1461		*						
*2			N21005	1461	1463		*						
*/													
*/ WING TRAILING EDGE CONTROL SURFACE RIBS													
*/													
	SPAR	M5	N101	263	3003		P4						
**2	0	0	2	200	100		0						
*2			N102	3003	3005		*						
**2	0	0	2	100	100		0						
*2			N107	1263	3305		*						
**3	0	0	1	200	100		*						
*/													
*/ WING TRAILING EDGE CONTROL SURFACE COVERS													
*/													
	COVER	M5	N151	263	463	3103	3003	.10					
*2			N153	463	663	3203	3103	*					
*2			N152	3003	3103	3105	3005	*					
*2			N154	3103	3203	3205	3105	*					
*2			N155	1263	1463	3405	3305	*					
**2	0	0	1	200	200	100	100	*					

```

*/
*/ HORIZONTAL TAIL SPARS
*/
    SPAR  M5  N14003  279  479      .10  1.2
    *2      N14005  479  679      **
    *2      N14103  281  481      .05  1.8
    *2      N14105  481  681      **
    *2      N14203  283  483      .05  1.6
    *2      N14205  483  683      **
    *2      N14303  285  485      .20  2.6
    *2      N14305  485  685      **

*/
*/ HORIZONTAL TAIL RIBS
*/
    SPAR  M5  N14401  279  281      .15  2.0 TO N14405  283  285      +
    *2      N14501  479  481      .10  1.2 TO N14505  483  485      +
    *2      N14601  679  681      .10  1.2 TO N14605  683  685      +
    BY N2      2      2
    BY N2      2      2

*/
*/ HORIZONTAL TAIL IN-BODY SPARS
*/
    SPAR  M5  N14001   79  279      .50  6.0
    *2      N14101   81  281      .25  9.0
    *2      N14201   83  283      .25  9.0
    *2      N14301   85  285      1.00 13.0

*/
*/ HORIZONTAL TAIL COVERS
*/
    COVER  M5  N15003  279  479  481  281  .16
    **2    0    0      200      2  **3  0.
    COVER  M5  N15005  479  679  681  481  .07
    **2    0    0      200      2  **3  0.

*/
*/ HORIZONTAL TAIL IN-BODY COVERS
*/
    COVER  M5  N15001   79  279  281   81  .80
    N15401   83  283  285   85      BY N200      2      TO **3      +

*/
*/ BODY BEAMS
*/
    BEAM  M5  N1001     1    3    5.    0.  **3  16000.  10.  0.  **3  30000.
    **30  0    0        2    2    2    5.  **4  14000.   5.  **4  14000.
    *2      N1063     63   65  160.  **4  450000. 148.  **4  416000.
    **12  0    0        2    2    2 -12.  **4 -34000. -12.  **4 -34000.

*/
*/ BEAMS AT 455 RIB TO PICK UP DISCONTINUED SPARS
*/
    BEAM  M5  N30002  1053 1054      P5
    **4    0    0        2    2    2      *
    BEAM  M5  N30011  1063 1062      P5
    **4    0    0       -2   -2   -2      *

    END ELEMENT DATA
    END STIFFNESS DATA
    BEGIN MASS DATA
    BEGIN MASS ELEMENT DATA
    BEAM  1456 2056 1463 .1 .1 **3
    BEAM  1458 2058 1463 **
    BEAM  1461 2061 1463 **
    BEAM  1463 2063 1461 **
    END MASS ELEMENT DATA
    END MASS DATA
    BEGIN BC DATA
    STAGE 1      *(FOR VIBRATION ANALYSIS)
    ORDER RETAIN BY INTERNALID
    SUPPORT ASYM IN SURFACE 2
    SUPPORT TX FOR 89
    RETAIN TZ FOR 1 7 13 19 27 45 55 63 67 73 79 85 89
    RETAIN TZ FOR 227 237 245 255 435 441 445 451 +55
    RETAIN TZ FOR 641 645 649 655 659 847 851 855 859 863 1051 **3+4
    RETAIN TZ FOR 1254 1259 1456 1459 1658 1661 1859 1860 1861

```


RETAIN TZ FOR 3003 3005 3103 3105 3203 3205
 RETAIN TZ FOR 3305 3405 3505 3605
 RETAIN TZ FOR 279 479 679
 RETAIN TY FOR 2058 2061 2258 2261 2458 2461
 RETAIN TZ RX RY FOR 263 463 663 1263 1463 1663 1863 285 485 685 83 +
 283 483 683

STAGE 2 *(FOR STRESS ANALYSIS)
 SUPPORT ASYM IN SURFACE 2
 SUPPORT TX TZ RY FOR 89

END BC DATA

BEGIN LOAD DATA

SET 1 STAGE 2

LOAD CASE ID SYMM **SYMMETRIC AIRLOADS*

BEGIN NODAL LOAD DATA

ORDER FZ

CASE SYMM

3	-2275.
9	-6110.
15	-4970.
23	-3255.
31	-245.
39	-5400.
45	-380.
53	-3830.
61	140.
67	-165.
75	-6365.
83	-3495.
87	-3160.
85	-150.
89	-150.

ORDER FZ FY

2056	-125.	1220.
2456	-100.	1360.
2458	-100.	-410.
2058	-125.	955.
2061	-125.	1075.
2461	-100.	7665.
2463	-100.	-4960.
2063	-125.	-660.

ORDER FZ

431	13475.
231	-8500.
637	8030.
237	-7750.
245	-11770.
655	-4640.
255	-5330.
663	1565.
263	5445.
843	36405.
645	-20790.
1051	21130.
649	3435.
1055	3365.
1063	1435.
1456	13820.
1459	21815.
1463	6155.
1860	860.
1861	14355.
1863	2762.
659	-450.
1059	-8710.
1461	-10655.
1862	-5150.
279	-5060.
679	-4040.
681	-7375.
281	-5415.
283	-1620.

```

683      -865.
685      -1725.
285      -3425.
END NODAL LOAD DATA
END LOAD DATA
BEGIN SUBSET DEFINITION
SUBSETS OF STIFFNESS SET 1
*/ SUBSETS FOR GEOMETRY PLOTS
E1 = ALL
N1 = ALL
*/ SUBSETS FOR BODY PROPERTY PLOTS
N2 = 1 TO 89
E2 = BEAMS IN N2
*/ SUBSETS FOR STRESS CONTOUR PLOTS
N10 = TUBE 227 1860 1863 **8-200 DIRECTION 0 0 1
N11 = SLAB 2 0.
N12 = N10 I N11
E12 = COVERS IN N12
ON2 = 227 435 641 847 1051 1254 1456 1658 1859 **4+1
      **8-200 **17-2
*/ SUBSET FOR VMODE PLOT
ON1 = 1 7 13 19 27 227 237 245 255 263 3003 3005
      3105 3103 463 455 451 445 441 435 641 645 649 655
      659 663 3203 3205 3105 3103 463 663 863 859 855 851
      847 1051 1055 1059 1063 1263 1259 1254 1456 1459 1463 3405
      3305 1263 1463 1663 1661 1658 1859 1860 1861 1863 3605 3505
      3405 3505 1663 1863 1861 1860 1859 1658 1456 1254 1051 847
      641 435 227 27 45 55 63 263 463 663 863 1063
      1263 1463 1459 2058 2258 2458 2461 2261 2258 2261 2061 1463
      1263 1063 663 663 463 263 63 67 73 79 83 85
      89 85 285 485 685 583 679 479 279 79 83 85
      285 283 279 479 483 485
END SUBSET DEFINITION
END PROBLEM DATA

```

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**Table 203-1. Natural Frequencies
for SST Aircraft**

Mode No.	Frequency (Hertz)
1	0.
2	0.
3	2.754
4	3.627
5	5.428
6	7.595
7	9.444
8	10.768

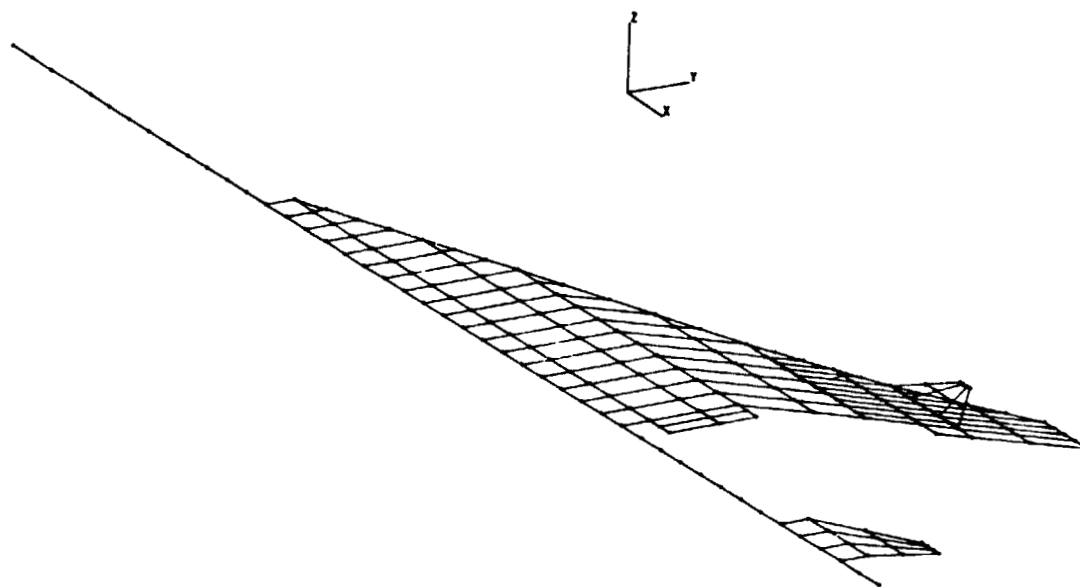
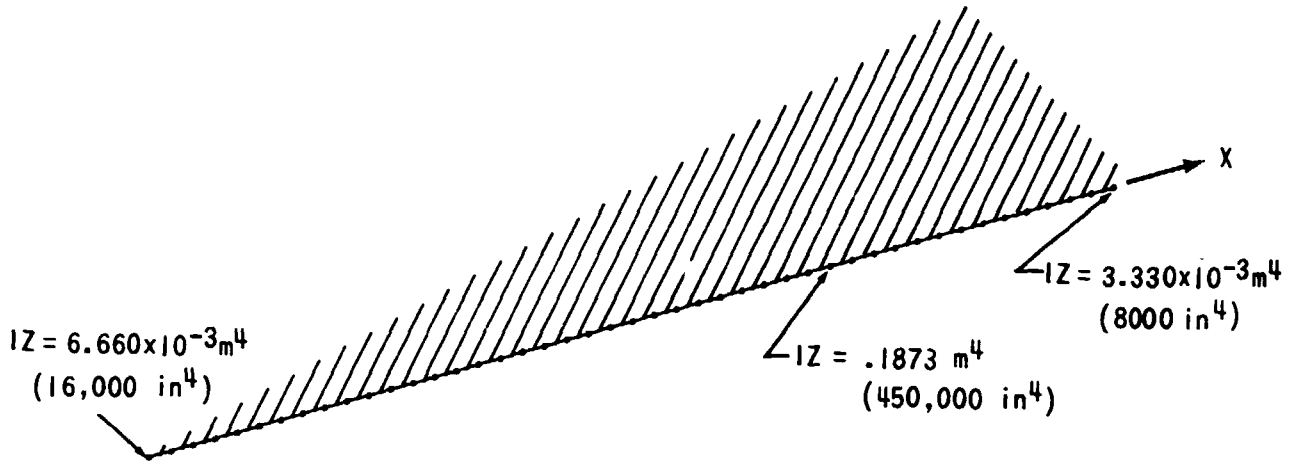


Figure 203-1. SST Structural Model

PROPERTY BMAL(1)



PROPERTY BMIZ(1)

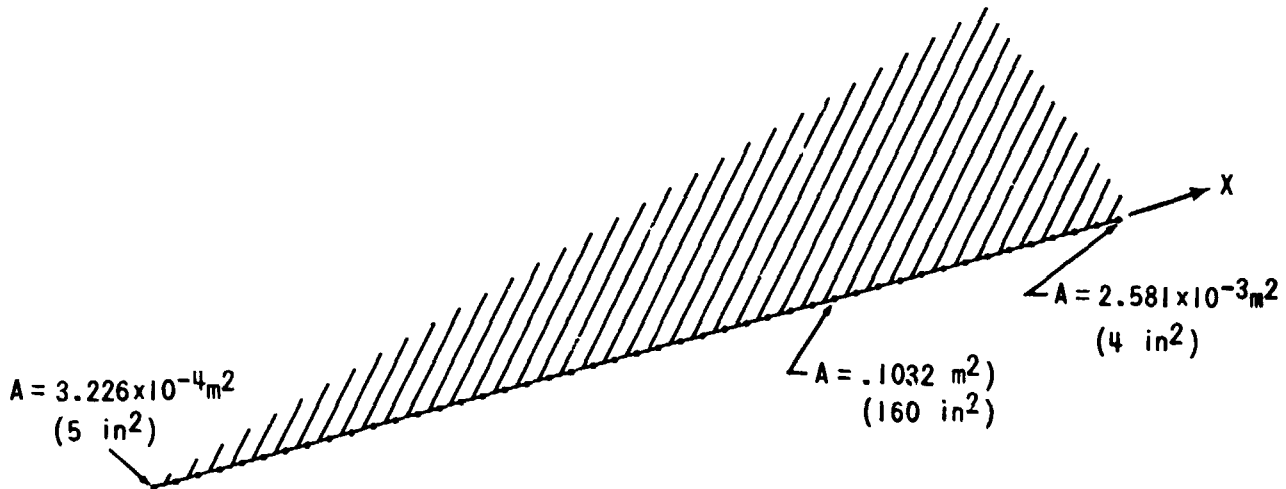


Figure 203-2. SST Body Stiffness Properties

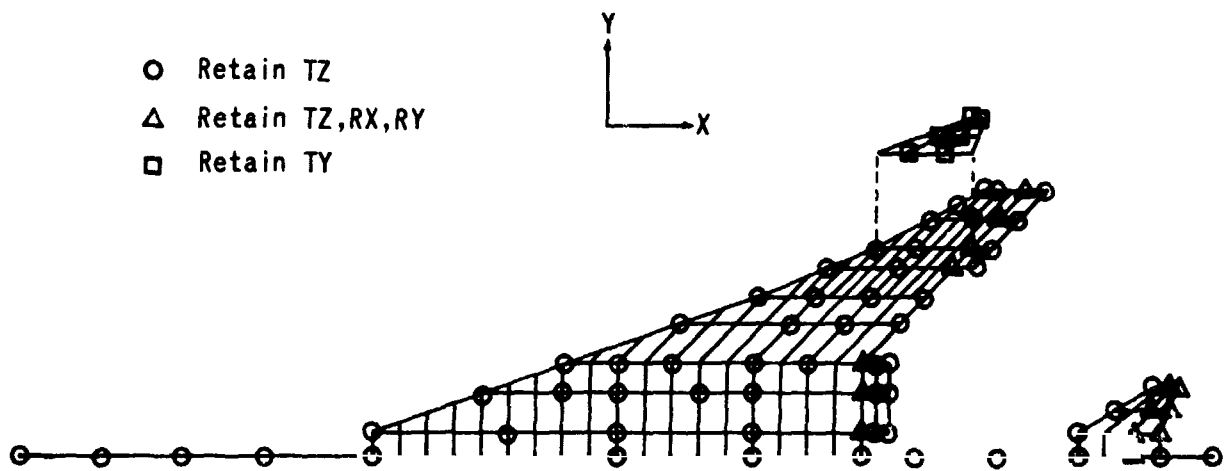
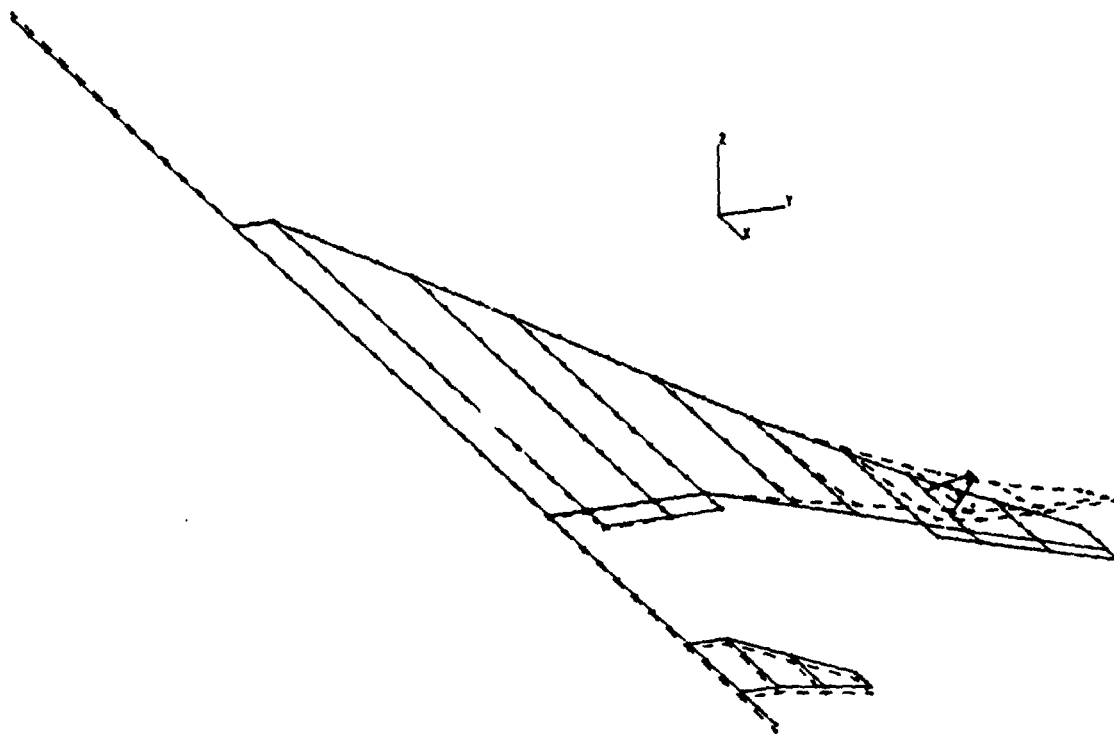


Figure 203-3. Freedoms Retained in SST Vibration Analysis



FREQUENCY= 2.754

Figure 203-4. Third Mode Shape, SST

204. SUBSTRUCTURED STRESS AND VIBRATION ANALYSES OF AN SST AIRCRAFT (DECK 1)

204.1 DESCRIPTION OF ANALYSES

The SST aircraft described in section 203 is analyzed using substructures. The same vibration and stress analyses are performed. The half-model of section 203 is modelled as three substructures: body, wing and horizontal tail as shown in figure 204-1. These three substructures are interacted in a single step to obtain the highest level substructure (substructure 4).

204.2 RESULTS

Natural frequencies, mode shapes, displacements and stresses obtained in this problem are identical to those obtained in section 203.

204.3 LISTING OF CONTROL PROGRAM AND DATA

```

C BEGIN CONTROL PROGRAM DEM001
C PROBLEM 10(DEM001 - SUBSTRUCTURED STRESS/VIBRATION ANALYSES)
C
C PURPOSE      THE PRIMARY CAPABILITIES DEMONSTRATED BY THIS
C              DECK ARE
C              1. SUBSTRUCTURED STRESS ANALYSIS
C              2. SUBSTRUCTURED VIBRATION ANALYSIS
C              3. EXPLODED PLOT OF MODEL
C
C AUTHOR       R.A. SAMUEL
C
C CORE         150K (OCTAL)
C
C METHOD        STRESS AND VIBRATION ANALYSES ARE PERFORMED ON A
C              SUBSTRUCTURED HALF-AIRPLANE MODEL OF AN SST.
C              DISPLACEMENTS, STRESSES, NATURAL FREQUENCIES AND
C              MODE SHAPES ARE COMPARED WITH RESULTS OF A
C              NON-SUBSTRUCTURED MODEL.
C
C USER COMMON(1)
C
C READ INPUT
C DO 10 I = 1,3
C PRINT INPUT(STIFFNESS,SET=I)
C PRINT INPUT (NODAL,SET=I)
C PRINT INPUT(MASS,SET=I)
10 CONTINUE
C EXECUTE EXTRACT(EXNAME=SS1,LSUB=KGRID,ESUB=E1,NSUB=N1)
C EXECUTE EXTRACT(EXNAME=SS2,LSUB=KGRID,KSET=2,ESUB=E1,NSUB=N1)
C EXECUTE EXTRACT(EXNAME=SS3,LSUB=KGRID,KSET=3,ESUB=E1,NSUB=N1)
C EXECUTE GRAPHICS(IGNAME=GEOMETRY,OFFLINE=CALCOMP,TYPE=(ORTH,
X          POINT),SIZE=(20.,20.),EXPLODE,RZ=30.,RY=20.,
X          RX=0.,EXNAME=SS1,TY=100.,EXNAME=(SS2,SS3))
C
C VIBRATION ANALYSIS
C
C DO 20 I = 1,4
C PRINT INPUT(INTERACT,SS=I,NODES,RETAINS,CONN,BC)
20 CONTINUE
C DO 30 I = 1,3
C EXECUTE STIFFNESS(SET=I)
C EXECUTE MASS(SET=I,OPTION=4,CONDITION=1)
30 CONTINUE
C PERFORM SS-MERGE(STIF,MASS,SS=1 TO 3)
C PERFORM SS-RECU(STIF,MASS,SS=1 TO 3)
C PERFORM SS-MERGE(STIF,MASS,SS=4)
C EXECUTE MASS(SET=4,OPTION=4,CONDITION=1)
C PRINT OUTPUT(MASS,SET=4,SUMMARY)
C PERFORM SS-VSOL(SS=4)

```

EXECUTE VIBRATION (STIF=KRED004,MASS=MRED004,NFREQS=8,SET=4)
PRINT OUTPUT (VIBRATION)
PURGE FILES(MERGRNF,MULTRNF,VIBRRNF,MASSRNF,CHOLRNF)

C
C
C

STRESS ANALYSIS

DO 40 I = 11,14
PRINT INPUT(INTERACT,SS=1,NODES,RETAINS,CONN,BC,LOADS)
40 CONTINUE
EXECUTE LOACS(SS=(11,12,13))
PERFORM SS-MERGE(STIF,LOADS,SS=11 TO 13)
PERFORM SS-REDU(STIF,LOADS,SS=11 TO 13)
PERFORM SS-MERGE(STIF,LOADS,SS=14)
PERFORM SS-SSOL(SS=14)
PERFORM SS-PART(SS=14)
PERFORM SS-BACK(SS=11 TO 13)
DO 45 I = 11,13
EXECUTE STRESS(SS=I)
45 CONTINUE
DO 50 I = 11,13
PRINT OUTPUT(DISP,SS=I)
PRINT OUTPUT(STRESS,SS=I)
PRINT OUTPUT(LOADS,SS=I)
PRINT OUTPUT(REACTIONS,SS=I)
50 CONTINUE
END CONTROL PROGRAM

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```

*/ MODE2 /
BEGIN NODAL DATA
SET 1      *(BODY)
      1      20.      0.  0.      TO      25      980.      0.  0.      BY      2
      27      1060.      0.  0.      30.0 TO      45      1780.      0.  0.      42.5 BY      2
**+1 200      0.      65.  0.      0      0      200      0.      65.      **
      45      TO      55      2180.      0.  0.      31.0 BY      2
**+1 200      0      200      0.      65.      **
      55      TO      63      2500.      0.  0.      13.5 BY      2
**+1 200      0      200      0.      65.      **
      65      2580.      0.  0.      TO      77      3060.      0.  0.      BY      2
      79      3140.      0.  0.      3.0
**+1 200      0.      65.      **
      81      3220.      0.  0.      6.5
**+1 200      0.      65.      **
      83      3300.      0.  0.      7.0
**+1 200      0.      65.      **
      85      3380.      0.  0.      2.0
**+1 200      0.      65.      **
      .87      3460.      0.  0.
      89      3540.      0.  0.
END NODAL DATA
BEGIN STIFFNESS DATA
BEGIN ELEMENT DATA
*/
*/ BODY BEAMS
*/
      BEAM      M5      N1001      1      3      5.      0.      **3      16000.      10.  0.      **3      30000.
**+30 0      0      2      2      2      5.      **4      14000.      5.      **4      14000.
      *2      N1063      63      65      160.      **4      450000.      148.      **4      416000.
**+12 0      0      2      2      2      -12.      **4      -34000.      -12.      **4      -34000.
*/
*/ WING IN-BODY SPARS
*/
      SPAR      M5      N2001      27      227      1.00      10.      TO      N3601      43      243      +
      BY      N200      2      2
      *2      N3801      45      245      1.50      10.      TO      N4601      53      253      +
      BY      N200      2      2
      *2      N4801      55      255      3.00      60.
      *2      N5001      57      257      1.20      60.      TO      N5401      61      261      +
      BY      N200      2      2
      *2      N5601      63      263      2.00      60.
*/
*/ S.O.B. RIB - WING
*/
      SPAR      M5      N6001      227      229      .25      4.      TO      N6035      261      263      +
      BY      N2      2      2
*/
*/ WING IN-BODY COVERS
*/
      COVER      M5      N7001      27      227      229      29      .30      TO      +
      N8601      43      243      245      45      BY      N200      2      **3
      *2      N8801      45      245      247      47      .60      TO      +
      N9601      53      253      255      55      BY      N200      2      **3
      *2      N9801      55      255      257      57      .70
      *2      N10001      57      257      259      59      .70
      *2      N10201      59      259      261      61      1.30      .70      1.10      .00
      *2      N10401      61      261      263      63      **
*/
*/ S.O.B. RIB - HORIZONTAL TAIL
*/
      SPAR      M5      N14401      279      281      .15      2.0      TO      N14405      283      285      +
      BY      N2      2      2
*/
*/ HORIZONTAL TAIL IN-BODY SPARS
*/
      SPAR      M5      N14001      79      279      .50      6.0
      *2      N14101      81      281      .25      9.0
      *2      N14201      83      283      .25      8.0
      *2      N14301      85      285      1.00      13.0
*/

```

*/ HORIZONTAL TAIL IN-BODY COVERS

*/

COVER M5 N15001 79 279 281 81 .80 TO
N15401 83 283 285 85 3Y N200 2 **3

END ELEMENT DATA

END STIFFNESS DATA

BEGIN NODAL DATA

SET 2 *(WING)

327	1060.	65.	0.	30.0	TO	345	1780.	65.	0.	42.5	BY	2
345					TO	355	2180.	65.	0.	31.0	BY	2
355					TO	363	2500.	65.	0.	13.5	BY	2
427	1060.	65.	0.	30.0	TO	435	1380.	180.	0.	17.5	BY	2
435					TO	445	1780.	180.	0.	27.5	BY	2
445					TO	455	2180.	180.	0.	25.0	BY	2
455					TO	465	2500.	180.	0.	13.0	BY	2
635	1380.	180.	0.	17.5	TO	641	1620.	265.	0.	10.0	BY	2
641					TO	655	2180.	265.	0.	22.5	BY	2
655					TO	663	2500.	265.	0.	12.5	BY	2
841	1620.	265.	0.	10.0	TO	847	1971.	380.	0.	9.0	BY	2
847					TO	855	2291.	380.	0.	17.0	BY	2
855					TO	863	2611.	380.	0.	10.0	BY	2
1047	1971.	380.	0.	9.0	TO	1051	2205.	455.	0.	8.5	BY	2
1051					TO	1059	2525.	455.	0.	15.0		
1059					TO	1063	2685.	455.	0.	8.0		
1251	2205.	455.	0.	8.5	TO	1254	2409.	538.	0.	6.5		
1254					TO	1259	2609.	538.	0.	11.0		
1259					TO	1263	2769.	538.	0.	5.5		
1454	2409.	538.	0.	6.5	TO	1456	2545.	594.	0.	5.0		
1456					TO	1459	2665.	594.	0.	7.5		
1459					TO	1463	2825.	594.	0.	3.5		
1656	2545.	594.	0.	5.0	TO	1658	2710.	680.	0.	3.0		
1658					TO	1663	2910.	680.	0.	3.0		
1858	2710.	680.	0.	3.0	TO	1860	2875.	765.	0.	1.5		
1860					TO	1863	2995.	765.	0.	2.5		

*/

*/ WING TRAILING EDGE NODES

*/

3001	2500.	65.	0.	13.5	TO	3005	2580.	65.	0.	1.0	BY	2
3101	2500.	130.	0.	13.0	TO	3105	2580.	180.	0.	1.0	**	
3201	2500.	265.	0.	12.5	TO	3205	2580.	265.	0.	1.0	**	
3305	2830.	538.	0.	1.0	TO	3605	3045.	765.	0.	1.0		

BY 100 OF 56. 86. 85.

*/

*/ WING FIN NODES

*/

REC WINGFIN 0. 594. 0., 1. 594. 0., 0. -1. 0.

2056	2545.	.1	0.	3.5	TO	2456	2830.	100.	0.	2.5	BY	200
2058	2625.	.1	0.	3.5	TO	2458	2942.	100.	0.	3.0	**	
2061	2745.	.1	0.	4.0	TO	2461	2859.	100.	0.	3.0	**	
2063	2825.	.1	0.	4.0	TO	2463	2870.	100.	0.	3.0	**	

END NODAL DATA

BEGIN STIFFNESS DATA

SET 2 *(WING)

BEGIN PROPERTY DATA

P1	.05	1.	*(WING FIN SPARS AND RIBS)										
P2	2.	0.	0.	.2	.2	.2	*(WING FIN ATTACHMENT BEAMS - TYPE 1)						
P3	10.	0.	0.	100.	100.	100.	*(WING FIN ATTACHMENT BEAMS - TYPE 2)						
P4	.15	.50	*(CONTROL SURFACE RIBS)										
P5	0.	**2	100.	100.	0.	10.	*(BEAMS AT 455 RIB TO PICK UP SPARS)						

END PROPERTY DATA

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BEGIN ELEMENT DATA

*/

*/ WING FRONT SPAR

*/

SPAR	MS	N2003	327	429	.12	2.					
*2		N2205	429	431	.12	2.	TO	N2605	433	435	+
							BY	N200	2	2	
*2		N2805	435	637	.12	2.					
*2		N3007	637	639	.12	2.	TO	N3207	639	641	+
							BY	N200	2	2	
*2		N3407	641	843	.12	2.					
*2		N3609	843	845	.12	2.	TO	N3809	845	847	+
							BY	N200	2	2	
*2		N4009	847	1049	.12	2.					
*2		N4211	1049	1051		**					
*2		N4411	1051	1253		**					
*2		N4613	1253	1254		**					
*2		N4713	1254	1455		**					
*2		N4815	1455	1456		**					
*2		N4915	1456	1657		**					
*2		N5017	1657	1658		**					
*2		N5117	1658	1859		**					
*2		N5219	1859	1860		**					

*/

*/ WING REAR SPAR

*/

SPAR	MS	N5603	363	463	.40	12.					
*2		N5605	463	663	.40	12.					
*2		N5607	663	863	.34	12.					
*2		N5609	863	1063	.34	12.					
*2		N5611	1063	1263	.30	8.					
*2		N5613	1263	1463	.30	8.					
*2		N5615	1463	1663	.30	4.					
*2		N5617	1663	1863	.30	4.					

*/

*/ WING INTERMEDIATE SPARS

*/

SPAR	MS	N2203	329	429	.20	2.	TO	N3603	343	443	+
							BY	N200	2	2	
*2		N3803	345	445	.36	2.					
*2		N4803	355	455	.60	12.					
*2		N5003	357	457	.24	12.	TO	N5403	361	461	+
							BY	N200	2	2	
*2		N3005	437	637	.20	2.	TO	N3605	443	643	+
							BY	N200	2	2	
*2		N3805	445	645	.36	2.					
*2		N4005	447	647	.20	4.	TO	N4605	453	653	+
							BY	N200	2	2	
*2		N4805	455	655	.60	12.					
*2		N5005	457	657	.24	12.	TO	N5405	461	661	+
							BY	N200	2	2	
*2		N3607	643	843	.20	2.	TO	N3807	645	845	+
							BY	N200	2	2	
*2		N4007	647	847	.20	4.	TO	N4607	653	853	+
							BY	N200	2	2	
*2		N4807	655	855	.20	8.					
*2		N5007	657	857	.20	10.	TO	N5407	661	861	+
							BY	N200	2	2	
*2		N4209	849	1049	.20	4.	TO	N4609	853	1053	+
							BY	N200	2	2	
*2		N4809	855	1055	.20	8.					
*2		N5009	857	1057	.20	10.	TO	N5409	861	1061	+
							BY	N200	2	2	
*2		N4611	1053	1253	.12	4.	TO	N4811	1055	1255	+
							BY	N100	1	1	
*2		N4911	1056	1256	.06	4.	TO	N5511	1062	1262	+
							BY	N100	1	1	
*2		N4813	1255	1455	.12	4.					
*2		N4913	1256	1456	.06	4.	TO	N5513	1262	1462	+
							BY	N100	1	1	
*2		N5015	1457	1657	.06	2.	TO	N5515	1462	1662	+
							BY	N100	1	1	
*2		N5217	1659	1859	.06	2.	TO	N5517	1662	1862	+
							BY	N100	1	1	

```

*/
*/ WING RIBS
*/
    SPAR      N6109      435  437      .30  4.  TO N6135      461  463      +
                      BY N2
    *2        N6215      641  643      .20  3.  TO N6235      661  663      +
                      BY N2
    *2        N6425      1051 1053      .20  4.
    *2        N6425      1053 1054      .20  4.  TO N6435      1062 1063
    *2        N6629      1456 1457      .12  2.  TO N6635      1462 1463
    *2        N6833      1860 1861      .30  1.4 TO N6835      1862 1863

*/
*/ BEAMS AT 455 RIB TO PICK UP DISCONTINUED SPARS
*/
    BEAM      M5      N30002      1053 1054      P5
    **4      0      0      2      2      2      *
    BEAM      M5      N30011      1063 1062      P5
    **4      0      0      -2      -2      -2      *

*/
*/ WING COVERS
*/
    COVER      M5      N7003      329  429  327      .06
    *2          N7203      329  429  431  331      .06
                      N8603      343  443  445  345      BY N200      2      **3      TO      +
    *2          N8803      345  445  447  347      .12      .00
                      N9603      353  453  455  355      BY N200      2      **3      TO      +
    *2          N9803      355  455  457  357      .10      .14
    *2          N10003     357  457  459  359      **
    *2          N10203     359  459  461  361      .26      .14 .22 .00
    *2          N10403     361  461  463  363      **
    *2          N7805      437  637  435      .06
    *2          N8005      437  637  639  439      .06
                      N9605      453  653  655  455      BY N200      2      **3      TO      +
    *2          N9805      455  655  657  457      .10      .14
    *2          N10005     457  657  659  459      **
    *2          N10205     459  659  661  461      .26      .14 .22 .00
    *2          N10405     461  661  663  463      **
    *2          N8407      643  843  641      .06
    *2          N8607      643  843  845  645      .06
                      N9607      653  853  855  655      BY N200      2      **3      TO      +
    *2          N9807      655  855  857  657      .10      .08
    *2          N10007     657  857  859  659      **
    *2          N10207     659  859  861  661      .30      .14 .20 .00
    *2          N10407     661  861  863  663      **
    *2          N9009      849  1049  847      .06
    *2          N9209      849  1049  1051  851      .06
                      N9609      853  1053  1055  855      BY N200      2      **3      TO      +
    *2          N9809      855  1055  1057  857      .10      .08
    *2          N10009     857  1057  1059  859      **
    *2          N10209     859  1059  1061  861      .30      .14 .20 .00
    *2          N10409     861  1061  1063  863      **
    *2          N9411      1053 1253 1051      .30      .14 .22 .12
    *2          N9611      1053 1253 1254 1054      .30      .14 .22 .12
                      N10511     1062 1262 1263 1063      BY N100      1      **3      TO      +
    *2          N9713      1255 1455 1254      .30      .14 .22 .12
    *2          N9813      1255 1455 1456 1256      .30      .14 .22 .12
                      N10513     1262 1462 1463 1263      BY N100      1      **3      TO      +
    *2          N9915      1457 1657 1456      .08
    *2          N10015     1457 1657 1658 1458      .08
                      N10515     1462 1662 1663 1463      BY N100      1      **3      TO      +
    *2          N10117     1659 1859 1658      .08
    *2          N10217     1659 1859 1860 1660      .08
                      N10517     1662 1862 1863 1663      BY N100      1      **3      TO      +

*/
*/ WING FIN SPARS
*/
    SPAR      M5      N11001      2056 2256      P1
    *2          N11003     2256 2456      *
    *2          N11201     2058 2258      *
    *2          N11203     2258 2458      *
    *2          N11501     2061 2261      *
    *2          N11503     2262 2461      *
    *2          N11701     2063 2263      *
    *2          N11703     2263 2463      *

```

*/ WING FIN RIBS

```

*/
    SPAR   M5   N12001   2256 2258      P1
      *2      N12003   2258 2261      *
      *2      N12005   2261 2263      *
      *2      N12201   2456 2458      *
      *2      N12203   2458 2461      *
      *2      N12205   2461 2463      *

```

*/ WING FIN COVERS

```

*/
    COVER   M5   N13001   2056 2256 2258 2058   .05
      *2      N13003   2058 2258 2261 2061      *
      *2      N13005   2061 2261 2263 2063      *
      *2      N13201   2256 2456 2458 2258      *
      *2      N13203   2258 2458 2461 2261      *
      *2      N13205   2261 2461 2463 2263      *

```

*/ WING FIN ATTACHMENT BEAMS

```

*/
    BEAM     Z5   N20001   1456 2056 1463   P2
      *2      N20003   1458 2058 1463      *
      *2      N20005   1461 2061 1463      *
      *2      N20007   1463 2063 1461      *
      *2      N21001   1456 1458      P3
      *2      N21003   1458 1461      *
      *2      N21005   1461 1463      *

```

*/ WING TRAILING EDGE CONTROL SURFACE RIBS

```

*/
    SPARF    M5   N101      363 3003      P4
**+1  0      0      2      100 100      0
**+1  0      0      2      200 100      0
      *2      N102      3003 3005      *
**+2  0      0      2      100 100      0
      *2      N107      1263 3305      *
**+3  0      0      1      200 100      *

```

*/ WING TRAILING EDGE CONTROL SURFACE COVERS

```

*/
    COVER     M5   N151      363 463 3103 3003   .10
      *2      N153      463 663 3203 3103      *
      *2      N152      3003 3103 3105 3005      *
      *2      N154      3103 3203 3205 3105      *
      *2      N155      1263 1463 3405 3305      *
**+2  0      0      1      200 200 100 100      *

```

END ELEMENT DATA

END STIFFNESS DATA

BEGIN NODAL DATA

SET 3 *(HORIZONTAL TAIL)

```

379 3140.0 65.0 0. 3.0
479 3252.5 132.5 0. 2.5
679 3365.0 200.0 0. 2.0
381 3220.0 65.0 0. 6.5
+81 3304. 132.5 0. 4.5
681 3388.0 200.0 0. 2.5
383 3300.0 65.0 0. 7.0
483 3356.0 132.5 0. 4.75
683 3412.0 200.0 0. 2.5
385 3380.0 65.0 0. 2.0
485 3407.5 132.5 0. 1.5
685 3435.0 200.0 0. 1.0

```

END NODAL DATA

BEGIN STIFFNESS DATA

SET 3 *(HORIZONTAL TAIL)

BEGIN ELEMENT DATA

*/ HORIZONTAL TAIL SPARS

```

*/
    SPAR   M5   N14003   379 479      .10 1.2
      *2      N14005   479 679      **
      *2      N14103   381 481      .05 1.8
      *2      N14105   481 681      **
      *2      N14203   383 483      .05 1.6

```

```

      *2      N14205      483 683      **
      *2      N14303      385 485      .20 2.6
      *2      N14305      485 685      **

*/
*/ HORIZONTAL TAIL RIBS
*/
      SPAR      N14501      479 481      .10 1.2 TU N14505      483 485      +
                        BY N2      2 2
      *2      N14601      679 681      .10 1.2 TO N14605      683 685      +
                        BY N2      2 2

*/
*/ HORIZONTAL TAIL COVERS
*/
      COVER M5 N15003      379 479 481 381 .16
      **2 0 0 200 2 **3 0.
      COVER M5 N15005      479 679 681 481 .07
      **2 0 0 200 2 **3 0.

END ELEMENT DATA
END STIFFNESS DATA
BEGIN MASS DATA
SET 2
BEGIN MASS ELEMENT DATA
      BEAM 1456 2056 1463 .1 **4
      BEAM 1458 2058 1463 **
      BEAM 1461 2061 1463 **
      BEAM 1463 2063 1461 **
END MASS ELEMENT DATA
END MASS DATA
BEGIN SUBSET DEFINITION
      SUBSETS OF STIFFNESS SET 1
*/
*/ E1 - BODY ELEMENTS
*/
      E1 = ALL
      SUBSETS OF STIFFNESS SET 2
*/
*/ E1 - WING ELEMENTS
*/ E2 - WING FIN ELEMENTS
*/
      E1 = SLAB 2 0.
      E2 = SLAB 2 .1 TO 500.
      SUBSETS OF STIFFNESS SET 3
*/
*/ E1 - HORIZONTAL TAIL ELEMENTS
*/
      E1 = ALL
END SUBSET DEFINITION
BEGIN BC DATA
*/
*/ STAGE 1 FOR VIBRATION ANALYSIS
*/ STAGE 2 FOR STRESS ANALYSIS
*/
SET 1 STAGE 1
      SUPPORT ASYM IN SURFACE 2
      SUPPORT TX FOR 89
      SUPPORT RZ FOR 227 TO 263 BY 2, 279 TO 285 BY 2
      RETAIN TZ FOR 1 7 13 19 27 45 55 63 67 73 79 85 89
      RETAIN TZ RX RY FOR 83
SET 2 STAGE 1
      SUPPORT ALL FOR 427 3001
      SUPPORT RZ FOR 327 TO 363 BY 2
      RETAIN TZ FOR 435 441 445 451 455
      RETAIN TZ FOR 641 645 649 655 659 847 851 855 859 863 1051 1055 1059 1063
      RETAIN TZ FOR 1254 1259 1456 1459 1658 1661 1859 1860 1861
      RETAIN TZ FOR 3003 3005 3103 3105 3203 3205
      RETAIN TZ FOR 3305 3405 3505 3605
      RETAIN TY FOR 2058 2061 2258 2261 2458 2461
      RETAIN TZ RX RY FOR 463 663 1263 1463 1663 1863
SET 3 STAGE 1
      SUPPORT RZ FOR 379 TO 385 BY 2
      RETAIN TZ FOR 479 679
      RETAIN TZ RX RY FOR 483 683 485 685

```



```

SET 1 STAGE 2
  SUPPORT ASYM IN SURFACE 2
  SUPPORT RZ FOR 227 TO 263 BY 2, 279 TO 285 BY 2
  SUPPORT ALL FOR 89
SET 2 STAGE 2
  SUPPORT ALL FOR 427 3001
  SUPPORT RZ FOR 327 TO 363 BY 2
SET 3 STAGE 2
  SUPPORT RZ FOR 379 TO 385 BY 2

```

END 3C DATA

BEGIN LOAD DATA

SET 1 STAGE 2

LOAD CASE ID SYMM **SYMMETRIC AIRLOADS*

BEGIN NODAL LOAD DATA

ORDER FZ

CASE SYMM

3	-2275.
9	-6110.
15	-4970.
23	-3255.
31	-245.
39	-5400.
45	-380.
53	-3830.
61	140.
67	-165.
75	-6365.
83	-3495.
87	-3160.
85	-150.
89	-150.

END NODAL LOAD DATA

SET 2 STAGE 2

LOAD CASE ID SYMM **SYMMETRIC AIRLOADS*

BEGIN NODAL LOAD DATA

ORDER FZ FY

CASE SYMM

2056	-125.	1220.
2456	-100.	1360.
2458	-100.	-410.
2058	-125.	955.
2061	-125.	1075.
2461	-100.	7665.
2463	-100.	-4960.
2063	-125.	-660.

ORDER FZ

431	13475.
331	-8500.
637	8030.
337	-7750.
345	-11770.
655	-4640.
355	-5330.
663	1565.
363	5445.
843	36405.
645	-20790.
1051	21130.
649	3435.
1055	3365.
1063	1435.
1456	13820.
1459	21815.
1463	6155.
1860	860.
1861	14395.
1863	2762.
659	-450.
1059	-8710.
1461	-10695.
1862	-5190.

END NODAL LOAD DATA

```

SET 3 STAGE 2
  LOAD CASE ID SYMM **SYMMETRIC AIRLOADS*
BEGIN NODAL LOAD DATA
  ORDER FZ
  CASE SYMM
    379 -5060.
    679 -4040.
    681 -7375.
    381 -5415.
    383 -1620.
    683 -865.
    685 -1725.
    385 -3425.
  END NODAL LOAD DATA
END LOAD DATA
BEGIN SUBSET DEFINITION
  SUBSETS OF STIFFNESS SET 1
    E1 = ALL
    N1 = ALL
  SUBSETS OF STIFFNESS SET 2
    E1 = ALL
    N1 = ALL
  SUBSETS OF STIFFNESS SET 3
    E1 = ALL
    N1 = ALL
END SUBSET DEFINITION
BEGIN INTERACT DATA
  DEFINE SS 1 AS SET 1 STAGE 1 *(BODY)
  DEFINE SS 2 AS SET 2 STAGE 1 *(WING)
  DEFINE SS 3 AS SET 3 STAGE 1 *(HORIZONTAL TAIL)
  SS 4
    INTERACT 1 2 3
BEGIN BC CHANGES
  SS 4
    REFERENCE SS 1
    RETAIN TZ FOR 227 237 245 255 279
    RETAIN TZ RX RY FOR 263 283 285
  END BC CHANGES
  DEFINE HIGHEST SS 4 AS SET 4
END INTERACT DATA
BEGIN INTERACT DATA
  DEFINE SS 11 AS SET 1 STAGE 2 *(BODY)
  DEFINE SS 12 AS SET 2 STAGE 2 *(WING)
  DEFINE SS 13 AS SET 3 STAGE 2 *(HORIZONTAL TAIL)
  SS 14
    INTERACT 11 12 13
  DEFINE HIGHEST SS 14
END INTERACT DATA
END PROBLEM DATA

```

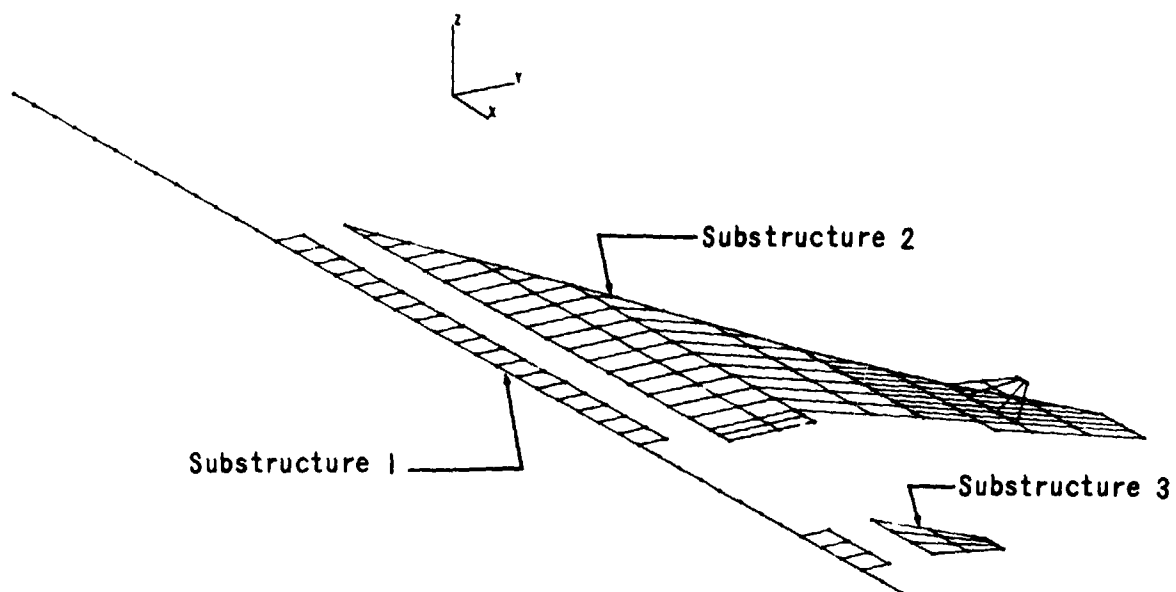


Figure 204-1. Substructured Model of SST

205. VIBRATION ANALYSIS OF THE FIREBEE DRONE (DECK 15)

205.1 DESCRIPTION OF ANALYSIS

An analysis is performed to determine symmetrical modes of vibration of the FIREBEE Drone. Because of structural symmetry, only one half of the Drone is modelled. The wing model is based upon the supercritical wing (ARW-1); the fuselage and horizontal tail models are based upon the data reported in reference 205-1.

The outboard wing is modelled using SPLATE and ROD elements. The wing center section is modelled using GPLATE and BEAM elements and the fuselage and horizontal tail are modelled using BEAM elements. The total structural model is shown in figure 205-1. More detailed views of the model are presented in figures 205-2 through 205-6.

The number of degrees of freedom retained in the analysis is 107. Z-direction translations are retained at outboard wing upper surface, fuselage and horizontal tail nodes. Rotations about the Y axis are retained at fuselage and horizontal tail nodes; rotations about the X axis are retained at horizontal tail nodes. Symmetry is imposed on the plane $Y=0$. Rigid body translation in the X-direction is restrained near the center of the fuselage.

The reduced mass matrix is a nondiagonal matrix produced directly by the Mass Processor. The wing mass is obtained exclusively from the stiffness finite elements; the fuselage and horizontal tail mass exclusively from concentrated masses.

205.2 RESULTS

The natural frequencies of the first ten modes are presented in table 205-1. The first two modes are rigid body modes. The mode shapes for modes 4 and 6 are shown in figures 205-7 and 205-8.

The third mode shape closely resembles the first mode shape of a cantilever wing. The frequency and mode shape for this mode are similar to the results obtained from a NASTRAN analysis of a cantilever wing.

Modes 4 and 5 are the first two fuselage bending modes and mode 8 is the first horizontal tail bending mode. The results for these three modes compare favorably with those reported in reference 205-1.

CCCCCCCCCCCC

PURPOSE	THE PRINCIPAL CAPABILITIES DEMONSTRATED BY THIS DECK ARE
	1. GENERATION OF NON-DIAGONAL MASS MATRIX BY MASS PROCESSOR
	2. VIBRATION ANALYSIS
	3. PLOTS OF VIBRATION MODE SHAPES

CORE 150 K (OCTAL)

END CONTROL PROGRAM

BEGIN MATERIAL DATA /

M51 .05 /

0 .228E+07 0. .695E+06 0. /

M52 .1 /

0 .10500000E+08 .31250000E+00 .40000000E+07 0. /

M53 0. /

0 .228E+07 0. .695E+06 0. /

M54 0. /

0 .10500000E+08 .31250000E+00 .40000000E+07 0. /

M55 .285 /

0 .29000000E+08 .31818182E+00 .11000000E+08 0. /

END MATERIAL DATA /

BEGIN NOCAL DATA /

REC WING -1.01 0. 0. 1. 0. 0. -1.01 0. 1. /

1	310.6360000	85.5000000	1.4070000
2	310.6360000	85.5000000	.9100000
3	311.8520000	85.5000000	1.6630000
4	311.8520000	85.5000000	.8630000
5	313.8790000	85.5000000	1.9310000
6	313.8790000	85.5000000	.9790000
7	316.2430000	85.5000000	2.1750000
8	316.2430000	85.5000000	1.2410000
9	318.6080000	85.5000000	2.3940000
10	318.6080000	85.5000000	1.5980000
11	321.9860000	85.5000000	2.5950000
12	321.9860000	85.5000000	2.2870000
13	323.8740000	85.5000000	2.4240000
21	304.5500000	79.2500000	1.3600000
22	304.5500000	79.2500000	.7860000
23	305.9200000	79.2500000	1.6310000
24	305.9200000	79.2500000	.7440000
25	308.2000000	79.2500000	1.9300000
26	308.2000000	79.2500000	.8720000
27	310.8700000	79.2500000	2.2110000
28	310.8700000	79.2500000	1.1400000
29	313.5300000	79.2500000	2.4560000
30	313.5300000	79.2500000	1.5280000
31	317.3400000	79.2500000	2.6550000
32	317.3400000	79.2500000	2.3210000
33	319.2480000	79.2500000	2.4395000
41	297.8290000	72.3490000	1.3470000
42	297.8290000	72.3490000	.6630000
43	298.6570000	71.5980000	1.6320000
44	298.6570000	71.5980000	.6170000
45	300.0810000	70.3040000	1.9740000
46	300.0810000	70.3040000	.7250000
47	301.8190000	68.7260000	2.3030000
48	301.8190000	68.7260000	.9750000
49	303.6430000	67.0700000	2.5820000
50	303.6430000	67.0700000	1.3870000
51	306.4150000	64.5530000	2.7630000
52	306.4150000	64.5530000	2.3580000
53	307.8790000	63.2230000	2.4530000
61	285.4500000	63.7470000	1.3680000
62	285.4500000	63.7470000	.5720000
63	290.3930000	62.8920000	1.6950000
64	290.3930000	62.8920000	.4990000
65	292.0140000	61.4200000	2.0760000
66	292.0140000	61.4200000	.5870000
67	293.9920000	59.6240000	2.4190000
68	293.9920000	59.6240000	.8340000
69	296.0670000	57.7400000	2.6840000
70	296.0670000	57.7400000	1.2720000
71	299.2210000	54.8760000	2.8070000
72	299.2210000	54.8760000	2.3480000
73	300.8870000	53.3630000	2.4410000
81	281.0740000	55.1450000	1.4420000
82	281.0740000	55.1450000	.5280000
83	282.1300000	54.1860000	1.8160000
84	282.1300000	54.1860000	.4080000
85	283.9470000	52.5360000	2.2320000
86	283.9470000	52.5360000	.4560000
87	286.1650000	50.5220000	2.5640000

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88	286.1650000	50.5220000	.6960000	/
89	288.4920000	48.4100000	2.7900000	/
90	288.4920000	48.4100000	1.1530000	/
91	292.0270000	45.1990000	2.8370000	/
92	292.0270000	45.1990000	2.3210000	/
93	293.8960000	43.5030000	2.4230000	/
101	272.6970000	46.5430000	1.5510000	/
102	272.6970000	46.5430000	.5090000	/
103	273.8670000	45.4810000	1.9720000	/
104	273.8670000	45.4810000	.3320000	/
105	275.8800000	43.6520000	2.4100000	/
106	275.8800000	43.6520000	.3290000	/
107	278.3380000	41.4210000	2.7170000	/
108	278.3380000	41.4210000	.5580000	/
109	280.9160000	39.0800000	2.8960000	/
110	280.9160000	39.0800000	1.0340000	/
111	284.8340000	35.5220000	2.8680000	/
112	284.8340000	35.5220000	2.2940000	/
113	286.5040000	33.6420000	2.4040000	/
121	264.3190000	37.9410000	1.7230000	/
122	264.3190000	37.9410000	.4270000	/
123	265.6030000	36.7750000	2.1280000	/
124	265.6030000	36.7750000	.2560000	/
125	267.8140000	34.7680000	2.5870000	/
126	267.8140000	34.7680000	.2010000	/
127	270.5110000	32.3190000	2.8710000	/
128	270.5110000	32.3190000	.4200000	/
129	273.3400000	29.7500000	3.0020000	/
130	273.3400000	29.7500000	.9150000	/
131	277.6400000	25.8450000	2.8980000	/
132	277.6400000	25.8450000	2.2660000	/
133	279.9130000	23.7820000	2.3850000	/
141	255.9420000	29.3390000	1.7790000	/
142	255.9420000	29.3390000	.4720000	/
143	257.3400000	28.0690000	2.2850000	/
144	257.3400000	28.0690000	.1300000	/
145	259.7470000	25.8840000	2.7650000	/
146	259.7470000	25.8840000	.0730000	/
147	262.6830000	23.2170000	3.0240000	/
148	262.6830000	23.2170000	.2830000	/
149	265.7650000	20.4200000	3.1090000	/
150	265.7650000	20.4200000	.7960000	/
165	251.6800000	17.0000000	2.9430000	/
166	251.6800000	17.0000000	-.0550000	/
167	254.8560000	14.1160000	3.1770000	/
168	254.8560000	14.1160000	.1450000	/
169	258.1890000	11.0900000	3.2150000	/
170	258.1890000	11.0900000	.6770000	/
174	251.6800000	17.0000000	1.9480000	/
176	258.1890000	11.0900000	1.9480000	/
200	243.3000000	9.0000000	1.9480000	/
201	244.4200000	9.0000000	1.5480000	/
202	251.6300000	9.0000000	1.9480000	/
203	258.1800000	9.0000000	1.9480000	/
204	259.9800000	9.0000000	1.9480000	/
205	263.3300000	9.0000000	1.9480000	/
206	268.1500000	9.0000000	1.9480000	/
207	272.3900000	9.0000000	1.9480000	/
208	275.0500000	9.0000000	1.9480000	/
223	258.1800000	4.3500000	1.9480000	/
225	263.3300000	4.3500000	1.9480000	/
226	268.1500000	4.3500000	1.9480000	/
227	272.3900000	4.3500000	1.9480000	/
242	245.7800000	.0000000	1.9480000	/
243	258.1800000	.0000000	1.9480000	/
245	263.3300000	.0000000	1.9480000	/
246	268.1500000	.0000000	1.9480000	/
247	272.3900000	.0000000	1.9480000	/

*/ BODY NODES /

REC BODY 0. 0. 1.948 1. 0. 1.948 0. 0. 10. /

302 100. 0. 0. /

304 120. 0. 0. /

```

306 130. 0. 0. /
308 140. 0. 0. /
310 150. 0. 0. /
312 160. 0. 0. /
314 170. 0. 0. /
316 180. 0. 0. /
318 190. 0. 0. /
320 200. 0. 0. /
322 210. 0. 0. /
324 220. 0. 0. /
326 230. 0. 0. /
328 240. 0. 0. /
330 250. 0. 0. /
332 260. 0. 0. /
334 270. 0. 0. /
336 280.4 0. 0. /
338 300.5 0. 0. /
340 312. 0. 0. /
342 315.1 0. 0. /
344 320. 0. 0. /
346 332.7 0. 0. /
348 340. 0. 0. /
350 344.2 0. 0. /
352 350. 0. 0. /
354 356.5 0. 0. /
356 359.50 0. 0. /
358 368. 0. 0. /
360 370. 0. 0. /
362 394.5 0. 0. /
364 400. 0. 0. /
366 408.1 0. 0. /
*/ HORIZONTAL TAIL NODES /
401 355.56 9.9 0. /
408 373.411 34.234 0. /
REC HT 401 408 355.56 9.9 10.0 /
ANALYSIS FRAME HT /
401 0. 0. 0. TO 408 28. 0. 0. /
411 0. .5823 0. /
412 4. 2.519 0. /
413 8. 1.978 0. /
414 12. 1.417 0. /
415 16. .887 0. /
416 20. .1507 0. /
417 24. -.5425 0. /
418 28. -1.306 0. /
END NCCAL DATA /
BEGIN BC DATA /
*/ RETAINED FREEDOMS /
*/ WING /
RETAIN TZ FOR 165 167 169 /
RETAIN TZ FOR 141 TO 149 BY 2 /
RETAIN TZ FOR 121 TO 133 BY 2 /
** 0 0 0 -20 0 -20 0 0 /
*/ FUSELAGE /
RETAIN TZ FOR 304 310 316 322 328 243 247
238 344 352 356 360 364 /
RETAIN KY FOR 304 310 316 322 328 243 247
238 344 352 356 360 364 /
*/ HORIZONTAL TAIL /
RETAIN TZ FOR 401 TO 408 /
RETAIN RX FOR 401 TO 408 /
RETAIN KY FOR 401 TO 408 /
SUPPORT ASYM IN SURFACE 2 /
SUPPORT TX FOR 247 /
END BC DATA /
BEGIN STIFFNESS DATA /
BEGIN ELEMENT DATA /
BEAM M52 T+0000 N4000 165 174 145
.12200000E+01 0. 0. 0.
.27100000E+00 .25000000E+00 0.0 /
BEAM M52 T+0000 N4001 166 174 146
.12200000E+01 0. 0. 0.
.27100000E+00 .25000000E+00 0.0 /

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BEAM M52 T+0000	N4002	169	176	149
.12200000E+01	0.	0.	0.	
.27100000E+00	.25000000E+00		0.0 /	
BEAM M52 T+0000	N4003	170	176	150
.12200000E+01	0.	0.	0.	
.27100000E+00	.25000000E+00		0.0 /	
BEAM M52 T+0000	N4005	174	176	242
.18750000E+01	0.	0.		.28500000E+00
.57700000E+00	.87900000E-01		0.0 /	
BEAM M52 T+0000	N4006	174	202	242
.31250000E+01	0.	0.		.11180000E+01
.16280000E+01	.40700000E+00		0.0 /	
BEAM M52 T+0000	N4007	174	201	242
.37500000E+01	0.	0.		.17610000E+01
.19530000E+01	.70300000E+00		0.0 /	
BEAM M52 T+0000	N4008	200	201	242
.31250000E+01	0.	0.		.11180000E+01
.16280000E+01	.40700000E+00		0.0 /	
BEAM M52 T+0000	N4009	201	202	242
.31250000E+01	0.	0.		.11180000E+01
.16280000E+01	.40700000E+00		0.0 /	
BEAM M52 T+0000	N4010	203	204	242
.31250000E+01	0.	0.		.11180000E+01
.16280000E+01	.40700000E+00		0.0 /	
BEAM M52 T+0000	N4011	204	205	242
.31250000E+01	0.	0.		.11180000E+01
.16280000E+01	.40700000E+00		0.0 /	
BEAM M52 T+0000	N4012	205	206	242
.31250000E+01	0.	0.		.11180000E+01
.16280000E+01	.40700000E+00		0.0 /	
BEAM M52 T+0000	N4013	206	207	242
.31250000E+01	0.	0.		.11180000E+01
.16280000E+01	.40700000E+00		0.0 /	
BEAM M52 T+0000	N4014	207	208	242
.31250000E+01	0.	0.		.11180000E+01
.16280000E+01	.40700000E+00		0.0 /	
BEAM M52 T+0000	N4015	201	242	243
.31250000E+01	0.	0.		.11180000E+01
.16280000E+01	.40700000E+00		0.0 /	
BEAM M52 T+0000	N4016	202	242	243
.31250000E+01	0.	0.		.11180000E+01
.16280000E+01	.40700000E+00		0.0 /	
BEAM M52 T+0000	N4017	202	243	242
.31250000E+01	0.	0.		.11180000E+01
.16280000E+01	.40700000E+00		0.0 /	
BEAM M52 T+0000	N4018	223	225	242
.12500000E+01	0.	0.		.91000000E-01
.65100000E+00	.26000000E-01		0.0 /	
BEAM M52 T+0000	N4019	225	226	242
.12500000E+01	0.	0.		.91000000E-01
.65100000E+00	.26000000E-01		0.0 /	
BEAM M52 T+0000	N4020	226	227	242
.12500000E+01	0.	0.		.91000000E-01
.65100000E+00	.26000000E-01		0.0 /	
BEAM M52 T+0000	N4021	242	243	201
.31250000E+01	0.	0.		.11180000E+01
.16280000E+01	.40700000E+00		0.0 /	
BEAM M52 T+0000	N4022	243	245	201
.12500000E+01	0.	0.		.91000000E-01
.65100000E+00	.26000000E-01		0.0 /	
BEAM M52 T+0000	N4023	245	246	201
.12500000E+01	0.	0.		.91000000E-01
.65100000E+00	.26000000E-01		0.0 /	
BEAM M52 T+0000	N4024	246	247	201
.12500000E+01	0.	0.		.91000000E-01
.65100000E+00	.26000000E-01		0.0 /	
BEAM M52 T+0000	N4025	203	223	242
.31250000E+01	0.	0.		.11180000E+01
.16280000E+01	.40700000E+00		0.0 /	
BEAM M52 T+0000	N4026	205	225	242
.12500000E+01	0.	0.		.91000000E-01
.65100000E+00	.26000000E-01		0.0 /	

BEAM M52 T+0000	N4027	206	226	242
.12500000E+01	0.	0.	0.0 /	.91000000E-01
.65100000E+00	.26000000E-01		227	242
BEAM M52 T+0000	N4028	207		.91000000E-01
.12500000E+01	0.	0.	0.0 /	
.65100000E+00	.26000000E-01		243	242
BEAM M52 T+0000	N4029	223		.11180000E+01
.31250000E+01	0.	0.	0.0 /	
.16280000E+01	.40700000E+00		245	242
BEAM M52 T+0000	N4030	225		.91000000E-01
.12500000E+01	0.	0.	0.0 /	
.65100000E+00	.26000000E-01		246	242
BEAM M52 T+0000	N4031	226		.91000000E-01
.12500000E+01	0.	0.	0.0 /	
.65100000E+00	.26000000E-01		247	242
BEAM M52 T+0000	N4032	227		.91000000E-01
.12500000E+01	0.	0.	0.0 /	
.65100000E+00	.26000000E-01		204	242
BEAM M54 T+0000	N8000	202		.40000000E+01
.40000000E+01	0.	0.	0.0 /	
.20000000E+03	.20000000E+03			
R00 M53 T+0000	N2000	1	21	.60000000E-01 /
R00 M53 T+0000	N2001	3	23	.98000000E-01 /
R00 M53 T+0000	N2002	5	25	.67000000E-01 /
R00 M53 T+0000	N2003	7	27	.13400000E+00 /
R00 M53 T+0000	N2004	9	29	.18800000E+00 /
R00 M53 T+0000	N2005	11	31	.15900000E+00 /
R00 M53 T+0000	N2006	13	33	.15500000E+00 /
R00 M53 T+0000	N2007	12	32	.15900000E+00 /
R00 M53 T+0000	N2008	10	30	.18800000E+00 /
R00 M53 T+0000	N2009	8	28	.13400000E+00 /
R00 M53 T+0000	N2010	6	26	.67000000E-01 /
R00 M53 T+0000	N2011	4	24	.98000000E-01 /
R00 M53 T+0000	N2012	2	22	.60000000E-01 /
R00 M53 T+0000	N2013	21	41	.52000000E-01 /
R00 M53 T+0000	N2014	23	43	.10400000E+00 /
R00 M53 T+0000	N2015	25	45	.12200000E+00 /
R00 M53 T+0000	N2016	27	47	.15700000E+00 /
R00 M53 T+0000	N2017	29	49	.20700000E+00 /
R00 M53 T+0000	N2018	31	51	.18600000E+00 /
R00 M53 T+0000	N2019	33	53	.18200000E+00 /
R00 M53 T+0000	N2020	32	52	.13600000E+00 /
R00 M53 T+0000	N2021	30	50	.20700000E+00 /
R00 M53 T+0000	N2022	28	48	.15700000E+00 /
R00 M53 T+0000	N2023	26	46	.12200000E+00 /
R00 M53 T+0000	N2024	24	44	.10400000E+00 /
R00 M53 T+0000	N2025	22	42	.52000000E-01 /
R00 M53 T+0000	N2026	41	61	.51000000E-01 /
R00 M53 T+0000	N2027	43	63	.11400000E+00 /
R00 M53 T+0000	N2028	45	65	.16000000E+00 /
R00 M53 T+0000	N2029	47	67	.18000000E+00 /
R00 M53 T+0000	N2030	49	69	.23200000E+00 /
R00 M53 T+0000	N2031	51	71	.21400000E+00 /
R00 M53 T+0000	N2032	53	73	.20800000E+00 /
R00 M53 T+0000	N2033	52	72	.21400000E+00 /
R00 M53 T+0000	N2034	50	70	.23200000E+00 /
R00 M53 T+0000	N2035	48	68	.18000000E+00 /
R00 M53 T+0000	N2036	46	66	.16000000E+00 /
R00 M53 T+0000	N2037	44	64	.11400000E+00 /
R00 M53 T+0000	N2038	42	62	.51000000E-01 /
R00 M53 T+0000	N2039	61	81	.58000000E-01 /
R00 M53 T+0000	N2040	63	83	.12900000E+00 /
R00 M53 T+0000	N2041	65	85	.18000000E+00 /
R00 M53 T+0000	N2042	67	87	.20300000E+00 /
R00 M53 T+0000	N2043	69	89	.26200000E+00 /
R00 M53 T+0000	N2044	71	91	.24200000E+00 /
R00 M53 T+0000	N2045	73	93	.23500000E+00 /
R00 M53 T+0000	N2046	72	92	.24200000E+00 /
R00 M53 T+0000	N2047	70	90	.52000000E+00 /
R00 M53 T+0000	N2048	68	88	.20300000E+00 /
R00 M53 T+0000	N2049	66	86	.18000000E+00 /
R00 M53 T+0000	N2050	64	84	.12900000E+00 /

R00	M53	T+0000	N2051	62	82	.58000000E-01 /
R00	M53	T+0000	N2052	81	101	.64000000E-01 /
R00	M53	T+0000	N2053	83	103	.14300000E+00 /
R00	M53	T+0000	N2054	85	105	.20100000E+00 /
R00	M53	T+0000	N2055	87	107	.22600000E+00 /
R00	M53	T+0000	N2056	89	109	.29200000E+00 /
R00	M53	T+0000	N2057	91	111	.26900000E+00 /
R00	M53	T+0000	N2058	93	113	.26200000E+00 /
R00	M53	T+0000	N2059	92	112	.26900000E+00 /
R00	M53	T+0000	N2060	90	110	.29200000E+00 /
R00	M53	T+0000	N2061	88	108	.22600000E+00 /
R00	M53	T+0000	N2062	86	106	.20100000E+00 /
R00	M53	T+0000	N2063	84	104	.14300000E+00 /
R00	M53	T+0000	N2064	82	102	.64000000E-01 /
R00	M53	T+0000	N2065	101	121	.71000000E-01 /
R00	M53	T+0000	N2066	103	123	.14900000E+00 /
R00	M53	T+0000	N2067	105	125	.23000000E+00 /
R00	M53	T+0000	N2068	107	127	.25000000E+00 /
R00	M53	T+0000	N2069	109	129	.32200000E+00 /
R00	M53	T+0000	N2070	111	131	.29700000E+00 /
R00	M53	T+0000	N2071	113	133	.28900000E+00 /
R00	M53	T+0000	N2072	112	132	.29700000E+00 /
R00	M53	T+0000	N2073	110	130	.32200000E+00 /
R00	M53	T+0000	N2074	108	128	.25000000E+00 /
R00	M53	T+0000	N2075	106	126	.23000000E+00 /
R00	M53	T+0000	N2076	104	124	.14900000E+00 /
R00	M53	T+0000	N2077	102	122	.71000000E-01 /
R00	M53	T+0000	N2078	121	141	.77000000E-01 /
R00	M53	T+0000	N2079	123	143	.16400000E+00 /
R00	M53	T+0000	N2080	125	145	.25100000E+00 /
R00	M53	T+0000	N2081	127	147	.27300000E+00 /
R00	M53	T+0000	N2082	129	149	.14000000E+00 /
R00	M53	T+0000	N2083	130	150	.14000000E+00 /
R00	M53	T+0000	N2084	128	148	.27300000E+00 /
R00	M53	T+0000	N2085	126	146	.25100000E+00 /
R00	M53	T+0000	N2086	124	144	.16400000E+00 /
R00	M53	T+0000	N2087	122	142	.77000000E-01 /
R00	M53	T+0000	N2088	145	165	.14500000E+00 /
R00	M53	T+0000	N2089	147	167	.29500000E+00 /
R00	M53	T+0000	N2090	149	169	.15200000E+00 /
R00	M53	T+0000	N2091	150	170	.15200000E+00 /
R00	M53	T+0000	N2092	148	168	.29500000E+00 /
R00	M53	T+0000	N2093	146	166	.14500000E+00 /
R00	M52	T+0000	N2102	47	67	.40000000E-01 /
R00	M52	T+0000	N2103	67	87	.44800000E-01 /
R00	M52	T+0000	N2104	87	107	.48300000E-01 /
R00	M52	T+0000	N2105	107	127	.51300000E-01 /
R00	M52	T+0000	N2106	127	147	.53500000E-01 /
R00	M52	T+0000	N2112	48	68	.40000000E-01 /
R00	M52	T+0000	N2113	68	88	.44800000E-01 /
R00	M52	T+0000	N2114	88	108	.48300000E-01 /
R00	M52	T+0000	N2115	108	128	.51300000E-01 /
R00	M52	T+0000	N2116	128	148	.53500000E-01 /
R00	M52	T+0000	N2117	148	168	.55300000E-01 /
R00	M51	T+0000	N2120	1	3	.19700000E-01 /
R00	M51	T+0000	N2121	3	5	.31200000E-01 /
R00	M51	T+0000	N2122	5	7	.33200000E-01 /
R00	M51	T+0000	N2123	7	9	.30900000E-01 /
R00	M51	T+0000	N2124	9	11	.19100000E-01 /
R00	M51	T+0000	N2125	11	13	.40000000E-03 /
R00	M51	T+0000	N2126	12	13	.40000000E-03 /
R00	M51	T+0000	N2127	10	12	.19100000E-01 /
R00	M51	T+0000	N2128	8	10	.30900000E-01 /
R00	M51	T+0000	N2129	6	8	.33200000E-01 /
R00	M51	T+0000	N2130	4	6	.31200000E-01 /
R00	M51	T+0000	N2131	2	4	.19700000E-01 /
R00	M52	T+0000	N2140	21	23	.20000000E+00 /
R00	M52	T+0000	N2141	23	25	.26600000E+00 /
R00	M52	T+0000	N2142	25	27	.29100000E+00 /
R00	M52	T+0000	N2143	27	29	.27300000E+00 /
R00	M52	T+0000	N2144	29	31	.17200000E+00 /
R00	M52	T+0000	N2145	31	33	.46000000E-01 /
R00	M52	T+0000	N2146	32	33	.46000000E-01 /

RDD	M52	T+0000	N2147	30	32	.17200000E+00 /
RDD	M52	T+0000	N2148	28	30	.27300000E+00 /
RDD	M52	T+0000	N2149	26	28	.29100000E+00 /
RDD	M52	T+0000	N2150	24	26	.26600000E+00 /
RDD	M52	T+0000	N2151	22	24	.20000000E+00 /
RDD	M52	T+0000	N2160	41	43	.22100000E-01 /
RCD	M52	T+0000	N2161	43	45	.30600000E-01 /
RDD	M52	T+0000	N2162	45	47	.29500000E-01 /
RCD	M52	T+0000	N2163	47	49	.29100000E-01 /
RDD	M52	T+0000	N2164	49	51	.24000000E-01 /
RDD	M52	T+0000	N2165	51	53	.50000000E-02 /
RDD	M52	T+0000	N2166	52	53	.50000000E-02 /
RCD	M52	T+0000	N2167	50	52	.24000000E-01 /
RDD	M52	T+0000	N2168	48	50	.29100000E-01 /
RDD	M52	T+0000	N2169	46	48	.29500000E-01 /
RDD	M52	T+0000	N2170	44	46	.30600000E-01 /
RDD	M52	T+0000	N2171	42	44	.22100000E-01 /
RDD	M52	T+0000	N2180	61	63	.25300000E-01 /
RDD	M52	T+0000	N2181	63	65	.33900000E-01 /
RDD	M52	T+0000	N2182	65	67	.32900000E-01 /
RCD	M52	T+0000	N2183	67	69	.32400000E-01 /
RDD	M52	T+0000	N2184	69	71	.26900000E-01 /
RDD	M52	T+0000	N2185	71	73	.74000000E-02 /
RDD	M52	T+0000	N2186	72	73	.74000000E-02 /
RDD	M52	T+0000	N2187	70	72	.26900000E-01 /
RDD	M52	T+0000	N2188	68	70	.32400000E-01 /
RCD	M52	T+0000	N2189	66	68	.32900000E-01 /
RCD	M52	T+0000	N2190	64	66	.33900000E-01 /
RDD	M52	T+0000	N2191	62	64	.25300000E-01 /
RCD	M52	T+0000	N2200	81	83	.28400000E-01 /
RDD	M52	T+0000	N2201	83	85	.37400000E-01 /
RCD	M52	T+0000	N2202	85	87	.36400000E-01 /
RDD	M52	T+0000	N2203	87	89	.35500000E-01 /
RDD	M52	T+0000	N2204	89	91	.29600000E-01 /
RCD	M52	T+0000	N2205	91	93	.95000000E-02 /
RCD	M52	T+0000	N2206	92	93	.95000000E-02 /
RDD	M52	T+0000	N2207	90	92	.29600000E-01 /
RCD	M52	T+0000	N2208	88	90	.35500000E-01 /
RDD	M52	T+0000	N2209	86	88	.36400000E-01 /
RDD	M52	T+0000	N2210	84	86	.37400000E-01 /
RCD	M52	T+0000	N2211	82	84	.28400000E-01 /
RDD	M52	T+0000	N2220	101	103	.31300000E-01 /
RDD	M52	T+0000	N2221	103	105	.40800000E-01 /
RCD	M52	T+0000	N2222	105	107	.39700000E-01 /
RCD	M52	T+0000	N2223	107	109	.38500000E-01 /
RCD	M52	T+0000	N2224	109	111	.32000000E-01 /
RDD	M52	T+0000	N2225	111	113	.11500000E-01 /
RDD	M52	T+0000	N2226	112	113	.11500000E-01 /
RCD	M52	T+0000	N2227	110	112	.32000000E-01 /
RCD	M52	T+0000	N2228	108	110	.38500000E-01 /
RDD	M52	T+0000	N2229	106	108	.39700000E-01 /
RCD	M52	T+0000	N2230	104	106	.40800000E-01 /
RCD	M52	T+0000	N2231	102	104	.31300000E-01 /
RDD	M52	T+0000	N2240	121	123	.33800000E-01 /
RDD	M52	T+0000	N2241	123	125	.43900000E-01 /
RDD	M52	T+0000	N2242	125	127	.42800000E-01 /
RDD	M52	T+0000	N2243	127	129	.41300000E-01 /
RDD	M52	T+0000	N2244	129	131	.34200000E-01 /
RDD	M52	T+0000	N2245	131	133	.13200000E-01 /
RDD	M52	T+0000	N2246	132	133	.13200000E-01 /
RDD	M52	T+0000	N2247	130	132	.34200000E-01 /
RDD	M52	T+0000	N2248	128	130	.41300000E-01 /
RDD	M52	T+0000	N2249	126	128	.42800000E-01 /
RCD	M52	T+0000	N2250	124	126	.43900000E-01 /
RDD	M52	T+0000	N2251	122	124	.33800000E-01 /
RDD	M52	T+0000	N2260	141	143	.36100000E-01 /
RDD	M52	T+0000	N2261	143	145	.46800000E-01 /
RDD	M52	T+0000	N2262	145	147	.45800000E-01 /
RDD	M52	T+0000	N2263	147	149	.43900000E-01 /

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RDD	M52	T+000C	N2264	148	150	.43900000E-01 /	
RDD	M52	T+0000	N2265	146	148	.45800000E-01 /	
RDD	M52	T+0000	N2266	144	146	.46800000E-01 /	
RDD	M52	T+000C	N2267	142	144	.36100000E-01 /	
RDD	M52	T+000C	N2282	165	167	.74700000E-01 /	
RDD	M52	T+0000	N2283	167	169	.71100000E-01 /	
RDD	M52	T+000C	N2284	168	170	.71100000E-01 /	
RDD	M52	T+0000	N2285	166	168	.74700000E-01 /	
RDD	M55	T+0000	N2301	25	45	.11600000E+00 /	
RDD	M55	T+0000	N2302	45	65	.13900000E+00 /	
RDD	M55	T+0000	N2303	65	85	.16300000E+00 /	
RDD	M55	T+0000	N2304	85	105	.18700000E+00 /	
RDD	M55	T+0000	N2305	105	125	.21400000E+00 /	
RDD	M55	T+0000	N2306	125	145	.24300000E+00 /	
RDD	M55	T+0000	N2307	145	165	.27700000E+00 /	
RDD	M55	T+0000	N2311	26	46	.11600000E+00 /	
RDD	M55	T+0000	N2312	46	66	.13900000E+00 /	
RDD	M55	T+0000	N2313	66	86	.16300000E+00 /	
RDD	M55	T+0000	N2314	86	106	.18700000E+00 /	
RDD	M55	T+0000	N2315	106	126	.21400000E+00 /	
RDD	M55	T+0000	N2316	126	146	.24300000E+00 /	
RDD	M55	T+0000	N2317	146	166	.27700000E+00 /	
RDD	M55	T+0000	N2321	29	49	.13700000E+00 /	
RDD	M55	T+0000	N2322	49	69	.15500000E+00 /	
RDD	M55	T+0000	N2323	69	89	.17200000E+00 /	
RDD	M55	T+0000	N2324	89	109	.19000000E+00 /	
RDD	M55	T+0000	N2325	109	129	.20700000E+00 /	
RDD	M55	T+0000	N2326	129	149	.22800000E+00 /	
RDD	M55	T+0000	N2327	149	169	.25000000E+00 /	
RDD	M55	T+0000	N2331	30	50	.13700000E+00 /	
RDD	M55	T+0000	N2332	50	70	.15500000E+00 /	
RDD	M55	T+0000	N2333	70	90	.17200000E+00 /	
RDD	M55	T+0000	N2334	90	110	.19000000E+00 /	
RDD	M55	T+0000	N2335	110	130	.20700000E+00 /	
RDD	M55	T+0000	N2336	130	150	.22800000E+00 /	
RDD	M55	T+0000	N2337	150	170	.25000000E+00 /	
GPLATE	M52	T+0000	N5500	243	223	225	245
			.25000000E+00	0.		/	
GPLATE	M52	T+0000	N5501	223	203	205	225
			.25000000E+00	0.		/	
GPLATE	M52	T+0000	N5502	245	225	226	246
			.25000000E+00	0.		/	
GPLATE	M52	T+0000	N5503	225	205	206	226
			.25000000E+00	0.		/	
GPLATE	M52	T+0000	N5504	246	226	227	247
			.25000000E+00	0.		/	
GPLATE	M52	T+0000	N5505	226	206	207	227
			.25000000E+00	0.		/	
RDD	M53	T+0000	N3000	1	2	.10000000E-01 /	
RDD	M53	T+0000	N3001	3	4	.10000000E-01 /	
RDD	M53	T+0000	N3002	5	6	.10000000E-01 /	
RDD	M53	T+0000	N3003	7	8	.10000000E-01 /	
RDD	M53	T+0000	N3004	9	10	.10000000E-01 /	
RDD	M53	T+0000	N3005	11	12	.10000000E-01 /	
RDD	M54	T+0000	N3006	21	22	.10000000E-01 /	
RDD	M54	T+0000	N3007	23	24	.10000000E-01 /	
RDD	M54	T+0000	N3008	25	26	.10000000E-01 /	
RDD	M54	T+0000	N3009	27	28	.10000000E-01 /	
RDD	M54	T+0000	N3010	29	30	.10000000E-01 /	
RDD	M54	T+0000	N3011	31	32	.10000000E-01 /	
RDD	M54	T+0000	N3012	41	42	.10000000E-01 /	
RDD	M54	T+0000	N3013	43	44	.10000000E-01 /	
RDD	M54	T+0000	N3014	45	46	.10000000E-01 /	
RDD	M54	T+0000	N3015	47	48	.10000000E-01 /	
RDD	M54	T+0000	N3016	49	50	.10000000E-01 /	
RDD	M54	T+0000	N3017	51	52	.10000000E-01 /	
RDD	M54	T+0000	N3018	61	62	.10000000E-01 /	
RDD	M54	T+0000	N3019	63	64	.10000000E-01 /	
RDD	M54	T+0000	N3020	65	66	.10000000E-01 /	
RDD	M54	T+0000	N3021	67	68	.10000000E-01 /	
RDD	M54	T+0000	N3022	69	70	.10000000E-01 /	
RDD	M54	T+0000	N3023	71	72	.10000000E-01 /	
RDD	M54	T+0000	N3024	81	82	.10000000E-01 /	

RDD	M54	T+0000	N3025	83	84	.10000000E-01	/
RDD	M54	T+0000	N3026	85	86	.10000000E-01	/
RDD	M54	T+0000	N3027	87	88	.10000000E-01	/
RDD	M54	T+0000	N3028	89	90	.10000000E-01	/
RDD	M54	T+0000	N3029	91	92	.10000000E-01	/
RDD	M54	T+0000	N3030	101	102	.10000000E-01	/
RDD	M54	T+0000	N3031	103	104	.10000000E-01	/
RDD	M54	T+0000	N3032	105	106	.10000000E-01	/
RDD	M54	T+0000	N3033	107	108	.10000000E-01	/
RDD	M54	T+0000	N3034	109	110	.10000000E-01	/
RDD	M54	T+0000	N3035	111	112	.10000000E-01	/
RDD	M54	T+0000	N3036	121	122	.10000000E-01	/
RDD	M54	T+0000	N3037	123	124	.10000000E-01	/
RDD	M54	T+0000	N3038	125	126	.10000000E-01	/
RDD	M54	T+0000	N3039	127	128	.10000000E-01	/
RDD	M54	T+0000	N3040	129	130	.10000000E-01	/
RDD	M54	T+0000	N3041	131	132	.10000000E-01	/
RDD	M54	T+0000	N3042	141	142	.10000000E-01	/
RDD	M54	T+0000	N3043	143	144	.10000000E-01	/
RDD	M54	T+0000	N3044	145	146	.10000000E-01	/
RDD	M54	T+0000	N3045	147	148	.10000000E-01	/
RDD	M54	T+0000	N3046	149	150	.10000000E-01	/
RDD	M54	T+0000	N3047	167	168	.10000000E-01	/
RDD	M55	T+0000	N3052	45	46	.50000000E-01	/
RDD	M55	T+0000	N3053	65	66	.50000000E-01	/
RDD	M55	T+0000	N3054	85	86	.50000000E-01	/
RDD	M55	T+0000	N3055	105	106	.50000000E-01	/
RDD	M55	T+0000	N3056	125	126	.50000000E-01	/
RDD	M55	T+0000	N3057	145	146	.50000000E-01	/
RDD	M55	T+0000	N3062	49	50	.50000000E-01	/
RDD	M55	T+0000	N3063	69	70	.50000000E-01	/
RDD	M55	T+0000	N3064	89	90	.50000000E-01	/
RDD	M55	T+0000	N3065	109	110	.50000000E-01	/
RDD	M55	T+0000	N3066	129	130	.50000000E-01	/
RDD	M55	T+0000	N3067	149	150	.50000000E-01	/
SPLATE	M51	T+0000	N1000	21	1	3	23 .70000000E-01 /
SPLATE	M51	T+0000	N1001	23	3	5	25 .70000000E-01 /
SPLATE	M51	T+0000	N1002	25	5	7	27 .70000000E-01 /
SPLATE	M51	T+0000	N1003	27	7	9	29 .70000000E-01 /
SPLATE	M51	T+0000	N1004	29	9	11	31 .70000000E-01 /
SPLATE	M51	T+0000	N1005	31	11	13	33 .70000000E-01 /
SPLATE	M51	T+0000	1006	33	13	12	32 .70000000E-01 /
SPLATE	M51	T+0000	1007	32	12	10	30 .70000000E-01 /
SPLATE	M51	T+0000	N1008	30	10	8	28 .70000000E-01 /
SPLATE	M51	T+0000	N1009	28	8	6	26 .70000000E-01 /
SPLATE	M51	T+0000	N1010	26	6	4	24 .70000000E-01 /
SPLATE	M51	T+0000	N1011	24	4	2	22 .70000000E-01 /
SPLATE	M51	T+0000	N1012	22	2	1	21 .70000000E-01 /
SPLATE	M51	T+0000	N1020	41	21	23	43 .70000000E-01 /
SPLATE	M51	T+0000	N1021	43	23	25	45 .70000000E-01 /
SPLATE	M51	T+0000	N1022	45	25	27	47 .70000000E-01 /
SPLATE	M51	T+0000	N1023	47	27	29	49 .70000000E-01 /
SPLATE	M51	T+0000	N1024	49	29	31	51 .70000000E-01 /
SPLATE	M51	T+0000	N1025	51	31	33	53 .70000000E-01 /
SPLATE	M51	T+0000	N1026	53	33	32	52 .70000000E-01 /
SPLATE	M51	T+0000	N1027	52	32	30	50 .70000000E-01 /
SPLATE	M51	T+0000	N1028	50	30	28	48 .70000000E-01 /
SPLATE	M51	T+0000	N1029	48	28	26	46 .70000000E-01 /
SPLATE	M51	T+0000	N1030	46	26	24	44 .70000000E-01 /
SPLATE	M51	T+0000	N1031	44	24	22	42 .70000000E-01 /
SPLATE	M51	T+0000	N1032	42	22	21	41 .70000000E-01 /
SPLATE	M51	T+0000	N1040	61	41	43	63 .70000000E-01 /
SPLATE	M51	T+0000	N1041	63	43	45	65 .70000000E-01 /
SPLATE	M51	T+0000	N1042	65	45	47	67 .70000000E-01 /
SPLATE	M51	T+0000	N1043	67	47	49	69 .70000000E-01 /
SPLATE	M51	T+0000	N1044	69	49	51	71 .70000000E-01 /
SPLATE	M51	T+0000	N1045	71	51	53	73 .70000000E-01 /
SPLATE	M51	T+0000	N1046	73	53	52	72 .70000000E-01 /
SPLATE	M51	T+0000	N1047	72	52	50	70 .70000000E-01 /
SPLATE	M51	T+0000	N1048	70	50	48	68 .70000000E-01 /
SPLATE	M51	T+0000	N1049	68	48	46	66 .70000000E-01 /
SPLATE	M51	T+0000	N1050	66	46	44	64 .70000000E-01 /
SPLATE	M51	T+0000	N1051	64	44	42	62 .70000000E-01 /

SPLATE	M51	T+0000	N1052	62	42	41	61	.70000000E-01 /
SPLATE	M51	T+0000	N1060	81	61	63	83	.70000000E-01 /
SPLATE	M51	T+0000	N1061	83	63	65	85	.70000000E-01 /
SPLATE	M51	T+0000	N1062	85	65	67	87	.70000000E-01 /
SPLATE	M51	T+0000	N1063	87	67	69	89	.70000000E-01 /
SPLATE	M51	T+0000	N1064	89	69	71	91	.70000000E-01 /
SPLATE	M51	T+0000	N1065	91	71	73	93	.70000000E-01 /
SPLATE	M51	T+0000	N1066	93	73	72	92	.70000000E-01 /
SPLATE	M51	T+0000	N1067	92	72	70	90	.70000000E-01 /
SPLATE	M51	T+0000	N1068	90	70	68	88	.70000000E-01 /
SPLATE	M51	T+0000	N1069	88	68	66	86	.70000000E-01 /
SPLATE	M51	T+0000	N1070	86	66	64	84	.70000000E-01 /
SPLATE	M51	T+0000	N1071	84	64	62	82	.70000000E-01 /
SPLATE	M51	T+0000	N1072	82	62	61	81	.70000000E-01 /
SPLATE	M51	T+0000	N1080	101	81	83	103	.70000000E-01 /
SPLATE	M51	T+0000	N1081	103	83	85	105	.70000000E-01 /
SPLATE	M51	T+0000	N1082	105	85	87	107	.70000000E-01 /
SPLATE	M51	T+0000	N1083	107	87	89	109	.70000000E-01 /
SPLATE	M51	T+0000	N1084	109	89	91	111	.70000000E-01 /
SPLATE	M51	T+0000	N1085	111	91	93	113	.70000000E-01 /
SPLATE	M51	T+0000	N1086	113	93	92	112	.70000000E-01 /
SPLATE	M51	T+0000	N1087	112	92	90	110	.70000000E-01 /
SPLATE	M51	T+0000	N1088	110	90	88	108	.70000000E-01 /
SPLATE	M51	T+0000	N1089	108	88	86	106	.70000000E-01 /
SPLATE	M51	T+0000	N1090	106	86	84	104	.70000000E-01 /
SPLATE	M51	T+0000	N1091	104	84	82	102	.70000000E-01 /
SPLATE	M51	T+0000	N1092	102	82	81	101	.70000000E-01 /
SPLATE	M51	T+0000	N1100	121	101	103	123	.70000000E-01 /
SPLATE	M51	T+0000	N1101	123	103	105	125	.70000000E-01 /
SPLATE	M51	T+0000	N1102	125	105	107	127	.70000000E-01 /
SPLATE	M51	T+0000	N1103	127	107	109	129	.70000000E-01 /
SPLATE	M51	T+0000	N1104	129	109	111	131	.70000000E-01 /
SPLATE	M51	T+0000	N1105	131	111	113	133	.70000000E-01 /
SPLATE	M51	T+0000	N1106	133	113	112	132	.70000000E-01 /
SPLATE	M51	T+0000	N1107	132	112	110	130	.70000000E-01 /
SPLATE	M51	T+0000	N1108	130	110	108	128	.70000000E-01 /
SPLATE	M51	T+0000	N1109	128	108	106	126	.70000000E-01 /
SPLATE	M51	T+0000	N1110	126	106	104	124	.70000000E-01 /
SPLATE	M51	T+0000	N1111	124	104	102	122	.70000000E-01 /
SPLATE	M51	T+0000	N1112	122	102	101	121	.70000000E-01 /
SPLATE	M51	T+0000	N1120	141	121	123	143	.70000000E-01 /
SPLATE	M51	T+0000	N1121	143	123	125	145	.70000000E-01 /
SPLATE	M51	T+0000	N1122	145	125	127	147	.70000000E-01 /
SPLATE	M51	T+0000	N1123	147	127	129	149	.70000000E-01 /
SPLATE	M51	T+0000	N1128	150	130	128	148	.70000000E-01 /
SPLATE	M51	T+0000	N1129	148	128	126	146	.70000000E-01 /
SPLATE	M51	T+0000	N1130	146	126	124	144	.70000000E-01 /
SPLATE	M51	T+0000	N1131	144	124	122	142	.70000000E-01 /
SPLATE	M51	T+0000	N1132	142	122	121	141	.70000000E-01 /
SPLATE	M51	T+0000	N1142	165	145	147	167	.70000000E-01 /
SPLATE	M51	T+0000	N1143	167	147	149	169	.70000000E-01 /
SPLATE	M51	T+0000	N1148	170	150	148	168	.70000000E-01 /
SPLATE	M51	T+0000	N1149	168	148	146	166	.70000000E-01 /
SPLATE	M51	T+0000	N1200	1	3	4	2	.70000000E-01 /
SPLATE	M51	T+0000	N1201	3	5	6	4	.70000000E-01 /
SPLATE	M51	T+0000	N1202	5	7	8	6	.70000000E-01 /
SPLATE	M51	T+0000	N1203	7	9	10	8	.70000000E-01 /
SPLATE	M51	T+0000	N1204	9	11	12	10	.70000000E-01 /
SPLATE	M52	T+0000	N1205	21	23	24	22	.16400000E+01 /
SPLATE	M52	T+0000	N1206	23	25	26	24	.16400000E+01 /
SPLATE	M52	T+0000	N1207	25	27	28	26	.16400000E+01 /
SPLATE	M52	T+0000	N1208	27	29	30	28	.16400000E+01 /
SPLATE	M52	T+0000	N1209	29	31	32	30	.16400000E+01 /
SPLATE	M52	T+0000	N1210	41	43	44	42	.50000000E-01 /
SPLATE	M52	T+0000	N1211	43	45	46	44	.50000000E-01 /
SPLATE	M52	T+0000	N1212	45	47	48	46	.50000000E-01 /
SPLATE	M52	T+0000	N1213	47	49	50	48	.50000000E-01 /
SPLATE	M52	T+0000	N1214	49	51	52	50	.50000000E-01 /
SPLATE	M52	T+0000	N1215	61	63	64	62	.50000000E-01 /
SPLATE	M52	T+0000	N1216	63	65	66	64	.50000000E-01 /
SPLATE	M52	T+0000	N1217	65	67	68	66	.50000000E-01 /
SPLATE	M52	T+0000	N1218	67	69	70	68	.50000000E-01 /
SPLATE	M52	T+0000	N1219	69	71	72	70	.50000000E-01 /

SPLATE	M52	T+0000	N1220	81	83	84	82	.50000000E-01 /
SPLATE	M52	T+0000	N1221	83	85	86	84	.50000000E-01 /
SPLATE	M52	T+0000	N1222	85	87	88	86	.50000000E-01 /
SPLATE	M52	T+0000	N1223	87	89	90	88	.50000000E-01 /
SPLATE	M52	T+0000	N1224	89	91	92	90	.50000000E-01 /
SPLATE	M52	T+0000	N1225	101	103	104	102	.50000000E-01 /
SPLATE	M52	T+0000	N1226	103	105	106	104	.50000000E-01 /
SPLATE	M52	T+0000	N1227	105	107	108	106	.50000000E-01 /
SPLATE	M52	T+0000	N1228	107	109	110	108	.50000000E-01 /
SPLATE	M52	T+0000	N1229	109	111	112	110	.50000000E-01 /
SPLATE	M52	T+0000	N1230	121	123	124	122	.50000000E-01 /
SPLATE	M52	T+0000	N1231	123	125	126	124	.50000000E-01 /
SPLATE	M52	T+0000	N1232	125	127	128	126	.50000000E-01 /
SPLATE	M52	T+0000	N1233	127	129	130	128	.50000000E-01 /
SPLATE	M52	T+0000	N1234	129	131	132	130	.50000000E-01 /
SPLATE	M52	T+0000	N1235	141	143	144	142	.50000000E-01 /
SPLATE	M52	T+0000	N1236	143	145	146	144	.50000000E-01 /
SPLATE	M52	T+0000	N1237	145	147	148	146	.50000000E-01 /
SPLATE	M52	T+0000	N1238	147	149	150	148	.50000000E-01 /
SPLATE	M52	T+0000	N1239	165	167	168	166	.80000000E-01 /
SPLATE	M52	T+0000	N1240	167	169	170	168	.80000000E-01 /
SPLATE	M55	T+0000	N1301	45	25	26	46	.10000000E+00 /
SPLATE	M55	T+0000	N1302	65	45	46	66	.10000000E+00 /
SPLATE	M55	T+0000	N1303	85	65	66	86	.10000000E+00 /
SPLATE	M55	T+0000	N1304	105	85	86	106	.10000000E+00 /
SPLATE	M55	T+0000	N1305	125	105	106	126	.10000000E+00 /
SPLATE	M55	T+0000	N1306	145	125	126	146	.10000000E+00 /
SPLATE	M55	T+0000	N1307	165	145	146	166	.10000000E+00 /
SPLATE	M55	T+0000	N1311	49	29	30	50	.10000000E+00 /
SPLATE	M55	T+0000	N1312	69	49	50	70	.10000000E+00 /
SPLATE	M55	T+0000	N1313	89	69	70	90	.10000000E+00 /
SPLATE	M55	T+0000	N1314	109	89	90	110	.10000000E+00 /
SPLATE	M55	T+0000	N1315	129	109	110	130	.10000000E+00 /
SPLATE	M55	T+0000	N1316	149	129	130	150	.10000000E+00 /
SPLATE	M55	T+0000	N1317	169	149	150	170	.10000000E+00 /
GPLATE	M52	T+0000	N5000	202	176	203		
		.25000000E+01	.25000000E+01	0.				/
GPLATE	M52	T+0000	N5001	201	202	242		
		.25000000E+00	.25000000E+00	0.				/
GPLATE	M52	T+0000	N5002	202	243	242		
		.25000000E+00	.25000000E+00	0.				/
GPLATE	M52	T+0000	N5003	202	203	243		
		.25000000E+00	.25000000E+00	0.				/

*/ ADDITIONAL ELEMENTS /

ROD M53 TO N7003 5 6 .01 /

ROD N7004 9 10 .01 /

ROD M54 TO N7005 25 26 .01 /

ROD M54 TO N7006 29 30 .01 /

SPLATE N7001 5 6 26 25 .1 /

SPLATE N7002 9 10 30 29 .1 /

PLATE M54 TO N7007 11 12 13 .05 /

PLATE N7008 31 32 33 .05 /

PLATE N7009 51 52 53 .05 /

PLATE N7010 71 72 73 .05 /

PLATE N7011 91 92 93 .05 /

PLATE N7012 111 112 113 .05 /

PLATE N7013 131 132 133 .05 /

*/ FUSELAGE BEAMS /

BEAM M54 TO	N6001	304	308	0.	**4	9.524	0.	**4	52.381	/
BEAM	N6002	308	310	0.	**4	52.381	0.	**4	59.524	/
BEAM	N6003	310	316	0.	**4	59.524	0.	**4	80.952	/
BEAM	N6004	316	320	0.	**4	80.952	0.	**4	126.190	/
BEAM	N6005	320	322	0.	**4	126.190	0.	**4	106.101	/
BEAM	N6006	322	326	0.	**4	106.101	0.	**4	61.905	/
BEAM	N6007	326	328	0.	**4	61.905	0.	**4	100.000	/
BEAM	N6008	328	242	0.	**4	100.000	0.	**4	106.625	/
BEAM	N6009	242	243	0.	**4	106.625	0.	**4	123.810	/
BEAM	N6010	243	246	0.	**4	123.810	0.	**4	116.667	/
BEAM	N6011	246	247	0.	**4	116.667	0.	**4	164.286	/
BEAM	N6012	247	334	0.	**4	164.286	0.	**4	169.048	/
BEAM	N6013	334	338	0.	**4	169.048	0.	**4	181.548	/
BEAM	N6014	338	340	0.	**4	181.548	0.	**4	195.238	/
BEAM	N6015	340	344	0.	**4	195.238	0.	**4	140.476	/


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BEAM      N6016 344 348 0. **4 140.476 0. **4 33.333 /
BEAM      N6017 348 352 0. **4 33.333 0. **4 47.619 /
BEAM      N6018 352 356 0. **4 47.619 0. **4 33.709 /
BEAM      N6019 356 358 0. **4 33.709 0. **4 21.429 /
BEAM      N6020 358 360 0. **4 21.429 0. **4 26.191 /
BEAM      N6021 360 364 0. **4 26.191 0. **4 9.524 /
*/ HORIZONTAL TAIL BEAMS /
BEAM M54 TO N8001 356 401 0. 0. 0. 100. 0. 100. /
BEAM      N8002 401 402 0. 0. 0. 1.330 0. .5635
0. 0. 0. 1.033 0. .427 /
BEAM      N8003 402 403 0. 0. 0. 1.033 0. .427
0. 0. 0. .7418 0. .2949 /
BEAM      N8004 403 404 0. 0. 0. .7418 0. .2949
0. 0. 0. .4873 0. .181 /
BEAM      N8005 404 405 0. 0. 0. .4873 0. .181
0. 0. 0. .2825 0. .0981 /
BEAM      N8006 405 406 0. 0. 0. .2825 0. .0981
0. 0. 0. .1575 0. .04856 /
BEAM      N8007 406 407 0. 0. 0. .1575 0. .04856
0. 0. 0. .0775 0. .02286 /
BEAM      N8008 407 408 0. 0. 0. .0775 0. .02286
0. 0. 0. .03 0. .00762 /
END ELEMENT DATA /
END STIFFNESS DATA /
BEGIN MASS DATA /
BEGIN CONDITION DATA /
STAGE 1 CONDITION 1 0 0 1 /
END CONDITION DATA /
BEGIN MASS ELEMENT DATA /
*/ FUSELAGE MASSES /
SCALAR F2 N326 326 29.3 /
SCALAR F2 N328 328 35.7 /
SCALAR F2 N330 330 42.6 /
SCALAR F2 N243 243 56.5 /
SCALAR F2 N246 246 30.2 /
SCALAR F2 N247 247 30.3 /
SCALAR F2 N332 332 18.0 /
END MASS ELEMENT DATA /
BEGIN CONCENTRATED MASS DATA 1 /
*/ FUSELAGE WEIGHTS /
CM302 304 302 2.4 /
CM304 304 304 27.2 /
CM306 304 306 11.3 /
CM308 310 308 16.4 /
CM310 310 310 18.5 /
CM312 310 312 19.0 /
CM314 316 314 24.8 /
CM316 316 316 18.7 /
CM318 316 318 18.2 /
CM320 322 320 21.8 /
CM322 322 322 29.6 /
CM324 322 324 36.8 /
CM336 338 336 10.8 /
CM338 338 338 221.0 0. 57450. /
CM342 344 342 11.0 /
CM346 344 346 11.8 /
CM350 352 350 16.1 0. .01 /
CM354 356 354 17.8 /
CM356 356 356 15.6 /
CM360 360 360 36.1 0. .01 /
CM362 364 362 12.9 /
CM366 364 366 5.9 /
*/ HORIZONTAL TAIL WEIGHTS /
CM411 401 411 I=HT 1.920 11.406 2.56 /
CM412 402 412 I=HT 1.588 19.544 2.12 /
CM413 403 413 I=HT 1.335 15.368 1.78 /
CM414 404 414 I=HT 1.080 11.482 1.44 /
CM415 405 415 I=HT 0.868 8.627 1.16 /
CM416 406 416 I=HT 0.702 6.623 0.94 /
CM417 407 417 I=HT 0.553 4.987 0.74 /
CM418 408 418 I=HT 0.245 1.662 0.33 /
END CONCENTRATED MASS DATA /
END MASS DATA /

```

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```

BEGIN SUBSET DEFINITION /
SUBSETS OF STIFFNESS SET 1 /
  N1 = ALL /
  N2 = 242 TO 247 302 TO 366 / FUSELAGE NODES
  N3 = 401 TO 418 352 TO 360 / HORIZ. TAIL NODES
  N4 = 1 TO 169 BY 2 / UPPER WING SURFACE
  N5 = 2 TO 170 BY 2 13 TO 133 BY 20 / LOWER WING SURFACE
  N6 = 174 TO 247 / WING-BODY
  E1 = ALL /
  E2 = CLOSED IN N2 /
  E3 = CLOSED IN N3 /
  E4 = CLOSED IN N4 /
  E5 = CLOSED IN N5 /
  E6 = CLOSED IN N6 /
  ON1 = 304 310 316 322 328 165 145 143 141 TO 1 BY -20 +
  3 TO 143 BY 20 145 TO 5 BY -20 7 TO 167 BY 20 +
  169 TO 9 BY -20 11 TO 131 BY 20 133 TO 13 BY -20 +
  11 TO 1 BY -2 21 TO 33 BY 2 53 TO 41 BY -2 61 TO 73 BY 2 +
  93 TO 81 BY -2 101 TO 113 BY 2 +
  133 TO 121 BY -2 141 TO 149 BY 2 169 167 165 328 243 169 243 +
  247 338 344 352 356 360 364 360 356 401 TO 408 /
END SUBSET DEFINITION /
END PROBLEM DATA /

```

Table 205-1. Natural Frequencies
for FIREBLE Drone

Mode No.	Frequency (Hertz)	Description
1	0.	Rigid body
2	0.	Rigid body
3	10.05	Wing bending
4	17.41	Fuselage bending
5	42.86	Fuselage bending
6	46.15	Wing bending
7	52.81	Wing twisting
8	63.76	Horizontal tail bending
9	73.05	Coupled wing, fuselage and tail
10	106.3	Wing twisting

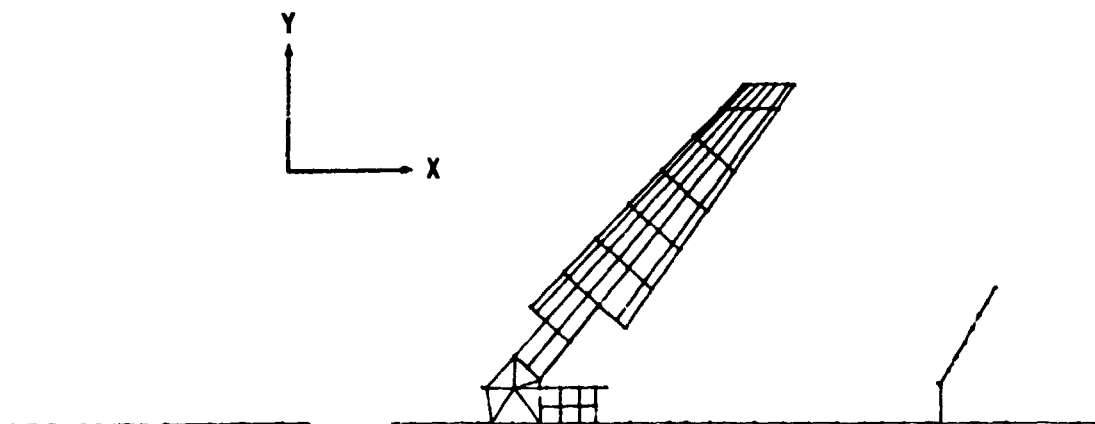


Figure 205-i. Total FIREBEE Structural Model

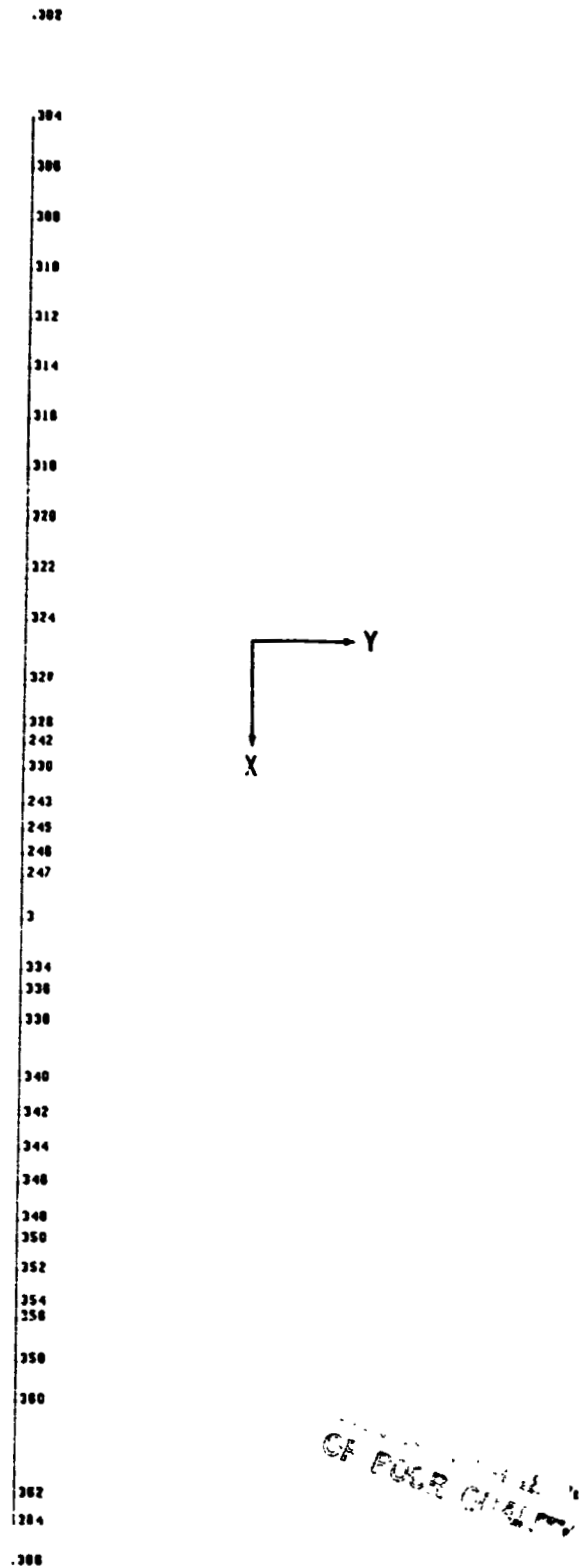


Figure 205-2. Fuselage Model, FIREBEE Drone

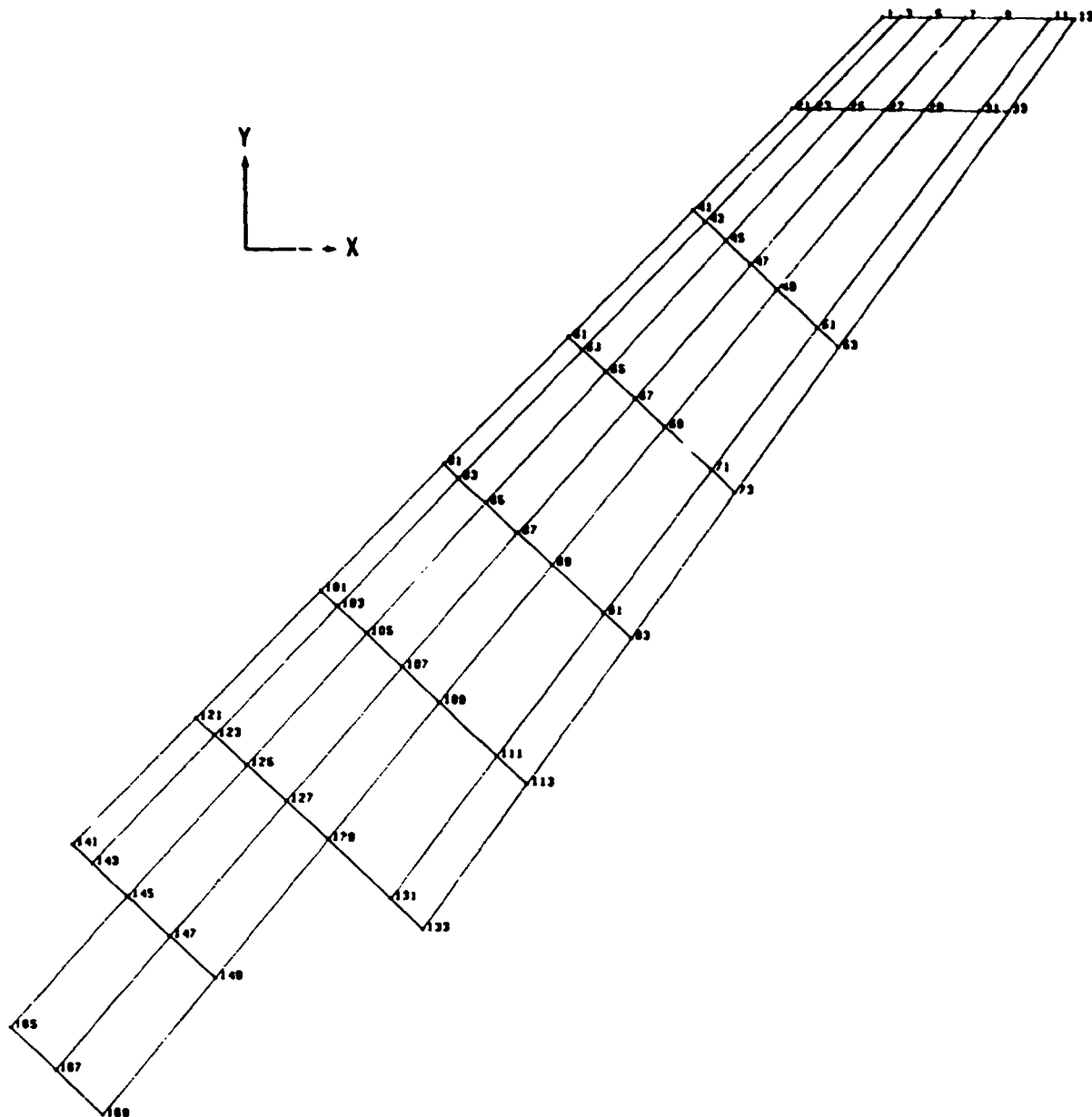
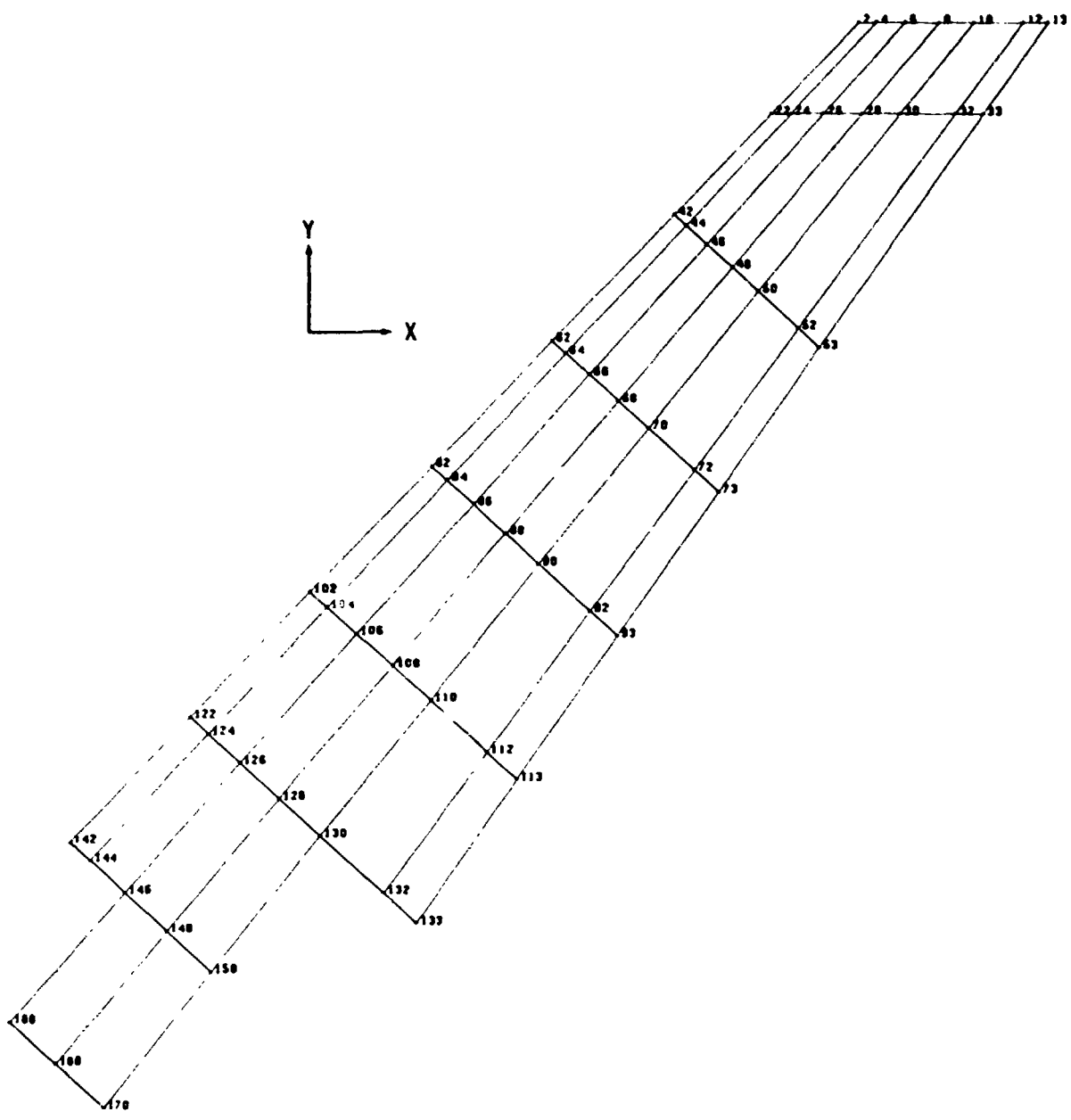


Figure 205-3. Wing Upper Surface Model, FIREBEE Drone



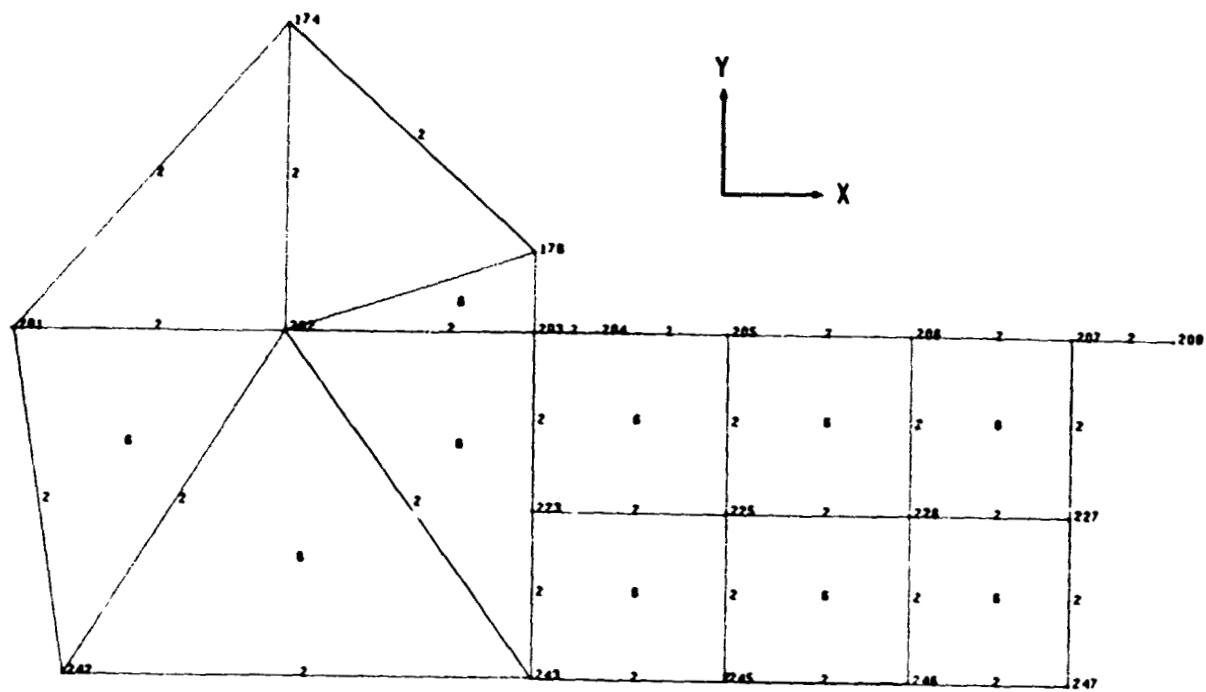


Figure 205-5. Wing-Body Intersection Model, FIREBEE Drone

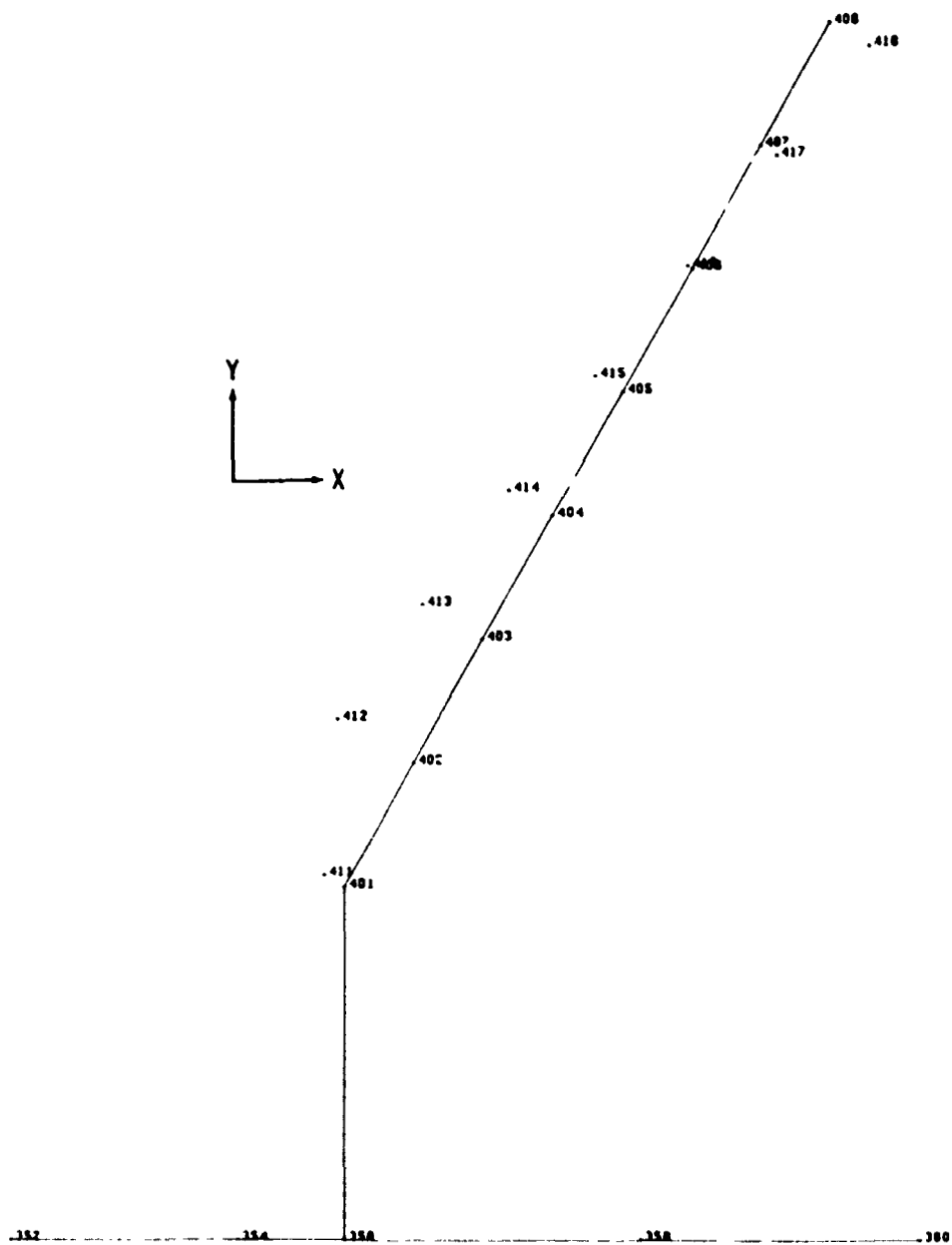


Figure 205-6. Horizontal Tail Model, FIREBEE Drone

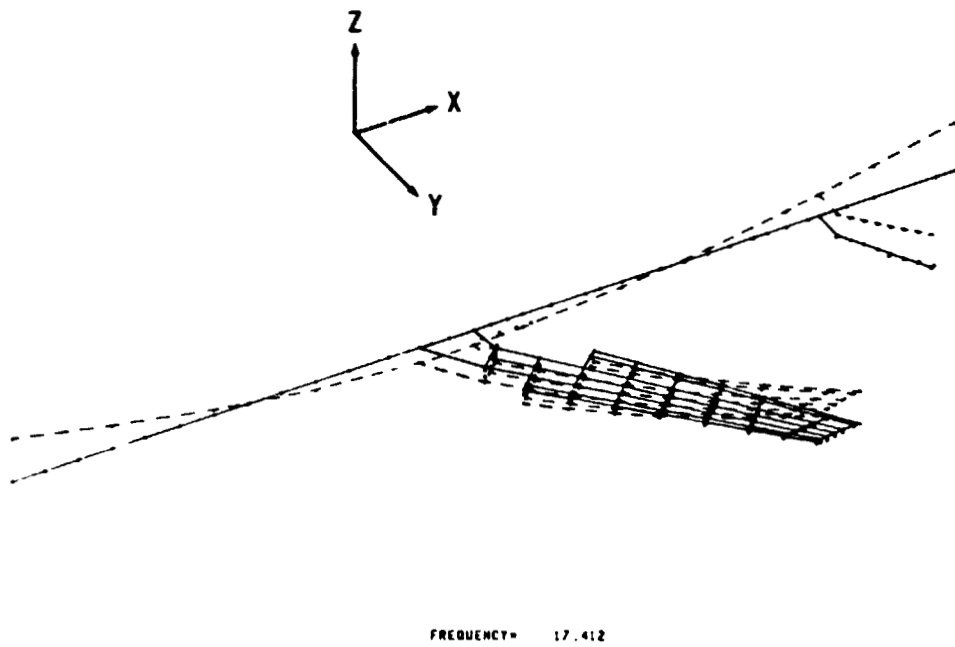
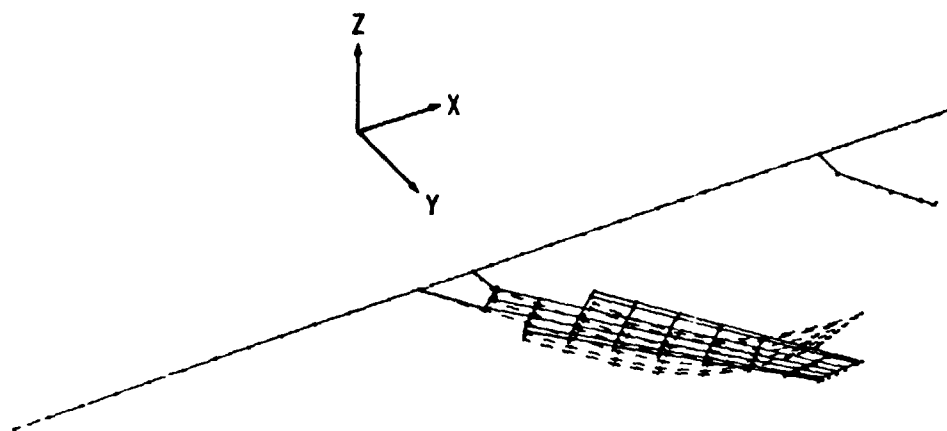


Figure 205-7. Fourth Mode Shape, FIREBEE Drone



FREQUENCY= 48.154

Figure 205-8. Sixth Mode Shape, FIREBEE Drone

206. BEAM VIBRATION (DECK 8)

206.1 DESCRIPTION OF ANALYSES

This problem demonstrates the various ATLAS mass matrix generation capabilities by using models of two cantilever beams:

- A beam with a straight elastic axis, uniform stiffness properties and concentrated masses offset from the elastic axis
- A beam of constant width and linearly varying depth along its span

206.1.1 Beam with Offset Concentrated Masses

The stiffness of this structure is modelled in two ways, both employing BEAM stiffness finite elements and concentrated masses:

- Structural nodes are located at the concentrated mass locations and the BEAMS are offset to the elastic axis. This model, SET 1, is shown in figure 206-1
- Structural nodes are located along the elastic axis and the concentrated masses are offset. This model, SET 2, is shown in figure 206-2

Four different mass matrices are calculated for each of these stiffness models and a normal mode analysis performed with each. The mass matrices used are:

- Guyan reduced mass matrix considering only the concentrated masses
- Guyan reduced mass matrix considering only the mass of the stiffness model
- Guyan reduced mass matrix considering both concentrated masses and stiffness element mass
- Reduced mass matrices produced directly by the Mass Processor considering only the concentrated masses

In all cases the retained freedoms are the translation in the Z-direction and rotations about the X and Y axes.

206.1.2 Tapered Beam

The structure analyzed is shown in figure 206-3. The stiffness of the structure is modelled in two ways: (1) with BEAM elements and (2) with 20-node BRICK elements.

The BEAM model, SET 3, is shown in figure 206-4. Three different mass matrices are calculated using the mass of the stiffness elements and normal mode analyses performed. The mass matrices used are:

- Guyan reduced mass matrix
- Diagonal mass matrix produced directly by the Mass Processor
- Nondiagonal mass matrix produced directly by the Mass Processor

For all three analyses the retained degrees of freedom are translation in the Z-direction and rotation about the Y axis.

The BRICK model, SET 4, is shown in figure 206-5. The mass matrix is obtained by Guyan reduction from the merged consistent elemental matrices. The retained degrees of freedom are the X- and Z-direction translations at the BRICK corner nodes.

206.2 RESULTS

206.2.1 Beam with Offset Concentrated Masses

First mode frequencies for the eight vibration analyses are presented in table 206-1. It can be seen that, as expected, identical results are obtained from SET 1 and SET 2 when the same procedure is used to generate the mass matrix. Frequencies for the beam without concentrated masses are compared with exact values in table 206-2. The fourth mode shape for this case is compared with the exact shape in figure 206-6. Exact values for frequency and mode shape were obtained using the methods of reference 206-1.

206.2.2 Tapered Beam

Frequencies obtained from the three BEAM element analyses and the BRICK element analysis are compared with exact values given in reference 206-2 in table 206-3. The mode shape for the third mode is shown in figure 206-7 for the BEAM element stiffness model and Guyan reduced mass matrix.

206.3 LISTING OF CONTROL PROGRAM AND DATA

```

BEGIN CONTROL PROGRAM DEM008
PROBLEM IDIDEM008 - VIBRATION ANALYSES WITH VARIOUS MASS MATRICES)

C
C PURPOSE      THE PRINCIPAL CAPABILITIES DEMONSTRATED BY THIS
C              DECK ARE
C              1. DIAGONAL REDUCED MASS MATRIX GENERATED BY
C                 MASS PROCESSOR
C              2. NON-DIAGONAL REDUCED MASS MATRIX GENERATED
C                 BY MASS PROCESSOR
C              3. GUYAN-REDUCED MASS MATRIX
C              4. VIBRATION ANALYSES USING BOTH REDUCED
C                 STIFFNESS AND REDUCED FLEXIBILITY MATRICES
C
C AUTHOR      F. P. GRAY
C
C CORE        130K (OCTAL)
C
C READ INPUT
C
C UNIFORM BEAM WITH OFFSET MASSES
C
C PRINT INPUT(NODAL)
C PRINT INPUT(STIFFNESS)
C PRINT INPUT(MASS)
C EXECUTE EXTRACT(EXNAME=SET1,LSUB=KGRID,ESUB=E1,NSUB=N1)
C EXECUTE GRAPHICS(GNAME=GEOM,OFFLINE=CALCOMP,VIEW=100,TYPE=ORTH,
X      SIZE=(20.,20.),LABEL=N+E,EXNAME=SET1)
C
C GUYAN REDUCED MASS MATRIX, STIFFNESS ELEMENTS ONLY
C
C PERFORM REDUCE(SET=1)
C PRINT INPUT(BC)
C EXECUTE VIBRATION(STIF=KRED,MASS=MRED,NFREQS=10,SET=1)
C PRINT OUTPUT(VIBRATION)
C PRINT INPUT(NODAL,SET=2)
C PRINT INPUT(STIFFNESS,SET=2)
C PRINT INPUT(MASS,SET=2)
C EXECUTE EXTRACT(EXNAME=SET2,LSUB=KGRID,KSET=2,ESUB=E1,NSUB=N1)
C EXECUTE GRAPHICS(GNAME=GEOM,VZ=-1,TYPE=ORTH,LABEL=N+E,
X      SIZE=(20.,20.),EXNAME=SET2)
C PERFORM REDUCE(SET=2)
C PRINT INPUT(BC,SET=2)
C EXECUTE VIBRATION(STIF=KRED,MASS=MRED,NFRECS=10,SET=2,VSET=2,
X      SUBSETS=N2)
C PRINT OUTPUT(VIBRATION,VSET=2)
C EXECUTE EXTRACT(EXNAME=MODE4,LSUB=VMODE,VSET=2,NSUB=N2,MODE=4,
X      SUB=ON1)
C EXECUTE GRAPHICS(GNAME=MODES,TYPE=ORTH,VECTORZ=VMODE,SCALE=0.1,
X      VSCALE=15,VX=5,VY=-70,EXNAME=MODE4)
C
C SAME ANALYSIS USING REDUCED FLEXIBILITY MATRIX
C
C EXECUTE CHOLSKY(IDECD,KRED=DKRED)
C EXECUTE CHOLSKY(IFOR,DKRED,DFRED)
C EXECUTE MULTIPLY(FRED=(DFRED(T)*DFRED))
C EXECUTE VIBRATION(FLEX=FRED,MASS=MRED,NFREQS=10,SET=2,VSET=2)
C PRINT OUTPUT(VIBRATION,VSET=2)
C PURGE FILES(MASSRNF)
C
C GUYAN REDUCED MASS MATRIX, CONCENTRATED MASSES ONLY

```

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C
PERFORM REDUCE(SET=1,[4]=[4,STIFELEM=0],
1 [MASS]=[MASS,CONMASS=1])
EXECUTE VIBRATION(STIF=KRED,MASS=MRED,NFREQS=10,SET=1)
PRINT OUTPUT(VIBRATION)
PERFORM REDUCE(SET=2,[4]=[4,STIFELEM=0],
1 [MASS]=[MASS,CONMASS=1])
EXECUTE VIBRATION(STIF=KRED,MASS=MRED,NFREQS=10,SET=2,VSET=2)
PRINT OUTPUT(VIBRATION,VSET=2)
PURGE FILES(MASSRNF)

C
C GUYAN REDUCED MASS MATRIX, STIFFNESS ELEMENTS + CONCENTRATED MASS
C
PERFORM REDUCE(SET=1,[MASS]=[MASS,CONMASS=1])
EXECUTE VIBRATION(STIF=KRED,MASS=MRED,NFREQS=10,SET=1)
PRINT OUTPUT(VIBRATION)
PERFORM REDUCE(SET=2,[MASS]=[MASS,CONMASS=1])
EXECUTE VIBRATION(STIF=KRED,MASS=MRED,NFREQS=10,SET=2,VSET=2)
PRINT OUTPUT(VIBRATION,VSET=2)
PURGE FILES(MASSRNF)

C
C DIAGONAL MASS MATRIX, CONCENTRATED MASSES ONLY
C
PERFORM K-REDUCE
EXECUTE MASS(SET=1,OPTION=2)
EXECUTE VIBRATION(STIF=KRED,MASS=MDC001A,NFREQS=10,SET=1)
PRINT OUTPUT(VIBRATION)

C
C NON-DIAGONAL MASS MATRIX, CONCENTRATED MASSES ONLY
C
PURGE FILES(MASSRNF)
PERFORM K-REDUCE(SET=2)
EXECUTE MASS(SET=2,OPTION=3)
EXECUTE VIBRATION(STIF=KRED,MASS=MDC001B,NFREQS=10,SET=2,VSET=2)
PRINT OUTPUT(VIBRATION,VSET=2)

C
C T A P E R E D B E A M
C
C BEAM ELEMENTS - GUYAN REDUCED MASS MATRIX
C
PRINT INPUT(NODAL,SET=3)
PRINT INPUT(STIFFNESS,SET=3)
EXECUTE EXTRACT(EXNAME=SET3,LSUB=KGRID,KSET=3,ESUB=E1,NSUB=N1)
EXECUTE GRAPHICS(GNAME=GEOM,VIEW=100,TYPE=LRT, LABEL=N,
X SIZE=(20.,20.),EXNAME=SET3)
PERFORM REDUCE(SET=3)
PRINT INPUT(BC,SET=3)
EXECUTE VIBRATION(STIF=KRED,MASS=MRED,NFREQS=10,SET=3,VSET=3)
PRINT OUTPUT(VIBRATION,VSET=3)

C
C BEAM ELEMENTS - DIAGONAL MASS MATRIX
C
EXECUTE MASS(SET=3,OPTION=2)
EXECUTE VIBRATION(STIF=KRED,MASS=MDC001C,NFREQS=10,SET=3,VSET=3)
PRINT OUTPUT(VIBRATION,VSET=3)

C
C BEAM ELEMENTS - NON-DIAGONAL MASS MATRIX
C
EXECUTE MASS(SET=3,OPTION=3)
EXECUTE VIBRATION(STIF=KRED,MASS=MDC001C,NFREQS=10,SET=3,VSET=3)
PRINT OUTPUT(VIBRATION,VSET=3,NOGSTIF,NOGMAS)
EXECUTE EXTRACT(EXNAME=MODE3,LSUB=VMODE,VSET=3,MODE=3,BSUB=ON1)
EXECUTE GRAPHICS(GNAME=MODES,TYPE=ORTH,VIEW=1000,VECTOR2=VMODE,
X SCALE=0.1,VSCALE=25.,EXNAME=MODE3)

C
C BRICK ELEMENTS - GUYAN REDUCED MASS MATRIX
C
PRINT INPUT(NODAL,SET=4)
PRINT INPUT(STIFFNESS,SET=4)
EXECUTE EXTRACT(EXNAME=SET4,LSUB=KGRID,KSET=4,ESUB=E1,NSUB=N1)
EXECUTE GRAPHICS(GNAME=GEOM,TYPE=ORTH,LABEL=E,SIZE=(20,20),
X RZ=60,RX=0,RY=30,EXNAME=SET4)

```

```

PERFORM REDUCE(SET=4)
PRINT INPUT(BC,SET=4)
EXECUTE VIBRATION(STIF=KRED,MASS=MRED,NFREQS=10,SET=4,VSET=99)
PRINT OUTPUT(VIBRATION,VSET=99)
CALL PRNTCAT
INDEX FILES(DATARNF,"IBRRNF)
END

```

```

*/
*/
*/ UNIFORM BEAM WITH OFFSET MASSES
*/
*/ STRUCTURAL NODES AT CONCENTRATED MASS LOCATIONS
*/
BEGIN NODAL DATA /
1 0. 0. 0. TO 15 70. 5. 0. /
21 0. 8. 0. /
22 4. 7. 0. /
23 11. 7. 0. /
24 17. 4. 0. /
25 23. 6. 0. /
26 26. 4. 0. /
27 31. 3. 0. /
28 34. 7. 0. /
29 39. 6. 0. /
30 47. 4. 0. /
31 51. 3. 0. /
32 54. 2. 0. /
33 60. 4. 0. /
34 66. 6. 0. /
35 71. 6. 0. /
END NODAL DATA /
BEGIN STIFFNESS DATA /
BEGIN ELEMENT DATA /
BEAM 21 22 1 2 1. 0. 0. .15 .15 .20 TO 34 35 14 15 /
END ELEMENT DATA /
END STIFFNESS DATA /
BEGIN MASS DATA /
BEGIN CONDITION DATA /
STAGE 1 CONDITION 1 0 0 1 /
END CONDITION DATA /
BEGIN CONCENTRATED MASS DATA 1 /
21 1.0 *3 /
22 2.5 4. 4. 4. /
*13 1 -.1 *3 /
END CONCENTRATED MASS DATA /
END MASS DATA /
BEGIN BC DATA /
SUPPORT TX TY TZ RX RY RZ FOR 21 /
RETAIN TZ RX RY FOR 22 TO 35 /
END BC DATA /
*/
*/ STRUCTURAL NODES ALONG ELASTIC AXIS
*/
BEGIN NODAL DATA /
SET 2 /
1 0. 0. 0. TO 15 70. 5. 0. /
21 0. 8. 0. /
22 4. 7. 0. /
23 11. 7. 0. /
24 17. 4. 0. /
25 23. 6. 0. /
26 26. 4. 0. /
27 31. 3. 0. /

```



```

28 34. 7. 0. /
29 39. 6. 0. /
30 47. 4. 0. /
31 51. 3. 0. /
32 54. 2. 0. /
33 60. 4. 0. /
34 66. 6. 0. /
35 71. 6. 0. /
END NODAL DATA /
BEGIN STIFFNESS DATA /
SET 2 /
BEGIN ELEMENT DATA /
BEAM 1 2 1.0 0. 0. .15 .15 .20 TO 14 15 /
END ELEMENT DATA /
END STIFFNESS DATA /
BEGIN MASS DATA /
SET 2 /
BEGIN CONDITION DATA /
STAGE 1 CONDITION 1 0 0 1 /
END CONDITION DATA /
BEGIN CONCENTRATED MASS DATA 1 /
1 21 1.0 *3 /
2 22 2.5 4. 4. 4. /
**13 1 1 -.1 *3 /
END CONCENTRATED MASS DATA /
END MASS DATA /
BEGIN BC DATA /
SET 2 /
SUPPORT TX TY TZ RX RY RZ FOR 1 /
RETAIN TZ RX RY FOR 2 TO 15 /
END BC DATA /
*/
*/
*/ T A P E R E D B E A M
*/
*/ BEAM ELEMENT MODEL
*/
BEGIN NODAL DATA /
SET 3 /
100 0. 0. 0. 0. TO 120 100. 0. 0. /
END NODAL DATA /
BEGIN STIFFNESS DATA /
SET 3 /
BEGIN ELEMENT DATA /
BEAM 100 101 10. 0. 0. 0. 0. 83.3333 9.6 0. 0. 0. 0. 73.728 /
101 102 9.6 *4 73.728 9.2 *4 64.6907 /
* 102 103 9.2 *4 64.6907 8.8 *4 56.7893 /
* 103 104 8.8 *4 56.7893 8.4 *4 49.5920 /
* 104 105 8.4 *4 49.5920 8.0 *4 42.6667 /
* 105 106 8.0 *4 42.6667 7.6 *4 36.5813 /
* 106 107 7.6 *4 36.5813 7.2 *4 31.1041 /
* 107 108 7.2 *4 31.1040 6.8 *4 26.2027 /
* 108 109 6.8 *4 26.2027 6.4 *4 21.8453 /
* 109 110 6.4 *4 21.8453 6.0 *4 18.0000 /
* 110 111 6.0 *4 18.0000 5.6 *4 14.6347 /
* 111 112 5.6 *4 14.6347 5.2 *4 11.7173 /
* 112 113 5.2 *4 11.7173 4.8 *4 9.216 /
* 113 114 4.8 *4 9.216 4.4 *4 7.0987 /
* 114 115 4.4 *4 7.0987 4.0 *4 5.3333 /
* 115 116 4.0 *4 5.3333 3.6 *4 3.8880 /
* 116 117 3.6 *4 3.8880 3.2 *4 2.7307 /
* 117 118 3.2 *4 2.7307 2.8 *4 1.8293 /
* 118 119 2.8 *4 1.8293 2.4 *4 1.1520 /
* 119 120 2.4 *4 1.1520 2.0 *4 .6667 /
END ELEMENT DATA /
END STIFFNESS DATA /
BEGIN BC DATA /
SET 3 /
RETAIN TZ RY FOR 102 TO 120 BY 2 /
SUPPORT TX TY TZ RX RY RZ FOR 100 /
END BC DATA /
BEGIN MASS DATA /
SET 3 /

```

```

BEGIN CONDITION DATA /
STAGE 1 CONDITION 1 /
END CONDITION DATA /
END MASS DATA /
*/
*/ BRICK ELEMENT MODEL /
*/
BEGIN NODAL DATA /
SET 4 /
REC JUNK 1. 0. 0. 2. 0. 0. 0. 0. 1. /
100 0. -.5 5. TO 120 100. -.5 1. /
200 0. .5 5. TO 220 100. .5 1. /
300 0. .5 -5. TO 320 100. .5 -1. /
400 0. -.5 -5. TO 420 100. -.5 -1. /
500 0. 0. 5. TO 510 100. 0. 1. /
600 0. .5 0. TO 610 100. .5 0. /
700 0. 0. -5. TO 710 100. 0. -1. /
800 0. .5 0. TO 810 100. -.5 0. /
END NODAL DATA /
BEGIN STIFFNESS DATA /
SET 4 /
BEGIN ELEMENT DATA /
BRICK 100 200 300 400 102 202 302 402 500 600 700 800
      501 601 701 801 101 201 301 401 /
**9 0 2 **7 1 **7 2 **3 /
END ELEMENT DATA /
END STIFFNESS DATA /
BEGIN BC DATA /
SET 4 /
ORDER RETAIN BY INTERNALID /
RETAIN TX TZ FOR 102 TO 120 BY 2 /
**3 0 **3 100 0 100 0 0 /
SUPPORT TX TY TZ RX RY RZ FOR 100 TO 800 BY 100 /
SUPPORT TY FOR 100 TO 1000 /
END BC DATA /
BEGIN SUBSET DEFINITION
SUBSETS OF STIFFNESS SET 1
N1 = ALL
E1 = ALL
SUBSETS OF STIFFNESS SET 2
N1 = ALL
E1 = ALL
N2 = 1 TO 15
ON1 = 2 TO 15
SUBSETS OF STIFFNESS SET 3
N1 = ALL
E1 = ALL
ON1 = 102 TO 120 BY 2
SUBSETS OF STIFFNESS SET 4
N1 = ALL
E1 = ALL
END SUBSET DEFINITION
END PROBLEM DATA /

```

**Table 206-1. First Mode Frequencies for
Uniform Beam with Offset Masses**

Mass Matrix		Stiffness Model	
		SET 1	SET 2
Guyan Reduced Matrix	Concentrated masses only	5.518 179	5.518 179
	Stiffness elements only	10.182 41	10.182 41
	Concentrated masses + Stiffness elements	4.852 565	4.852 565
Concentrated masses only produced by Mass Processor		5.518 179	5.518 179

Frequencies in Hertz

**Table 206-2. Natural Frequencies of
Uniform Beam without Concentrated
Masses**

(1) Mode No.	Frequency (Hertz)		(4) Difference
	(2) Exact	(3) ATLAS	$\frac{(3)-(2)}{(2)} \times 100$ (%)
1	10.181 5	10.182 4	0.0
2	63.806 4	63.584 6	-0.3
3	178.660	176.658	-1.1
4	350.104	341.924	-2.3

Table 206-3. Natural Frequencies of Tapered Beam

Stiffness Model	Mass Matrix	Frequency (Hertz)					
		Mode 1 $f_{\text{exact}} = 39.5196$		Mode 2 $f_{\text{exact}} = 144.931$		Mode 3 $f_{\text{exact}} = 339.566$	
		ATLAS	%Error	ATLAS	%Error	ATLAS	%Error
BEAM	Diagonal Lumped	39.1177	-1.0	138.441	-4.5	307.584	-9.4
BEAM	Non-Diagonal Lumped	39.5951	0.2	144.394	-0.4	332.875	-2.0
BEAM	Guyan	39.5294	0.0	144.566	-0.3	336.253	-1.0
BRICK	Guyan	41.4888	6.2	150.553	3.9	347.329	2.3

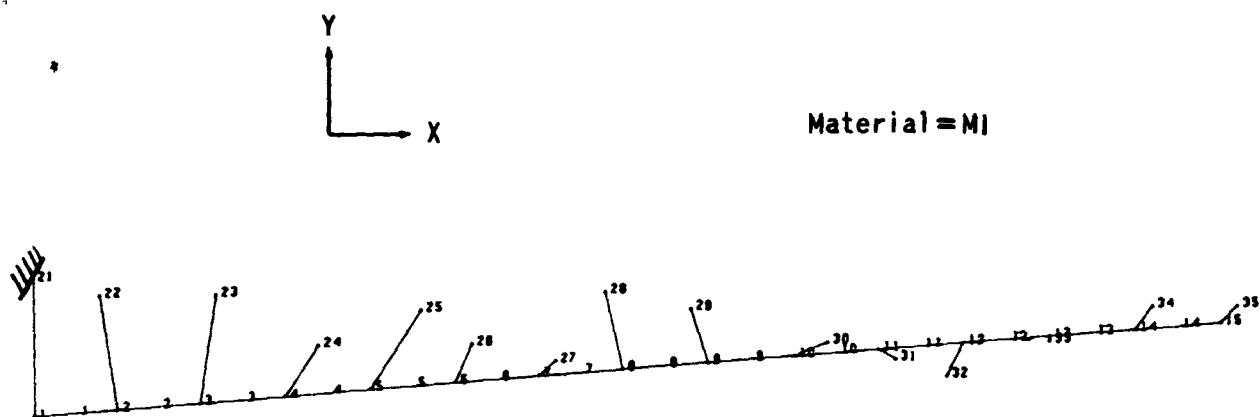


Figure 206-1. Beam Model with Structural Nodes at Concentrated Mass C.G.'s (SET 1)

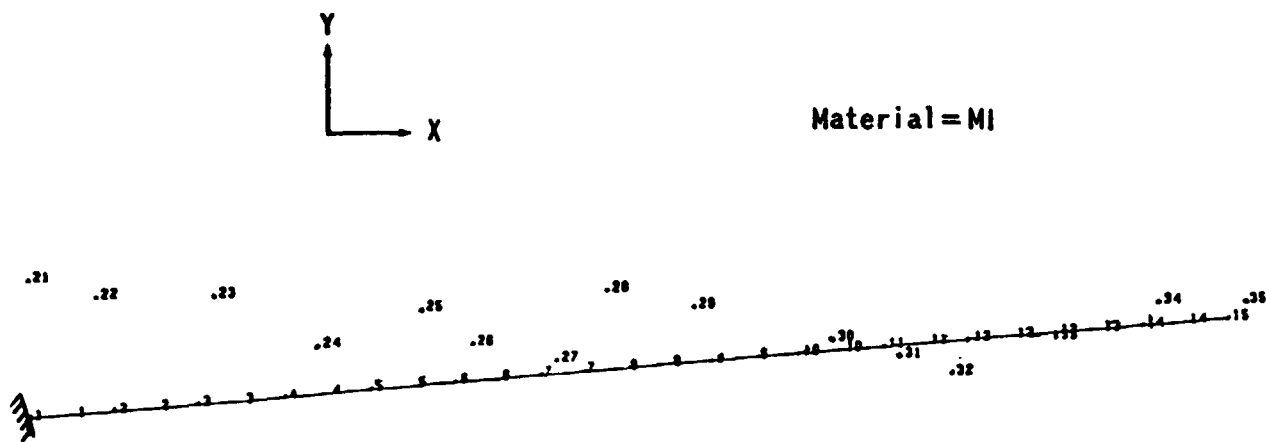


Figure 206-2. Beam Model with Structural Nodes at Elastic Axis (SET 2)

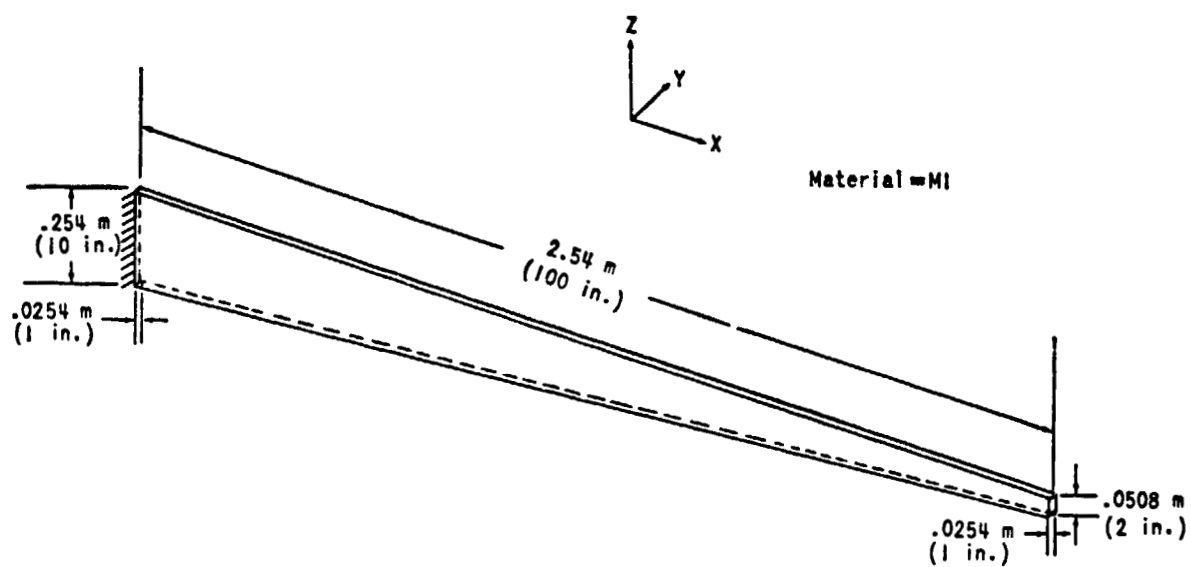


Figure 206-3. Tapered Beam

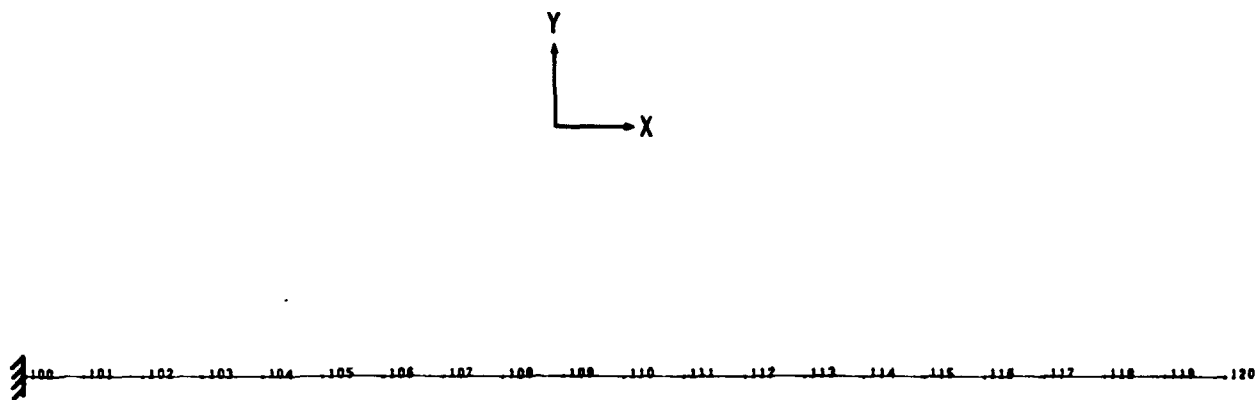


Figure 206-4. BEAM Element Model of Tapered Beam (SET 3)

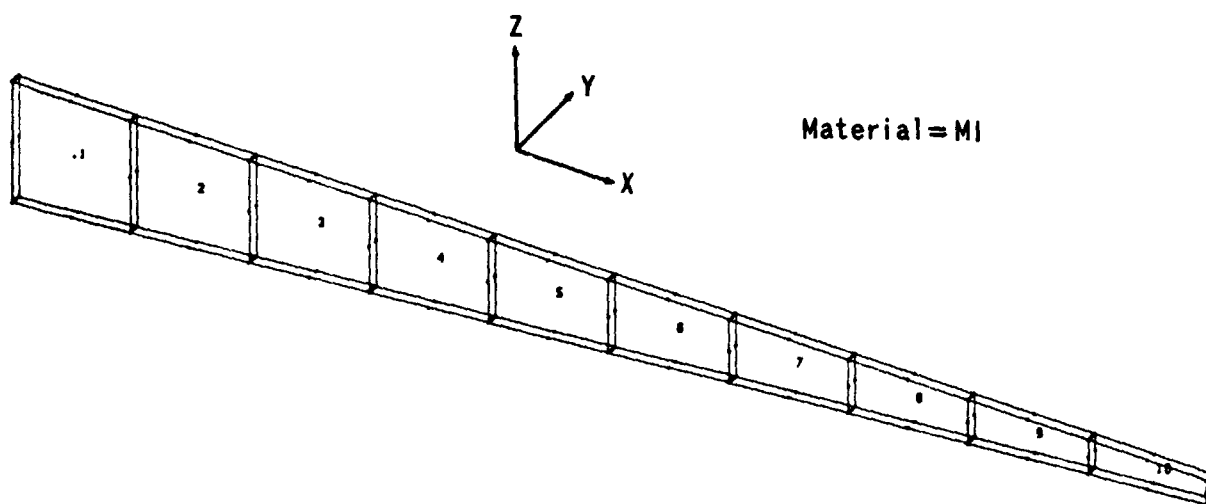


Figure 206-5. BRICK Element Model of Tapered Beam (SET 4)

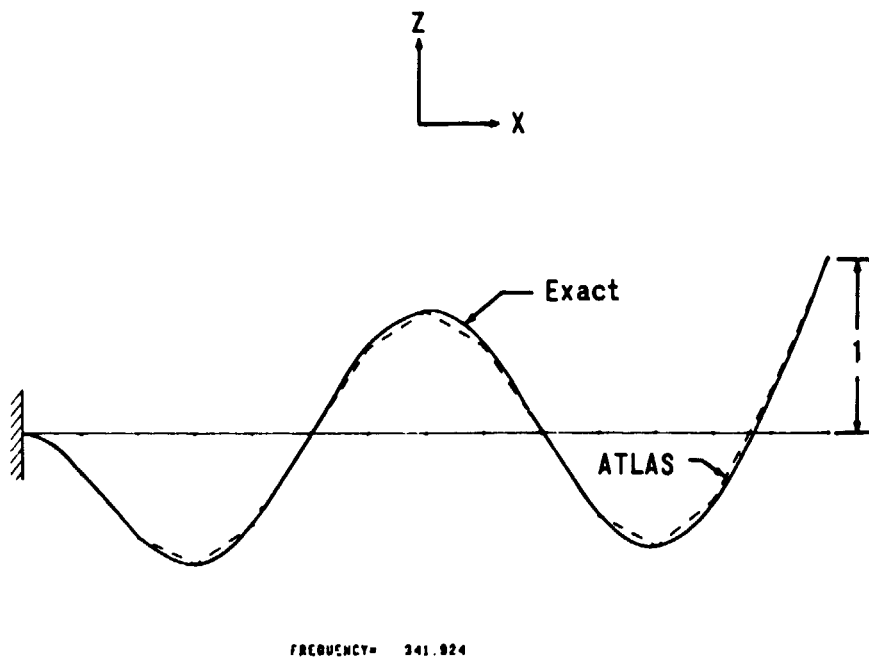


Figure 206-6. Fourth Mode Shape, Uniform Beam without Concentrated Masses (SET 2)

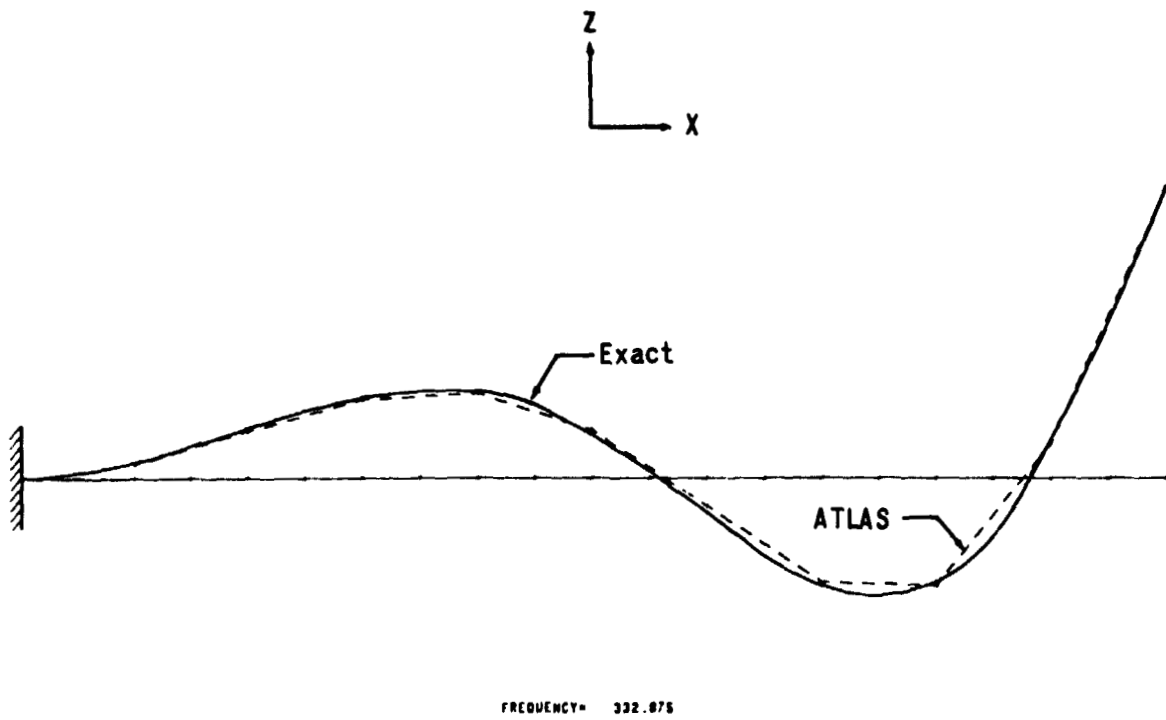


Figure 206-7. Third Mode Shape, Tapered Beam (SET 3)

207. BUCKLING AND SUPERPOSITION (DECK 13)

207.1 DESCRIPTION OF ANALYSES

Two separate analyses are performed in this demonstration problem. The first is a buckling analysis and the second is a stress analysis demonstrating the ATLAS superposition capability.

Buckling loads are calculated for a plane frame with equal concentrated loads at the column tops. The model and loading are shown in figure 207-1. Translations in the X and Y-directions and rotation about the Z axis are retained at all nodes except where a freedom is supported.

Superposition is demonstrated by performing a stress analysis of the structure in figure 207-1 loaded as shown in figure 207-2 in two ways. The first analysis is performed using the total model and total loads as shown in figure 207-2. The second analysis takes advantage of the symmetry of the structure. SET 2 is defined as shown in figure 207-3. STAGE 1 is defined to have symmetry on section A-A with the symmetric load components applied. STAGE 2 is defined to have antisymmetry on section A-A with the antisymmetric load components applied. The total solution is obtained by adding 5 times the solution from STAGE 1 to 2 times the solution from STAGE 2.

In addition to the two analysis capabilities described a this problem is used to demonstrate the capability to produce graphs of element stress vs. load case and plots of displacements. Four loadcases were added to SET 1 to demonstrate stress vs. loadcase graphs (BEAM1, BEAM2, BEAM3 and BEAM4). These cases consist of distributed loading along part or all of the horizontal beam. To demonstrate displacement plots loadcase MOVE1 was added. This case consists of a unit displacement in the X-direction at node 1.

207.2 RESULTS

Critical buckling loads for the first six modes were calculated and are presented in table 207-1. Also presented are analytical solutions obtained using the techniques of reference 207-1. The buckled shape for the third mode is shown in figure 207-4 along with the shape obtained using the techniques of reference 207-1.

Nodal displacements and element stresses calculated by superimposing STAGES 1 and 2 of SET 2 are identical to those calculated from SET 1 within the accuracy of the computer.

Figure 207-5 presents a graph of bending moment at the left end of the beam vs. loadcase for loadcases BEAM1 through BEAM4.

Displacements due to motion of the left support are shown in figure 207-6.

207.3 LISTING OF CONTROL PROGRAM AND DATA

```

BEGIN CONTROL PROGRAM DEMO13
PROBLEM 1010EM013 - BUCKLING AND SUPERPOSITION)

C
C PURPOSE      THE PRINCIPAL CAPABILITIES DEMONSTRATED BY THIS
C              DECK ARE
C              1. BUCKLING
C              2. SUPERPOSITION
C              3. PLOTS OF BUCKLING MODE SHAPES
C              4. PLOTS OF STRESS VS. LOADCASE
C              5. PLOTS OF STATIC DISPLACEMENTS
C
C AUTHOR      R. A. SAMUEL
C
C CORE      130K (OCTAL)
C
READ INPUT(MODE2)
PRINT INPUT(NODAL)
PRINT INPUT(STIFFNESS)
PRINT INPUT(NODAL,SET=2)
PRINT INPUT(STIFFNESS,SET=2)
EXECUTE EXTRACT(EXNAME=TOTAL,LSUB=KGRID,ESUB=E1,NSUB=N1)
EXECUTE GRAPHICS(GNAME=GEOMETRY,OFFLINE=CALCOMP,VIEW=100,
X              TYPE=ORTH,LABEL=N+E,SIZE=(10,15),EXNAME=TOTAL)
EXECUTE EXTRACT(EXNAME=HALF,LSUB=KGRID,ESUB=E1,NSUB=N1,KSET=2)
EXECUTE GRAPHICS(GNAME=GEOMETRY,VIEW=100,TYPE=ORTH,LABEL=N+E,
X              SIZE=(10,15),EXNAME=HALF)
C
C BUCKLING AND STRESS ANALYSES
C              SET 1
C
PERFORM R-STRESS
PRINT INPUT(BC)
PRINT OUTPUT(LOADS,L2=L21)
PRINT OUTPUT(DISP)
PRINT OUTPUT(STRESS)
EXECUTE EXTRACT(EXNAME=BEAM4,LSUB=STRESS,LC=BEAM1 TO BEAM4,
X              ESUB=E2,NSUB=N1)
EXECUTE GRAPHICS(GNAME=MOMENT,TYPE=GRAPH,X=LC,Y1=8MMZ(1),
X              XMIN=1,XMAX=6,Y1MIN=0.,Y1MAX=40.,SIZE=(10,10),
X              EXNAME=BEAM4)
EXECUTE EXTRACT(EXNAME=DEFL,LSUB=DISGRID,ESUB=E1,NSUB=N1,
X              LC=MOVE1)
EXECUTE GRAPHICS(GNAME=DISPL,TYPE=ORTH,SCALE=.2,VIEW=100,
X              VECTOR2=DISP,VSCALE=1.,EXNAME=DEFL)
EXECUTE STIFFNESS(LC=COLMLO,BSET=1)
EXECUTE MERGEIGSTIF,BSET=1,KG22=22)
EXECUTE BUCKLING(STIF=KRED,KG=KG22,BSET=1)
PRINT OUTPUT(BUCKLING,BSET=1)
EXECUTE EXTRACT(EXNAME=MODE3,LSUB=BMODE,BSET=1,MODE=3,BSUB=ON1)
EXECUTE GRAPHICS(GNAME=BUCKLING,TYPE=ORTH,VIEW=100,
X              SCALE=.2,VECTOR2=BMODE,VSCALE=3.,
X              EXNAME=MODE3)
C
C STRESS ANALYSIS - SET 2
C              (SUPERPOSITION)
C
PURGE FILES(MERGRNF,MULTRNF,CHOLRNF)
PERFORM STRESS(SET=2)
PRINT INPUT(BC,SET=2,STAGE=1)
PRINT OUTPUT(LOADS,SET=2,L1=L11)
PURGE FILES(MERGRNF,MULTRNF,CHOLRNF)
PERFORM STRESS(SET=2,STAGE=2)
PRINT INPUT(BC,SET=2,STAGE=2)
PRINT OUTPUT(LOADS,SET=2,STAGE=2,L1=L11)

```

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EXECUTE STRESS(SET=2,SUBSTAGE=3)
PRINT OUTPUT(DISP,SET=2,STAGE=3)
PRINT OUTPUT(STRESS,SET=2,STAGE=3)
END CONTROL PROGRAM

```

```

BEGIN NODAL DATA
  SET 1 / COMPLETE MODEL
    1 0. 0. 0. TO 4 0. 12. 0.
    4 TO 8 24. 12. 0.
    8 TO 11 24. 0. 0.
    REORDER FROM -1
  SET 2 / HALF MODEL
    1 0. 0. 0. TO 4 0. 12. 0.
    4 TO 6 12. 12. 0.
    REORDER FROM -1
END NODAL DATA
BEGIN STIFFNESS DATA
  SET 1 / COMPLETE MODEL
  BEGIN ELEMENT DATA
    BEAM N1 1 2 11 10000. 11 TO N3 3 4 11
    BEAM N4 4 5 11 10000. 21 TO N7 7 8 11
    BEAM N8 8 9 1 10000. 1. TO N10 10 11 1
  END ELEMENT DATA
  SET 2 / HALF MODEL
  BEGIN ELEMENT DATA
    BEAM N1 1 2 6 10000. 11 TO N3 3 4 6
    BEAM N4 4 5 1 10000. 21 TO N5 5 6 1
  END ELEMENT DATA
END STIFFNESS DATA
BEGIN BC DATA
  SET 1 STAGE 1 / BC FOR BUCKLING AND STRESS ANALYSES
    SUPPORT TX TY FOR 1 11
    RETAIN TX TY RZ FOR 2 TO 10
    RETAIN RZ FOR 1 11
  SET 2 STAGE 1 / SYMMETRIC BC
    SUPPORT TX TY FOR 1
    SUPPORT ASYM IN SURFACE 1 THROUGH 6
  SET 2 STAGE 2 / ANTISYMMETRIC BC
    SUPPORT TX TY FOR 1
    SUPPORT SYMM IN SURFACE 1 THROUGH 6
END BC DATA
BEGIN LOADS DATA
  SET 1 STAGE 1
    LOAD CASE IC COLMLO **UNIT LOAD CONDITION FOR BUCKLING ANALYSIS*
    LOAD CASE ID TOTAL **LOAD CASE FOR SUPERPOSITION DEMONSTRATION*
    LOAD CASE ID BEAM1 **1 LB/INCH LOAD ON BEAM 4 *
    LOAD CASE ID BEAM2 **1 LB/INCH LOAD ON BEAMS 4 AND 5 *
    LOAD CASE ID BEAM3 **1 LB/INCH LOAD ON BEAMS 4, 5 AND 6 *
    LOAD CASE ID BEAM4 **1 LB/INCH LOAD ON BEAMS 4, 5, 6 AND 7*
    LOAD CASE ID MOVE1 **UNIT X DISPLACEMENT AT NODE 1*
  BEGIN NODAL LOAD DATA
    CASE COLMLO
      4 8 FY -1.
    CASE TOT*1
      4 FX 1. FY -3.
      8 FX -3. FY -7.
  END NODAL LOAD DATA
  BEGIN ELEMENT LOAD DATA
    DIRECTION 0. 1. 0.
    CASE BEAM1
      4 1.

```



```

CASE BEAM2
  4 5 1.
CASE BEAM3
  4 5 6 1.
CASE BEAM4
  4 TO 7 1.
END ELEMENT LOAD DATA
BEGIN SUPPORT DISPLACEMENT DATA
CASE MOVE1
  1 TX 1.
END SUPPORT DISPLACEMENT DATA
SET 2 STAGE 1
LOAD CASE ID SYMPART **SYMMETRIC PART OF LOADCASE TOTAL*
BEGIN NODAL LOAD DATA
CASE SYMPART
  4 FX .4 FY -1.
END NODAL LOAD DATA
SET 2 STAGE 2
LOAD CASE ID ASMPART **ANTISYMMETRIC PART OF LOADCASE TOTAL*
BEGIN NODAL LOAD DATA
CASE ASMPART
  4 FX -.5 FY 1.
END NODAL LOAD DATA
END LOADS DATA
BEGIN STRESS DATA
SET 2
  SUPSTAGE 3
    TOTAL 1 5. SYMPART , 2 2. ASMPART
  LOAD CASE ID TOTAL **SAME AS LOADCASE TOTAL IN SET 1 *
END STRESS DATA
BEGIN SUBSET DEFINITION
SUBSETS OF STIFFNESS SET 1
  E1 = ALL
  E2 = 4
  N1 = ALL
  ON1 = 1 *-10+1
SUBSETS OF STIFFNESS SET 2
  E1 = ALL
  N1 = ALL
END SUBSET DEFINITION
END PROBLEM DATA

```

**Table 207-1. Critical Load Values
for Plane Frame**

(1) Mode Number	(2) K Ref. 207-1)	(3) K (ATLAS)	(4) $\frac{(3)-(2)}{(2)} \times 100$ (%)
1	1.349 553	1.349 558	0.0
2	3.590 681	3.594 686	0.1
3	4.111 618	4.118 577	0.2
4	6.566 437	6.638 602	1.1
5	6.992 352	7.073 246	1.2
6	9.625 433	10.654 702	10.7

$$P_{cr} = \frac{K^2 EI}{l^2}$$

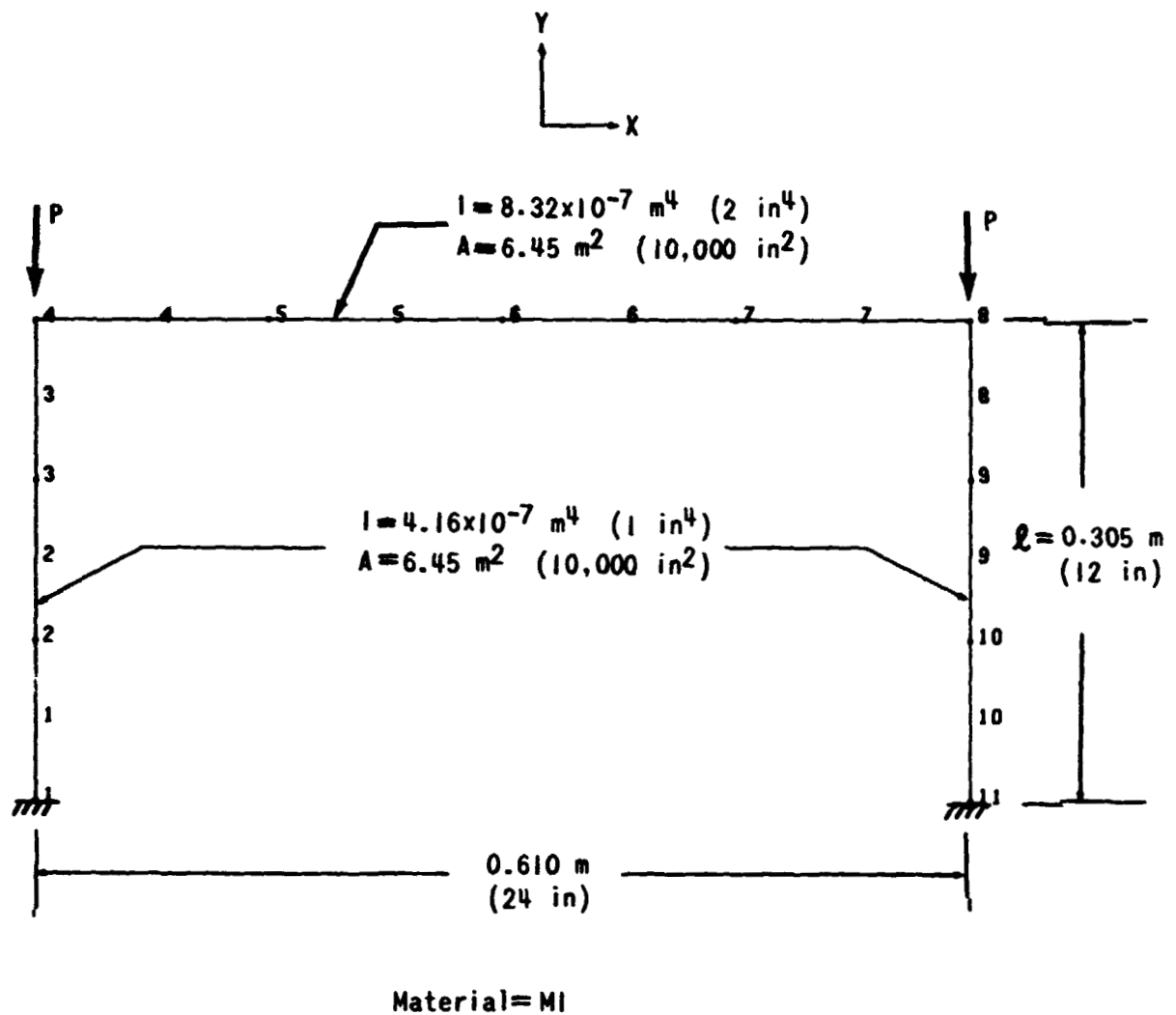


Figure 207-1. Structural Model and Loading for Buckling Analysis (SET 1)

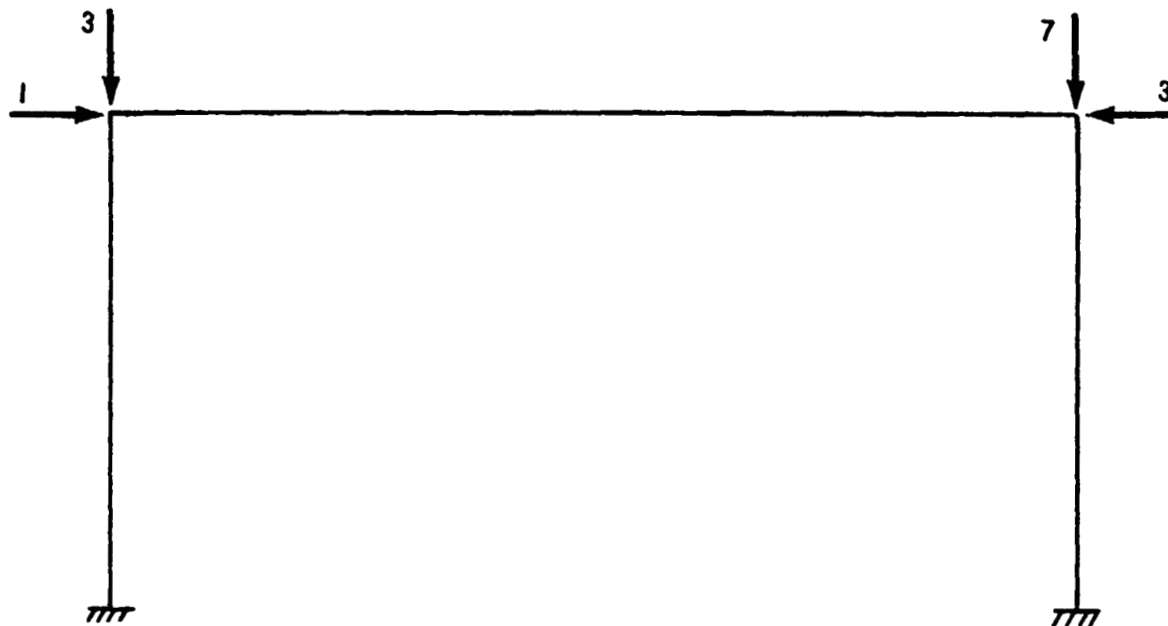


Figure 207-2. Loading for Superposition Demonstration

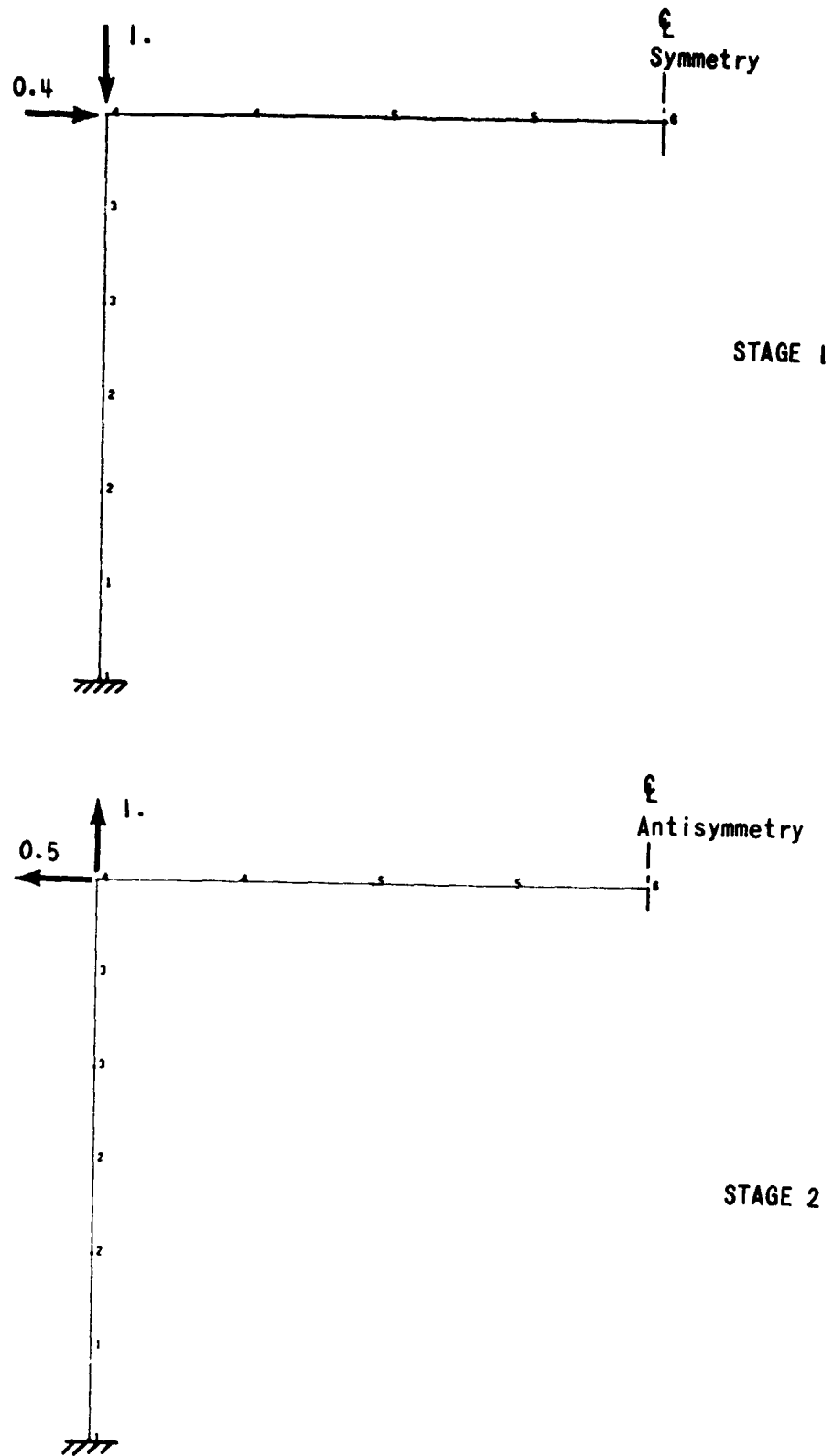


Figure 207-3. Half-Models for Superposition Demonstration (SET 2)

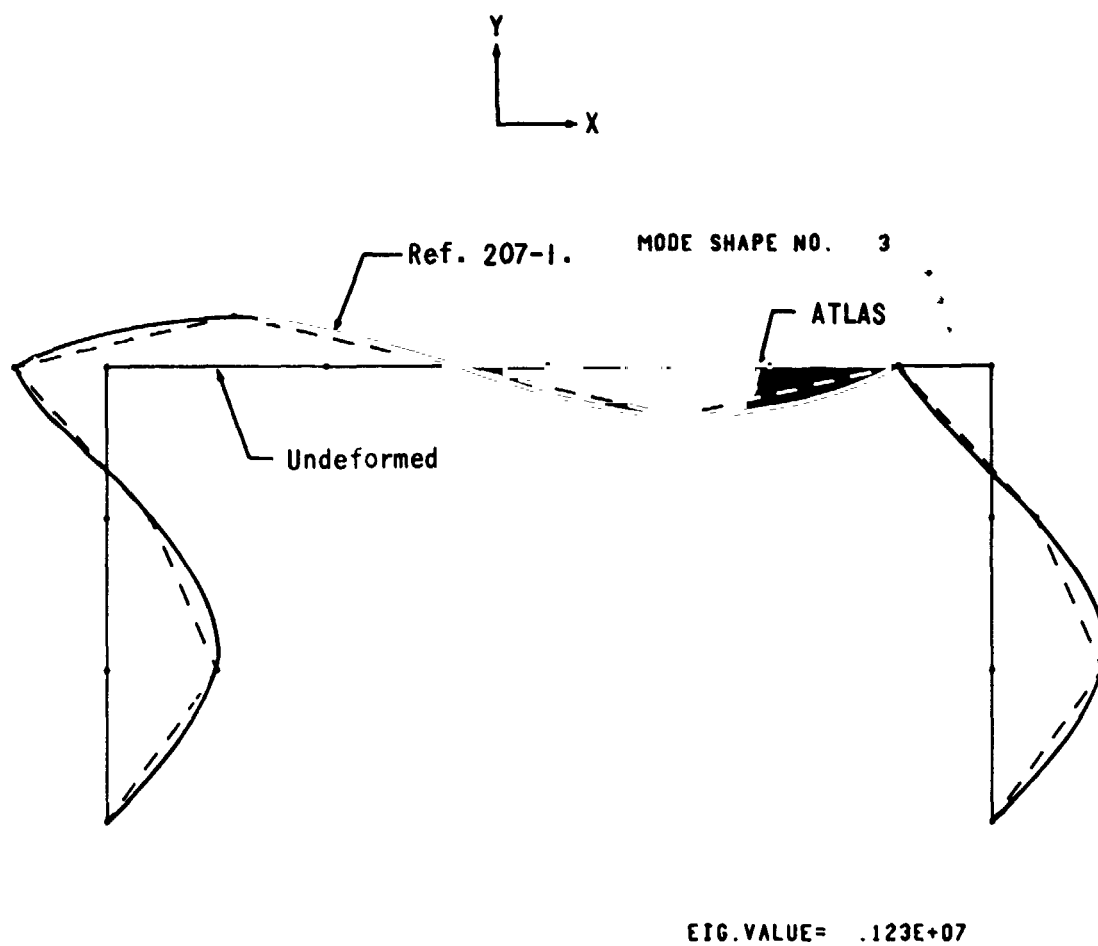


Figure 207-4. Buckled Shape for Third Mode of Frame

For Beam 4

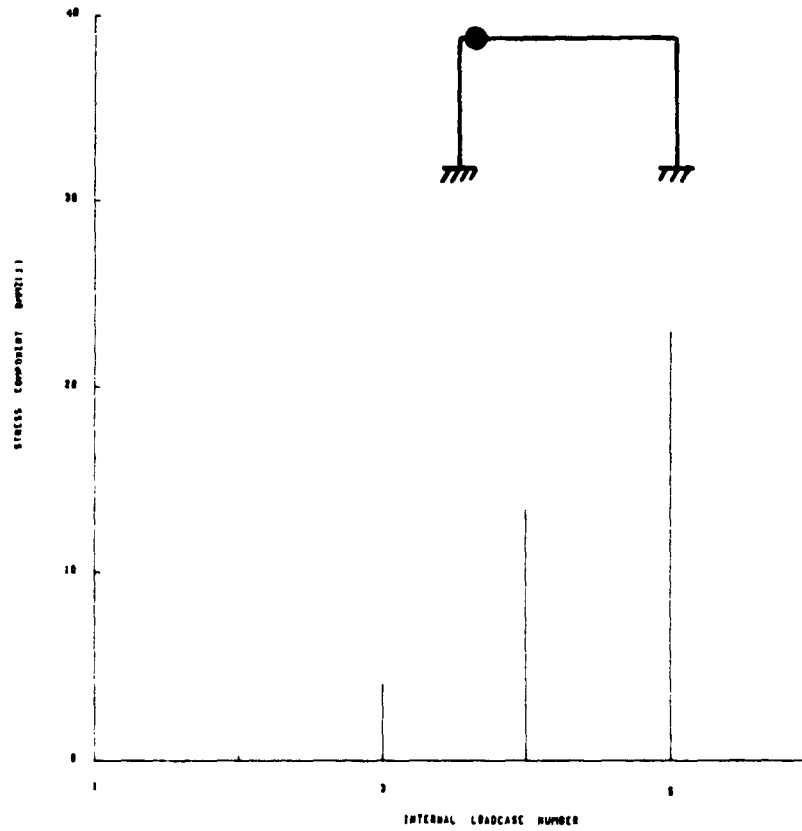


Figure 207-5. Bending Moment at End of Beam

Case BEAM4



Figure 207-6. Frame Displacements Due to Support Motion
(Loadcase MOVE1)

208. FUEL AND PAYLOAD MANAGEMENT (DECK 16)

208.1 DESCRIPTION OF ANALYSIS

This problem demonstrates the ATLAS capabilities for calculating weights based upon user specified management sequences for fuel and payload.

The mass model is shown in figure 208-1; no stiffness element model is used. Locations of the fuel tanks and body cargo holds are shown in figure 208-2. Passenger seating is two abreast in the half airplane model spaced at 1.02 m (40 in).

The first fuel management sequence is as follows:

- The tanks are loaded until not quite full such that the weight ratio of tanks 11 and 12 is 4:3 and tanks 21 and 22 is 1:1
- Fuel is used from tanks 11 and 12 in proportion to their weights until their total equals the total of tanks 21, 22 and 31
- All fuel in tank 12 is transferred to tank 11
- Fuel is used from tanks 11, 21 and 22 at rates in the ratio of 2:1:1 until the weight of fuel in tank 21 is 6803.9kg (15 000 lb)
- Fuel is used from tanks 11, 21 and 31 in rough proportion to their weights until all are empty

The second sequence loads all tanks until full to demonstrate the system's ability to calculate fuel capacities.

The payload sequence specifies that the cargo holds are partially loaded from the bottom with the forward hold being loaded before the aft hold. Passengers are loaded from each end.

In addition to the fuel and payload sequences described above, two loading sequences are defined for the purpose of generating a loadability diagram. In the first of these sequences passengers are loaded from fore to aft with all window seats loaded before any aisle seats. Cargo is also loaded from fore to aft. The second sequence is similar to the first except that loading occurs in the aft to forward direction.

208.2 RESULTS

The loadability diagram resulting from the last two loading sequences is shown in figure 208-3.

208.3 LISTING OF CONTROL PROGRAM AND DATA

```

C BEGIN CONTROL PROGRAM DEMO16
C PROBLEM ID( DEMO16 - FUEL AND PAYLOAD MANAGEMENT)
C
C PURPOSE      THE PRINCIPAL CAPABILITIES DEMONSTRATED BY THIS
C               DECK ARE
C               1. FUEL AND PAYLOAD MANAGEMENT
C               2. LOADABILITY DIAGRAM GENERATION
C
C AUTHOR       R. A. WOODWARD
C
C CORE        130K (OCTAL)
C
C READ INPUT
C PRINT INPUT(NODAL)
C PRINT INPUT(MASS)
C EXECUTE EXTRACT(EXNAME=MASSGRD,LSUB=MGRID,ESUB=E5,NSUB=1)
C EXECUTE GRAPHICS(GNAME=GEOM,OFFLINE=CALCOMP,TYPE=(ORTH,PULL),
X      SIZE=(20,20),RZ=30,RX=0,RY=20,EXNAME=MASSGRD)
C EXECUTE MASS (OPTION=1)
C PRINT OUTPUT (MASS,FUEL,TABLES,TANKS=22,PAYLOAD=22,MDC=MDC***A)
C EXECUTE EXTRACT(EXNAME=LOADAB,LSUB=LOADAB,PCOND=20,PCOND=30,
1      CCOND=20,CCOND=30,FCOND=15,FCOND=15)
C EXECUTE GRAPHICS(GNAME=LOADAB,SIZE=(10,10),
1      LWLNE=540000.,WTINC=20000.,FCGLNE=6.,LCGLNE=36.,
2      DATUM=21.,CGINC=3.,LEMAC=1600.,MAC=1100.,
3      FUEL FAC=2.,PASSFAC=2.,CARGOFAC=2.,CGTOL=1.,
4      OEW FAC=2.,EXNAME=LOADAB, TYPE=GRAPH)
C END CONTROL PROGRAM

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*/MODE2/
BEGIN NODAL DATA
1 20. 0. 1. TO 9 340. 0. 65. BY 2
101 20. 0. -1. TO 109 340. 0. -65. BY 2
201 20. 1. 0. TO 209 340. 65. 0. BY 2
11 420. 0. 65. TO 83 3300. 0. 65. BY 2
111 420. 0. -65. TO 189 3540. 0. -65. BY 2
211 420. 65. 0. TO 225 380. 65. 0. BY 2
265 2580. 65. 0. TO 277 3060. 65. 0. BY 2
287 3460. 65. 0. TO 289 3540. 65. 0. BY 2
*/ WING COORDINATES
227 1060. 65. 0. 26.25 TO 245 1780. 65. 0. 36.35 BY 2
245 TO 255 2180. 65. 0. 28.8 BY 2
255 TO 263 1500. 65. 0. 12.0 BY 2
327 1060. 65. 0. 26.25 TO 341 1620. 265. 0. 8.85 BY 2
445 1780. 195. 0. 22.65 TO 455 2180. 195. 0. 20.15 BY 2
541 1620. 265. 0. 8.85 TO 551 2205. 455. 0. 5.75 BY 2
651 2205. 455. 0. 5.75 TO 656 2545. 594. 0. 3.2
756 2545. 594. 0. 3.2 TO 760 2875. 765. 0. .95
760 TO 763 2995. 765. 0. 1.85
341 TO 355 2180. 255. 0. 20.15 BY 2
355 TO 363 2500. 265. 0. 11.25 BY 2
551 TO 559 2525. 455. 0. 10.0
559 TO 563 2685. 455. 0. 5.0
656 TO 659 2665. 594. 0. 4.85
659 TO 663 2825. 594. 0. 2.45
*/ HORIZONTAL TAIL
279 3140. 65. 0. 1.80
779 3140. 65. 0. 1.80 TO 979 3365. 200. 0. 1.25 BY 100
281 3220. 65. 0. 4.25
781 3220. 65. 0. 4.25 TO 981 3388. 200. 0. 1.75 BY 100
283 3300. 65. 0. 4.55
783 3300. 65. 0. 4.55 TO 983 3412. 200. 0. 1.80 BY 100
285 3380. 65. 0. 1.40
785 3380. 65. 0. 1.40 TO 985 3435. 200. 0. .80 BY 100
*/ VERTICAL TAIL
REC REC1 0. 0. 0. 1. 0. 0. 0. -1. 0.
85 3380. 65. 0. 3.25
87 3460. 65. 0. 2.40
1085 3460. 140. 0. 1.50
1087 3500. 140. 0. 1.80
*/ WING FIN
1156 2545. .1 -594. 2.40 TO 1356 2830. 100. -594. 1.80 BY 100
1158 2625. .1 -594. 2.40 TO 1358 2842. 100. -594. 1.90 BY 100
1161 2745. .1 -594. 2.80 TO 1361 2859. 100. -594. 1.95 BY 100
1163 2825. .1 -594. 2.80 TO 1363 2870. 100. -594. 2.05 BY 100
RESUME GLOBAL
89 3540. 0. 65.
*/ AIRLOAD PANEL NODES
*/ BODY
5100 0. 0. 0. TO 5112 3564. 0. 0.
5251 0. 26.1279 0.
5252 297. 26.1279 0.
5253 297. 63.5215 0.
5254 594. 63.5215 0.
5202 594. 65.1 0. TO 5212 3564. 65.1 0.
*/ WING
5400 741. 65.1 0. TO 5405 2715. 65.1 0.
5410 1017.7530 146.6 0. TO 5415 2705.9945 146.6 0.
5420 1294.1665 228. 0. TO 5425 2697. 228. 0.
5430 1677.8854 341. 0. TO 5435 2722.8855 341. 0.
5440 2065. 455. 0. TO 5445 2749. 455. 0.
5450 2487. 594. 0. TO 5455 2874.059 594. 0.
5460 2689.47 696. 0. TO 5465 2965.8289 696. 0.
5470 2884. 794. 0. TO 5475 3054. 794. 0.
*/ HOR TAIL
5500 3124. 65.1 0. TO 5502 3417. 65.1 0.
5510 3255.0804 146.6 0. TO 5512 3440.5144 146.6 0.
5520 3386. 228. 0. TO 5522 3464. 228. 0.
*/ VERT WING FIN
5313 2487. 594. 0. TO 5315 2880. 594. 134.
5316 2680.5 594. 0. TO 5318 2910. 594. 134.
5319 2874.059 594. 0. TO 5321 2940. 594. 134.

```

```

*/ WEIGHT PANELS - BODY
6001 0. 0. 0. TO 6016 3564. 0. 0.
6021 0. 65. 0. TO 6036 3564. 65. 0.

*/ WEIGHT PANELS - WING
6100 741.0 65.0 0. TO 6220 2487.0 594.0 0. BY 20
6100 TO 6260 2487.0 594.0 0. BY 80
6180 TO 6240 2487.0 594.0 0. BY 20
6260 TO 6320 2884.0 794.0 0. BY 20
6110 2715.0 65.0 0. TO 6170 2715.0 329.5 0. BY 20
6189 2715.0 329.5 0. TO 6249 2874.0 594.0 0. BY 20
6266 2874.0 594.0 0. TO 6326 3054.0 794.0 0. BY 20
6100 TO 6110
**3 20 0 20
6180 TO 6189
**3 20 0 20
6260 TO 6266
**3 20 0 20
*/ WEIGHT PANELS - HOK TAIL
6400 3124. 65.1 0. TO 6403 3417. 65.1 0.
6410 3386. 228.0 0. TO 6413 3464. 228.0 0.

*/ WEIGHT PANELS - VERT FIN
6501 3374.6 0. 92.8
6502 3472. 0. 92.8
6503 3458.7 0. 149.8
6504 3514.6 0. 149.8

*/ WEIGHT PANELS - WING VERT FIN
6601 2487. 594. 0. TO 6603 2880. 594. 134.
6604 2874.059 594. 0. TO 6606 2940. 594. 134.

*/ NODES FOR CARGO HCLDS /
7001 400. 0. -55.
7002 400. 20. -55.
7003 400. 50. -20.
7004 400. 0. -20.
7005 650. 0. -55.
7006 650. 20. -55.
7007 650. 50. -20.
7008 650. 0. -20.
7011 2800. 0. -55.
7012 2800. 20. -55.
7013 2800. 50. -20.
7014 2800. 0. -20.
7015 2950. 0. -55.
7016 2950. 20. -55.
7017 2950. 50. -20.
7018 2950. 0. -20.

END NODAL DATA
BEGIN MASS DATA
BEGIN CONDITION DATA
PANEL DATA 1 CONDITION 1 11 11 0
PANEL DATA 1 CONDITION 2 12 11 0
PANEL DATA 1 CONDITION 3 20 12 0
PANEL DATA 1 CONDITION 4 20 13 0
END CONDITION DATA
BEGIN MASS ELEMENT DATA
PLATE F2 8-1 6001 6002 6022 3495.
PLATE F2 8-2 6002 6003 6023 6022 5955.
PLATE F2 8-3 6003 6004 6024 6023 2589.
PLATE F2 8-4 6004 6005 6025 6024 3440.
PLATE F2 8-5 6005 6006 6026 6025 5420.
PLATE F2 8-6 6006 6007 6027 6026 3280.
PLATE F2 8-7 6007 6008 6028 6027 3306.
PLATE F2 8-8 6008 6009 6029 6028 4346.
PLATE F2 8-9 6009 6010 6030 6029 4507.
PLATE F2 8-10 6010 6011 6031 6030 4486.
PLATE F2 8-11 6011 6012 6032 6031 3619.
PLATE F2 8-12 6012 6013 6033 6032 4730.
PLATE F2 8-13 6013 6014 6034 6033 3982.
PLATE F2 8-14 6014 6015 6035 6034 947.
PLATE F2 8-15 6015 6016 6036 6035 1788.
PLATE F2 VT-1 6501 6502 6504 6503 600.
PLATE F2 W-1 6100 6101 6121 6120 768.
PLATE F2 W-2 6101 6102 6122 21 1151.
PLATE F2 W-3 6102 6103 6123 22 1667.

```

PLATE F2	W-4	6103	6104	6124	6123	1112.
PLATE F2	W-5	6104	6105	6125	6124	1190.
PLATE F2	W-6	6105	6106	6126	6125	1659.
PLATE F2	W-7	6106	6107	6127	6126	1988.
PLATE F2	W-8	6107	6108	6128	6127	2467.
PLATE F2	W-9	6108	6109	6129	6128	1335.
PLATE F2	W-10	6109	6110	6130	6129	338.
PLATE F2	W-11	6120	6121	6141	6140	795.
PLATE F2	W-12	6121	6122	6142	6141	1415.
PLATE F2	W-13	6122	6123	6143	6142	813.
PLATE F2	W-14	6123	6124	6144	6143	1259.
PLATE F2	W-15	6124	6125	6145	6144	1248.
PLATE F2	W-16	6125	6126	6146	6145	1720.
PLATE F2	W-17	6126	6127	6147	6146	1494.
PLATE F2	W-18	6127	6128	6148	6147	1888.
PLATE F2	W-19	6128	6129	6149	6148	498.
PLATE F2	W-20	6129	6130	6150	6149	126.
PLATE F2	W-21	6140	6141	6161	6160	508.
PLATE F2	W-22	6141	6142	6162	6161	1279.
PLATE F2	W-23	6142	6143	6163	6162	536.
PLATE F2	W-24	6143	6144	6164	6163	532.
PLATE F2	W-25	6144	6145	6165	6164	559.
PLATE F2	W-26	6145	6146	6166	6165	1055.
PLATE F2	W-27	6146	6147	6167	6166	1405.
PLATE F2	W-28	6147	6148	6168	6167	1953.
PLATE F2	W-29	6148	6149	6169	6168	274.
PLATE F2	W-30	6149	6150	6170	6169	172.
PLATE F2	W-31	6180	6181	6201	6200	614.
PLATE F2	W-32	6181	6182	6202	6201	1286.
PLATE F2	W-33	6182	6183	6203	6202	562.
PLATE F2	W-34	6183	6184	6204	6203	786.
PLATE F2	W-35	6184	6185	6205	6204	1380.
PLATE F2	W-36	6185	6186	6206	6205	1849.
PLATE F2	W-37	6186	6187	6207	6206	1649.
PLATE F2	W-38	6187	6188	6208	6207	421.
PLATE F2	W-39	6188	6189	6209	6208	255.
PLATE F2	W-40	6200	6201	6221	6220	207.
PLATE F2	W-41	6201	6202	6222	6221	497.
PLATE F2	W-42	6202	6203	6223	6222	692.
PLATE F2	W-43	6203	6204	6224	6223	755.
PLATE F2	W-44	6204	6205	6225	6224	816.
PLATE F2	W-45	6205	6206	6226	6225	843.
PLATE F2	W-46	6206	6207	6227	6226	687.
PLATE F2	W-47	6207	6208	6228	6227	136.
PLATE F2	W-48	6208	6209	6229	6228	94.
PLATE F2	W-49	6220	6221	6241	6240	136.
PLATE F2	W-50	6221	6222	6242	6241	522.
PLATE F2	W-51	6222	6223	6243	6242	510.
PLATE F2	W-52	6223	6224	6244	6243	536.
PLATE F2	W-53	6224	6225	6245	6244	555.
PLATE F2	W-54	6225	6226	6246	6245	580.
PLATE F2	W-55	6226	6227	6247	6246	704.
PLATE F2	W-56	6227	6228	6248	6247	119.
PLATE F2	W-57	6228	6229	6249	6248	91.
PLATE F2	W-58	6260	6261	6281	6280	289.
PLATE F2	W-59	6261	6262	6282	6281	306.
PLATE F2	W-60	6262	6263	6283	6282	244.
PLATE F2	W-61	6263	6264	6284	6283	507.
PLATE F2	W-62	6264	6265	6285	6284	116.
PLATE F2	W-63	6265	6266	6286	6285	76.
PLATE F2	W-64	6290	6281	6301	6300	216.
PLATE F2	W-65	6281	6282	6302	6301	144.
PLATE F2	W-66	6282	6283	6303	6302	245.
PLATE F2	W-67	6283	6284	6304	6303	365.
PLATE F2	W-68	6284	6285	6305	6304	86.
PLATE F2	W-69	6285	6286	6306	6305	71.
PLATE F2	W-70	6300	6301	6321	6320	184.
PLATE F2	W-71	6301	6302	6322	6321	160.
PLATE F2	W-72	6302	6303	6323	6322	126.
PLATE F2	W-73	6303	6304	6324	6323	273.
PLATE F2	W-74	6304	6305	6325	6324	66.
PLATE F2	W-75	6305	6306	6326	6325	66.
PLATE F2	MT-1	6400	6401	6411	6410	283.

PLATE F2 MT-2 6401 6402 6412 6411 212.
 PLATE F2 MT-3 6402 6403 6413 6412 522.
 PLATE F2 WF-1 6601 6602 6605 6604 500.
 PLATE F2 WF-2 6602 6603 6606 6605 400.

END MASS ELEMENT DATA

BEGIN FUEL DATA

TANK 11

POLYGON 20 95. PERCENT

237 337 339 239 TO 243 343 345 245 BY 2 2 2 2
 445 345 347 447 TO 449 349 351 451 BY 2 2 2 2

TANK 12

POLYGON 20 97. PERCENT

451 351 353 453
 453 353 355 455
 255 355 357 257 TO 261 361 363 263 BY 2 2 2 2

TANK 21

POLYGON 30 90. PERCENT

347 547 549 349 TO 353 553 555 355 BY 2 2 2 2

TANK 22

POLYGON 30 90. PERCENT

355 555 557 357 TO 361 561 563 363 BY 2 2 2 2

TANK 31

POLYGON 20 85. PERCENT

553 653 654 554 TO 562 662 663 563

MANAGEMENT SEQUENCE 10

LOAD TANKS 21 22 UNTIL 70000.
 LOAD TANKS 11 12 31 RATIO 8. 6. 1. UNTIL 220000. TOTAL
 LOAD TANKS 31 UNTIL 31
 USE TANKS 11 12 RATIO 1. .75 UNTIL 11 12 EQ'ALS 2. 21 31
 TRANSFER 100. PERCENT 12 TO 11
 USE TANKS 11 21 22 RATIO 2. 1. 1. UNTIL 22 15000.
 TRANSFER 15000. FROM 22 TO 21
 USE TANKS 11 21 31 RATIO 3. 2. 1. UNTIL 60000.
 USE TANKS 11 21 31 RATIO 3. 2. 1. UNTIL 0. TOTAL

MANAGEMENT SEQUENCE 20

LOAD TANKS 11 12 21 UNTIL 11
 LOAD TANKS 22 31 UNTIL 22

CONDITION 11 180000. 10
 CONDITION 12 120000. 10
 CONDITION 15 100000. 10
 CONDITION 20 0. 20

END FUEL DATA

BEGIN PAYLOAD DATA

BEGIN SEAT LOCATION DATA

101 400. -10. 54. TO 166 3000. -10. 54.
 201 400. -10. 34. TO 266 3000. -10. 34.

END SEAT LOCATION DATA

HOLD 1 BRICK .05

7001 7002 7003 7004 7005 7006 7007 7008

HOLD 2 BRICK .05

7011 7012 7013 7014 7015 7016 7017 7018

LOADING SEQUENCE 1

LOAD SEATS 101 166 201 266 TO 133 134 233 234 BY 1 -1 1 -1
 LOAD CARGO HOLD 1 IN DIRECTION +Z UNTIL 10000. LOADED
 LOAD CARGO HOLD 2 IN DIRECTION +Z UNTIL 5000. LOADED

LOADING SEQUENCE 10

LOAD SEATS 101 TO 166
 LOAD SEATS 201 TO 266
 LOAD CARGO HOLD 1 IN DIRECTION +X UNTIL FULL
 LOAD CARGO HOLD 2 IN DIRECTION +X UNTIL FULL

LOADING SEQUENCE 11

LOAD SEATS 166 TO 101 BY -1
 LOAD SEATS 266 TO 201 BY -1
 LOAD CARGO HOLD 2 IN DIRECTION -X UNTIL FULL
 LOAD CARGO HOLD 1 IN DIRECTION -X UNTIL FULL

CONDITION 11 SEQUENCE 1 80 14000.
 CONDITION 12 SEQUENCE 1 132 0.
 CONDITION 13 SEQUENCE 1 0 15000.
 CONDITION 20 SEQUENCE 11 132 24500.
 CONDITION 30 SEQUENCE 10 132 24500.

END PAYLOAD DATA

```

BEGIN PANEL DATA 1
*/ BODY
MASS SUBSETS 1
FUEL,PAYLOAD
DIRECTION 2
1 5100 5251 5252 5101
2 5101 5253 5254 5102
3 5202 5203 5103 5102 TO 12

*/ WING FIN
MASS SUBSETS 2
DIRECTION Y
13 5313 5316 5317 5314
14 5316 5319 5320 5317
15 5314 5317 5318 5315
16 5317 5320 5321 5318

*/ WING
MASS SUBSETS 3
FUEL,PAYLOAD
DIRECTION 2
17 5400 5401 5411 5410 TO 21
**6 5 10 **3 0 5
*/ HOR TAIL
MASS SUBSETS 4
DIRECTION 2
52 5500 5501 5511 5510 TO 53
**1 2 10 **3 0 2
END PANEL DATA 1
END MASS DATA
BEGIN SUBSET DEFINITION
SUBSETS OF MASS SET 1
N1 = 6001 TO 6036 6501 TO 6504
E1 = ALL IN N1
N2 = 6601 TO 6606
E2 = ALL IN N2
N3 = 6100 TO 6326
E3 = ALL IN N3
N4 = 6400 TO 6413
E4 = ALL IN N4
N5 = 6001 TO 6606
E5 = ALL IN N5
END SUBSET DEFINITION
END PROBLEM DATA

```

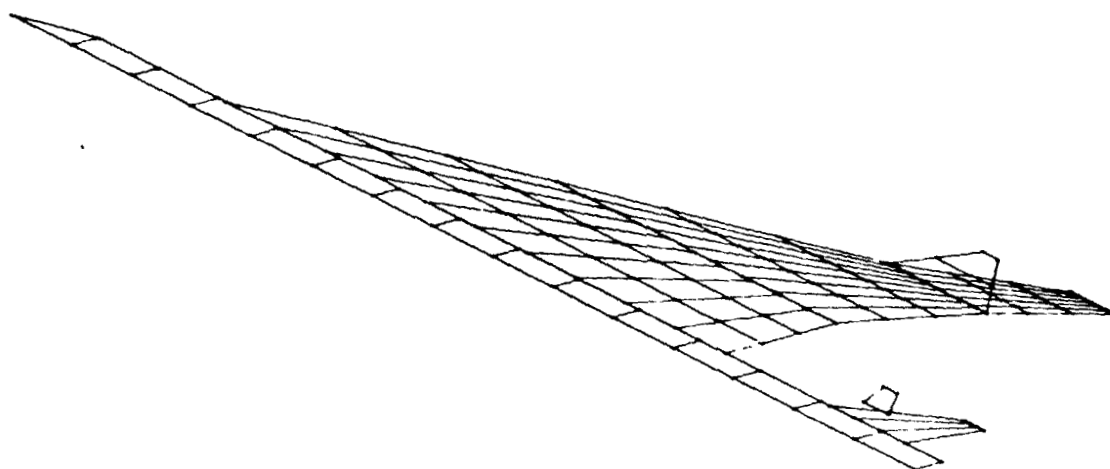



Figure 208-1. Mass Model for Fuel and Payload Demonstration

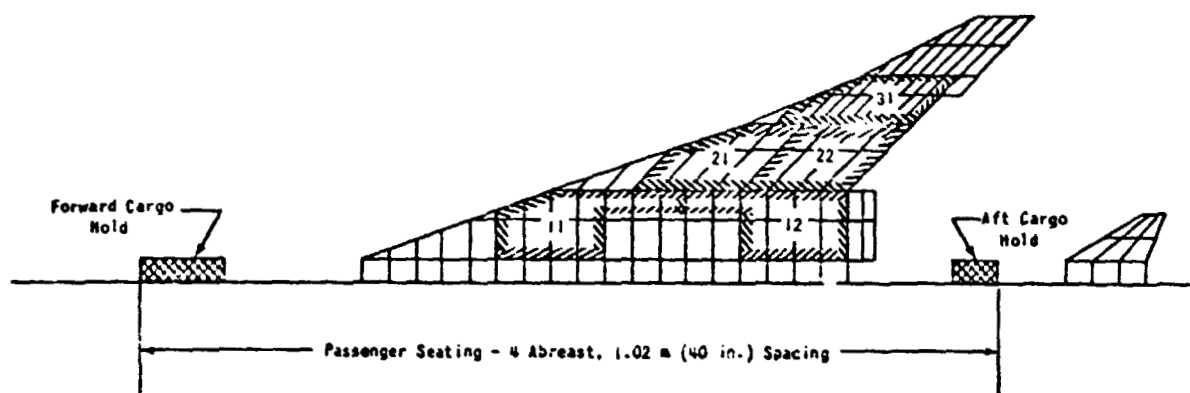


Figure 208-2. Location of Fuel Tanks, Cargo Holds and Seating

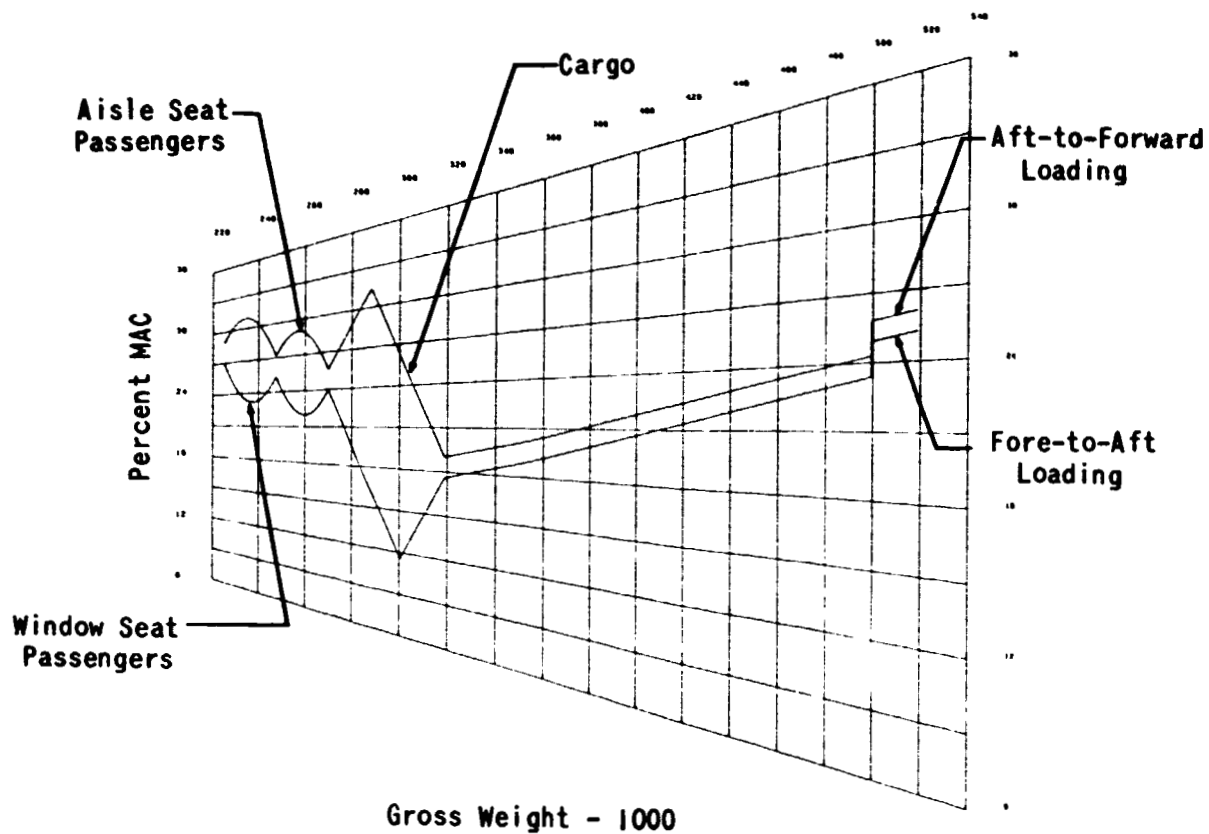


Figure 208-3. Loadability Diagram, Fuel and Payload Demonstration

209. FULLY-STRESSED DESIGN AND COMPOSITE OPTIMIZATION (DECK 3)

209.1 DESCRIPTION OF PROBLEM

This problem demonstrates the fully-stressed design and composite optimization capabilities of the Design Module. The structural model, shown in figure 209-1, is the same as that described in section 203 with the addition of several CCOVER elements (element subset 200 as shown in figure 209-2). These CCOVERs have upper surfaces only with a stackup of (0/+45/90). The symmetric loading described in section 203 is factored by ten to obtain the design loading condition (except as shown in table 209-1).

All the CCOVER elements constitute a single optimization problem. A separate execution of the Design Module produces an optimized lay-up based upon the strains in a subregion consisting of one element.

The subsets used to define the design problem are shown in figures 209-2 and 209-3. The design options employed are summarized in table 209-1.

209.2 RESULTS

Two resize cycles were executed. The total weight at each cycle is shown in figure 209-4. As an example, upper and lower surface basic plate thicknesses before and after resize are shown in figure 209-5 for element subset 121. Margins of safety for this subset for the two cycles are shown in figures 209-6 and 209-7.

The composite optimization converged after 7 local and 2 global iterations producing the number of layers shown in table 209-2.

209.3 LISTING OF CONTROL PROGRAM AND DATA

```

C BEGIN CONTRCL MATRIX PROGRAM DEM003
C PROBLEM IC(DEM003 - FULLY-STRESSED DESIGN/COMPOSITE OPTIMIZATION)
C
C PURPOSE      THE PRINCIPAL CAPABILITIES DEMONSTRATED BY THIS
C              DECK ARE
C              1. FULLY-STRESSED DESIGN
C              2. COMPOSITE OPTIMIZATION
C              3. STRENGTH MARGIN OF SAFETY PLOTS
C
C AUTHOR      BJURN BACKMAN
C
C CORE        170K (OCTAL)
C
C INTEGER BEGCYCL,ENDCYCL,CURCYCL
C DIMENSION CONVERG(17)
C USER COMMON (BEGCYCL,ENDCYCL,CURCYCL,CONVERG,{SET,ISTAGE,IPOS)
C
C BEGCYCL=1
C ENDCYCL=2
C READ INPUT
C PRINT INPUT(NODAL)
C PRINT INPUT(STIFFNESS)
C PRINT INPUT(BC,STAGE=2)
C EXECUTE EXTRACT(EXNAME=TOTAL,LSUB=KGRID,ESUB=E1,NSUB=N1)
C EXECUTE GRAPHICS(GNAME=GEOM,OFFLINE=CALCOMP,RZ=30,RX=0,RY=20,
X      TYPE=(ORTH,POINT),SIZE=(20,20),EXNAME=TOTAL)
C PERFORM DESIGN (STAGE=2)
C PRINT INPUT(DESIGN,SET=1)
C EXECUTE DESIGN(HISTORY,SET=1,STAGE=2,CYCLE=(1,2),IELN=(1,3,16,18,
119,21,29))
C EXECUTE DESIGN(COMPOSITE,SET=1,STAGE=2,CYCLE=3)
C PRINT OUTPUT(DESIGN,SET=1)
C PRINT OUTPUT(DESIGN,HISTORY,SET=1)
C EXECUTE EXTRACT(EXNAME=MARGINS,LSUB=SMS,STAGE=2,CYCLE=(1,2),
X      ESUB=E121,NSUB=N121)
C EXECUTE GRAPHICS(GNAME=DESIGN,TYPE=ORTH,SIZE=(15,15),
X      VIEW=100,SCALAR=COVSMS,SSCALE=100,EXNAME=MARGINS)
C END CONTROL PROGRAM

```

```

*/ MODE2 /
BEGIN MATERIAL DATA
COMPOSITE MATERIAL DATA
C01 .0052 3.77E-4
70 30.0E6 2.7E6 .21 .7E6 1.E-6 *= 1.28E5 2.E4 1.28E5 2.E4 6.4E4 *=5
500 29.E6 2.6E6 .20 .6E6 .9E-6 *= 1.18E5 1.9E4 1.18E5 1.9E4 6.3E4 *=5
END MATERIAL DATA

```

```

BEGIN NODAL DATA

```

```

*/

```

```

*/ BODY NODES

```

```

*/

```

1	20.	0.	0.		TO	25	980.	0.	0.		BY	2
27	1060.	0.	0.	30.0	TO	45	1780.	0.	0.	42.5	BY	2
**+1	200	0.	65.	0.	0	200	0.	65.			**	
45					TO	55	2180.	0.	0.	31.0	BY	2
**+1	200				0	200	0.	65.			**	
55					TO	63	2500.	0.	0.	13.5	BY	2
**+1	200				0	200	0.	65.			**	
65	2580.	0.	0.		TO	77	3060.	0.	0.		BY	2
79	3140.	0.	0.	3.0								
**+1	200	0.	65.	**								
81	3220.	0.	0.	6.5								
**+1	200	0.	65.	**								
83	3300.	0.	0.	7.0								
**+1	200	0.	65.	**								
85	3380.	0.	0.	2.0								
**+1	200	0.	65.	**								
87	3460.	0.	0.									
89	3540.	0.	0.									

```

*/

```

```

*/ WING NODES

```

```

*/

```

427	1060.	65.	0.	30.0	TO	435	1380.	180.	0.	17.5	BY	2
435					TO	445	1780.	180.	0.	27.5	BY	2
445					TO	455	2180.	180.	0.	25.0	BY	2
455					TO	463	2500.	180.	0.	13.0	BY	2
635	1380.	180.	0.	17.5	TO	641	1620.	265.	0.	10.0	BY	2
641					TO	655	2180.	265.	0.	22.5	BY	2
655					TO	663	2500.	265.	0.	12.5	BY	2
841	1620.	265.	0.	10.0	TO	847	1971.	380.	0.	9.0	BY	2
847					TO	855	2291.	380.	0.	17.0	BY	2
855					TO	863	2611.	380.	0.	10.0	BY	2
1047	1971.	380.	0.	9.0	TO	1051	2205.	455.	0.	8.5	BY	2
1051					TO	1059	2525.	455.	0.	15.0		
1059					TO	1063	2685.	455.	0.	8.0		
1251	2205.	455.	0.	8.5	TO	1254	2409.	538.	0.	6.5		
1254					TO	1259	2609.	538.	0.	11.0		
1259					TO	1263	2769.	538.	0.	5.5		
1454	2409.	538.	0.	6.5	TO	1456	2545.	594.	0.	5.0		
1456					TO	1459	2665.	594.	0.	7.5		
1459					TO	1463	2825.	594.	0.	3.5		
1656	2545.	594.	0.	5.0	TO	1658	2710.	680.	0.	3.0		
1658					TO	1663	2910.	680.	0.	3.0		
1858	2710.	680.	0.	3.0	TO	1860	2875.	765.	0.	1.5		
1860					TO	1863	2995.	765.	0.	2.5		

```

*/

```

```

*/ WING TRAILING EDGE NODES

```

```

*/

```

3001	2500.	65.	0.	13.5	TO	3005	2715.	65.	0.	1.0	BY	2
3101	2500.	180.	0.	13.0	TO	3105	2715.	180.	0.	1.0	**	
3201	2500.	265.	0.	12.5	TO	3205	2715.	265.	0.	1.0	**	
3405	2874.	594.	0.	1.0	TO	3605	3027.9	765.	0.	1.0		

BY 100 OF 86. 85.

```

*/

```

```

*/ WING FIN NODES

```

```

*/

```

REC	WINGFIN	0.	594.	0.	1.	594.	0.	0.	-1.	0.		
2056	2545.	.1	0.	3.5	TO	2456	2830.	100.	0.	2.5	BY	200
2058	2625.	.1	0.	3.5	TO	2458	2842.	100.	0.	3.0	**	
2061	2745.	.1	0.	4.0	TO	2461	2859.	100.	0.	3.0	**	
2063	2825.	.1	0.	4.0	TO	2463	2870.	100.	0.	3.0	**	

```

*/

```

*/ HORIZONTAL TAIL NODES

*/

RESUME GLOBAL

279	TO	679	3365.	200.	0.	2.0	BY	200
281	TO	681	3388.	200.	0.	2.5	**	
283	TO	683	3412.	200.	0.	2.5	**	
285	TO	685	3435.	200.	0.	1.0	**	

END NODAL DATA

BEGIN STIFFNESS DATA

BEGIN PROPERTY DATA

P1	.05	1.	*(WING FIN SPARS AND RIBS)					
P2	2.	0.	0.	.2	.2	.2	*(WING FIN ATTACHMENT BEAMS - TYPE 1)	
P3	10.	0.	0.	100.	100.	100.	*(WING FIN ATTACHMENT BEAMS - TYPE 2)	
P4	.15	.50	*(CONTROL SURFACE RIBS)					
P5	0.	*=2	100.	100.	0.	10.	*(BEAMS AT 455 RIB TO PICK UP SPARS)	

END PROPERTY DATA

BEGIN ELEMENT DATA

*/

*/ WING FRONT SPAR

*/

SPAR	M5	N2003	227	429	.12	2.				
*2		N2205	429	431	.12	2.	TO	N2605	433	435
							BY	N200	2	2
*2		N2805	435	637	.12	2.				
*2		N3007	637	639	.12	2.	TO	N3207	639	641
							BY	N200	2	2
*2		N3407	641	843	.12	2.				
*2		N3609	843	845	.12	2.	TO	N3809	845	847
							BY	N200	2	2
*2		N4009	847	1049	.12	2.				
*2		N4211	1049	1051		**				
*2		N4411	1051	1253		**				
*2		N4613	1253	1254		**				
*2		N4713	1254	1455		**				
*2		N4815	1455	1456		**				
*2		N4915	1456	1657		**				
*2		N5017	1657	1658		**				
*2		N5117	1658	1859		**				
*2		N5219	1859	1860		**				

*/

*/ WING REAR SPAR

*/

SPAR	M5	N5603	263	463	.40	12.
*2		N5605	463	663	.40	12.
*2		N5607	663	863	.34	12.
*2		N5609	863	1063	.34	12.
*2		N5611	1063	1263	.30	8.
*2		N5613	1263	1463	.30	8.
*2		N5615	1463	1663	.30	4.
*2		N5617	1663	1863	.30	4.

*/

*/ WING INTERMEDIATE SPARS

*/

SPAR	M5	N2203	229	429	.20	2.	TO	N3603	243	443
							BY	N200	2	2
*2		N3803	245	445	.36	2.				
*2		N4803	255	455	.60	12.				
*2		N5003	257	457	.24	12.	TO	N5403	261	461
							BY	N200	2	2
*2		N3005	437	637	.20	2.	TO	N3605	443	643
							BY	N200	2	2
*2		N3805	445	645	.36	2.				
*2		N4005	447	647	.20	4.	TO	N4605	453	653
							BY	N200	2	2
*2		N4805	455	655	.60	12.				
*2		N5005	457	657	.24	12.	TO	N5405	461	661
							BY	N200	2	2
*2		N3607	643	843	.20	2.	TO	N3807	645	845
							BY	N200	2	2
*2		N4007	647	847	.20	4.	TO	N4607	653	853
							BY	N200	2	2
*2		N4807	655	855	.20	8.				

*2	N5007	657	857	.20	10.	TO	N5407	661	861	+	
						BY	N200	2	2		
*2	N4209	849	1 49	.20	4.	TO	N4609	853	1053	+	
						BY	N200	2	2		
*2	N4809	855	1055	.20	8.						
*2	N5009	857	1057	.20	10.	TO	N5409	861	1061	+	
						BY	N200	2	2		
*2	N4611	1053	1253	.12	4.	TO	N4811	1055	1255	+	
						BY	N100	1	1		
*2	N4911	1056	1256	.06	4.	TO	N5511	1062	1262	+	
						BY	N100	1	1		
*2	N4813	1255	1455	.12	4.						
*2	N4913	1256	1456	.06	4.	TO	N5513	1262	1462	+	
						BY	N100	1	1		
*2	N5015	1457	1657	.06	2.	TO	N5515	1462	1662	+	
						BY	N100	1	1		
*2	N5217	1659	1859	.06	2.	TO	N5517	1662	1862	+	
						BY	N100	1	1		
*/											
*/ WING IN-BODY SPARS											
*/											
SPAR	M5	N7001	27	227	1.00	10.	TO	N3601	43	243	+
						BY	N200	2	2		
*2		N3801	45	245	1.80	10.	TO	N4601	53	253	+
						BY	N200	2	2		
*2		N4801	55	255	3.00	60.					
*2		N5001	57	257	1.20	60.	TO	N5401	61	261	+
						BY	N200	2	2		
*2		N5601	63	263	2.00	60.					
*/											
*/ WING RIBS											
*/											
SPAR	M5	N6001	227	229	.25	4.	TO	N6035	261	263	+
						BY	N2	2	2		
*2		N6109	435	437	.30	4.	TO	N6135	461	463	+
						BY	N2	2	2		
*2		N6215	641	643	.20	3.	TO	N6235	661	663	+
						BY	N2	2	2		
*2		N6425	1051	1053	.20	4.					
*2		N6426	1053	1054	.20	4.	TO	N6435	1062	1063	
*2		N6629	1456	1457	.12	2.	TO	N6635	1462	1463	
*2		N6833	1860	1861	.30	1.4	TO	N6835	1862	1863	
*/											
*/ WING COVERS											
*/											
COVER	M5	N7003	229	429	227	.06					
*2		N7203	229	429	431	231	.06			TO	
		N8603	243	443	445	245		BY	N200	2	
CCOVER T70 N27203 229 429 431 231 0. A0 TO L1 C01 A-45. A45. A90. +											
TO N28603 243 443 445 245 BY N200 2 **3											
COVER M5 N8803 245 445 447 247 .12 .00 TO +											
		N9603	253	453	455	255		BY	N200	2	
*2		N9803	255	455	457	257	.10	.14		**3	
*2		N10003	257	457	459	259		**			
*2		N10203	259	459	461	261	.26	.14	.22	.00	
*2		N10403	261	461	463	263		**			
*2		N7805	437	637	435		.06				
*2		N8005	437	637	639	39	.06			TO	
		N9605	453	653	655	455		BY	N200	2	
*2		N9805	455	655	657	457	.10	.14		**3	
*2		N10005	457	657	659	459		**			
*2		N10205	459	659	661	461	.26	.14	.22	.00	
*2		N10405	461	661	663	463		**			
*2		N8407	643	843	641		.06				
*2		N8607	643	843	845	645	.06			TO	
		N9607	653	853	855	655		BY	N200	2	
*2		N9807	655	855	857	657	.10	.08		**3	
*2		N10007	657	857	859	659		**			
*2		N10207	659	859	861	661	.30	.14	.20	.00	
*2		N10407	661	861	863	663		**			
*2		N9009	849	1049	847		.06				
*2		N9209	849	1049	1051	851	.06			TO	
		N9609	853	1053	1055	855		BY	N200	2	

*2	N9809	855	1055	1057	857	.10	.08						
*2	N10009	857	1057	1059	859		**						
*2	N10209	859	1059	1061	861	.30	.14	.20	.00				
*2	N10409	861	1061	1063	863		**						
*2	N9411	1053	1253	1051		.30	.14	.22	.12				
*2	N9611	1053	1253	1254	1054	.30	.14	.22	.12	TO	+		
	N10511	1062	1262	1263	1063		BY	N100	1	*=3			
*2	N9713	1255	1455	1254		.30	.14	.22	.12				
*2	N9813	1255	1455	1456	1256	.30	.14	.22	.12	TO	+		
	N10513	1262	1462	1463	1263		BY	N100	1	*=3			
*2	N9915	1457	1657	1456		.08							
*2	N10015	1457	1657	1658	1458	.08				TO			
	N10515	1462	1662	1663	1463		BY	N100	1	*=3			
*2	N10117	1659	1859	1658		.08							
*2	N10217	1659	1859	1860	1660	.08				TO	+		
	N10517	1662	1862	1863	1663		BY	N100	1	*=3			
*/													
*/ WING IN-BODY COVERS													
*/													
COVER	M5	N7001	27	227	229	29	.30			TO	+		
		N8601	43	243	245	45		BY	N200	2	*=3		
*2		N8801	45	245	247	47	.60			TO	+		
		N9601	53	253	255	55		BY	N200	2	*=3		
*2		N9801	55	255	257	57	.70						
*2		N10001	57	257	259	59	.70						
*2		N10201	59	259	261	61	1.30	.70	1.10	.00			
*2		N10401	61	261	263	63		**					
*/													
*/ WING FIN SPARS													
*/													
SPAR	M5	N11001	2056	2256		P1							
*2		N11003	2256	2456		*							
*2		N11201	2058	2258		*							
*2		N11203	2258	2458		*							
*2		N11501	2061	2261		*							
*2		N11503	2261	2461		*							
*2		N11701	2063	2263		*							
*2		N11703	2263	2463		*							
*/													
*/ WING FIN RIBS													
*/													
SPAR	M5	N12001	2256	2258		P1							
*2		N12003	2258	2261		*							
*2		N12005	2261	2263		*							
*2		N12201	2456	2458		*							
*2		N12203	2458	2461		*							
*2		N12205	2461	2463		*							
*/													
*/ WING FIN COVERS													
*/													
COVER	M5	N13001	2056	2256	2258	2058	.05						
*2		N13003	2058	2258	2261	2061	*						
*2		N13005	2061	2261	2263	2063	*						
*2		N13201	2256	2456	2458	2258	*						
*2		N13203	2258	2458	2461	2261	*						
*2		N13205	2261	2461	2463	2263	*						
*/													
*/ WING FIN ATTACHMENT BEAMS													
*/													
BEAM	L5	N20001	1456	2056	1463	P2							
*2		N20003	1458	2058	1463	*							
*2		N20005	1461	2061	1463	*							
*2		N20007	1463	2063	1461	*							
*2		N21001	1458	1458		P3							
*2		N21003	1458	1461		*							
*2		N21005	1461	1463		*							
*/													

*/ WING TRAILING EDGE CONTROL SURFACE RIBS

```

*/
    SPAR  M5  N101      263 3003      P4
**+2  0    0          2    200 100      0
    *2      N102      3003 3005      *
**+2  0    0          2    100 100      0
    *2      N108      1463 3405      *
**+2  0    0          1    200 100      *

```

*/ WING TRAILING EDGE CONTROL SURFACE COVERS

```

*/
    COVER  M5  N151      263 463 3103 3003  .10
    *2      N153      463 663 3203 3103      *
    *2      N152      3003 3103 3105 3005      *
    *2      N154      3103 3203 3205 3105      *
    *2      N156      1463 1663 3505 3405      *
**+1  0    0          1    200 200 100 100      *

```

*/ HORIZONTAL TAIL SPARS

```

*/
    SPAR  M5  N14003      279 479      .10 1.2
    *2      N14005      479 679      **
    *2      N14103      281 481      .05 1.8
    *2      N14105      481 681      **
    *2      N14203      283 483      .05 1.6
    *2      N14205      483 683      **
    *2      N14303      285 485      .20 2.6
    *2      N14305      485 685      **

```

*/ HORIZONTAL TAIL RIBS

```

*/
    SPAR  M5  N14401      279 281      .15 2.0 TO N14405 283 285      +
    *2      N14501      479 481      .10 1.2 TO N14505 483 485      +
    *2      N14601      679 681      .10 1.2 TO N14605 683 685      +
                                     BY N2      2      2
                                     BY N2      2      2

```

*/ HORIZONTAL TAIL IN-BODY SPARS

```

*/
    SPAR  M5  N14001      79 279      .50 6.0
    *2      N14101      81 281      .25 9.0
    *2      N14201      83 283      .25 8.0
    *2      N14301      85 285      1.00 13.0

```

*/ HORIZONTAL TAIL COVERS

```

*/
    COVER  M5  N15003      279 479 481 281  .16
**+2  0    0          200      2 **3      0.
    COVER  M5  N15005      479 679 681 481  .07
**+2  0    0          200      2 **3      0.

```

*/ HORIZONTAL TAIL IN-BODY COVERS

```

*/
    COVER  M5  N15001      79 279 281  81  .80
    N15401      83 283 285  85      BY N200      2      **3

```

*/ BODY BEAMS

```

*/
    BEAM  M5  N1001      1 3 5. 0. **3 16000. 10. 0. **3 30000.
**+30  0    0          2 2 5. **4 14000. 5. **4 14000.
    *2      N1063      63 65 160. **4 450000. 148. **4 416000.
**+12  0    0          2 2 -12. **4 -34000. -12. **4 -34000.

```

*/ BEAMS AT 455 RIB TO PICK UP DISCONTINUED SPARS

```

*/
    BEAM  M5  N30002      1053 1054      P5
**+4  0    0          2 2 2      *
    BEAM  M5  N30011      1063 1062      P5
**+4  0    0          -2 -2 -2      *

```

END ELEMENT DATA
END STIFFNESS DATA

```

BEGIN BC DATA
  STAGE 2
    SUPPORT ASYM IN SURFACE 2
    SUPPORT TX TZ RY FOR 89
END BC DATA
BEGIN LOAD DATA
  SET 1 STAGE 2
  LOAD CASE ID SYMM **SYMMETRIC AIRLOADS*
  BEGIN NODAL LOAD DATA
    ORDER FZ
    CASE SYMM
      3      -2275.
      9      -6110.
      15     -4970.
      23     -3255.
      31     -245.
      39     -5400.
      45     -380.
      53     -3830.
      61      140.
      67     -165.
      75     -6365.
      83     -3495.
      87     -3160.
      89     -150.
      89     -150.
    ORDER FZ FY
      2056    -125.    1220.
      2456    -100.    1360.
      2458    -100.    -410.
      2058    -125.    955.
      2061    -125.    1075.
      2461    -100.    7665.
      2463    -100.    -4960.
      2063    -125.    -660.
    ORDER FZ
      431     13475.
      231     -8530.
      637      8030.
      237     -7750.
      245     -11770.
      655     -4640.
      255     -5330.
      663      1565.
      263      5445.
      843     36405.
      645     -20750.
      105      21130.
      649      3435.
      1055     3365.
      1063      1435.
      1456     13820.
      1459     21815.
      1463      6155.
      1860      860.
      1861     14395.
      1863     2762.
      659      -450.
      1059     -8710.
      1461     -10655.
      1862     -5190.
      279     -5060.
      679     -4040.
      681     -7375.
      281     -5415.
      283     -1620.
      683      -865.
      685     -1725.
      285     -3425.
    END NODAL LOAD DATA
  END LOAD DATA

```

```

*/MODEL /
BEGIN SUBSET DEFINITION /
SUBSETS OF STIFFNESS SET 1 /
*/
*/ SUBSETS FOR GEOMETRY PLOTS /
E1 = ALL /
N1 = ALL /
*/
*/ELEMENT SUBSETS FOR DESIGN /
*/ALL SUBSETS ARE IN THE RANGE E100 TO E199 /
*/
*/
*/
*/
*/ GROUP 1 /
*/ BODY SUBSET /
E100 = 1027 TO 1073 BY 2 /
*/
*/ GROUP 2 /
*/ WING SUBSETS /
*/STARTING WITH THE SPAR ELEMENTS REPRESENTING SPARS /
*/BEGINNING AT FRONT SPAR AND CONTINUING AFT /
E101 = 2001 2003 2205 TO 2805 BY 200 3007 TO 3407 BY 200
      3609 TO 4009 BY 200 4211 4411 4613 4713 4815 4915
      5017 5117 5219 / FRONT SPAR
E102 = 2201 2203 2401 2403 2601 2603 2801 2803 / 1 TO 4 INT SPARS
E103 = 3001 TO 3005 BY 2 3201 TO 3205 BY 2 3401 TO 3405 BY 2
      3601 TO 3607 BY 2 / 5 TO 8 INT SPAR
E104 = 3801 TO 3807 BY 2 4001 TO 4007 BY 2 4201 TO 4209 BY 2
      4401 TO 4409 BY 2 / 9 TO 12 INT SPAR
E105 = 4601 TO 4609 BY 2 4801 TO 4809 BY 2 5001 TO 5009 BY 2
      5201 TO 5209 BY 2 5401 TO 5409 BY 2 / 13 TO 17 INT SPAR TO FINE GRID
E106 = 5601 TO 5617 BY 2 / REAR SPAR
E107 = 4611 TO 5511 BY 100 4813 TO 5513 BY 100
      5015 TO 5515 BY 100 5217 TO 5517 BY 100 / OUTBOARD INT SPARS
*/
*/SPAR ELEMENTS REPRESENTING RIBS /
*/BEGINNING INBOARD /
E108 = 6001 TO 6035 BY 2 / SIDE OF BODY RIB
E109 = 6109 TO 6135 BY 2 / FIRST OUTBOARD RIB
E110 = 6215 TO 6235 BY 2 / SECOND OUTBOARD RIB
E111 = 6425 TO 6435 / THIRD OUTBOARD RIB
E112 = 6629 TO 6635 / FOURTH OUTBOARD RIB
E113 = 6833 TO 6835 / TIP RIB
*/
*/AUXILIARY BEAMS /
E114 = 30002 TO 30011 / BEAMS AT THIRD RIB (455 RIB)
E115 = 20001 TO 20007 BY 2 21001 TO 21005 BY 2 / FIN ATTACHMENT BEAM
*/
*/ GROUP 3 /
*/ WING COVERS /
*/STARTING INBOARD /
E116 = 7001 TO 10401 BY 200 / CENTER SECTION
E117 = 7003 TO 7603 BY 200 / FIRST BAY FS TO INT4
E118 = 7803 TO 8403 BY 200 7805 TO 8405 BY 200 8407 / INT4 TO INT8 TO FS
E119 = 8603 TO 9203 BY 200 8605 TO 9205 BY 200
      8607 TO 9207 BY 200 9209 9209 / INT8 TO INT12 TO FS
E120 = 9403 TO 9803 BY 200 9405 TO 9805 BY 200
      9405 TO 9805 BY 200 9407 TO 9807 BY 200
      9409 TO 9809 BY 200 / INT12 TO INT15 TO RIB 455
E121 = 10003 TO 10403 BY 200 10005 TO 10405 BY 200
      10007 TO 10407 BY 200 10009 TO 10409 BY 200 / INT14 TO RS TO 455
N121 = NUDES IN E121 /
E122 = 9411 TO 10511 BY 100 9713 TO 10513 BY 100 / 2 BAYS OUTBOARD 455
E123 = 9915 TO 10515 BY 100 10117 TO 10517 BY 100 / 2 OUTBOARD BAYS
*/
*/ GROUP 4 /
*/ CONTROL SURFACES /
E124 = 107 TO 110 155 TO 157 / OUTBOARD
E125 = 101 TO 106 151 TO 154 / INBOARD
*/

```

```

*/ GROUP 5 /
*/ E004 IS THE HORIZONTAL TAIL /
*/ E002 IS THE VERTICAL WING FIN /
E2 = SLAB Y 594. /
E4 = SPARS COVERS TUBE 79 279 679 685 85 DIRE. ON O. O. 1. /
*/ E200 AND E201 ARE COMPOSITE SUBSETS /
E200 = 27203 TO 28603 BY 200 /
E201 = 27203 /
END SUBSET DEFINITION /
BEGIN MATERIAL DATA /
M51 .16 /
60 1. *11 170.E3 168.E3 166.E3 140.E3 138.E3 136.E3 100.E3 98.E3 96.E3
50.E3 *8 /
120 *12 165.E3 163.E3 161.E3 135.E3 133.E3 131.E3 95.E3 93.E3 91.E3
48.E3 *8 /
200 *12 160.E3 158.E3 156.E3 130.E3 128.E3 126.E3 90.E3 88.E3 86.E3
46.E3 *8 /
500 *12 130.E3 128.E3 126.E3 100.E3 98.E3 96.E3 60.E3 58.E3 56.E3
26.E3 *8 /
M52 .10 /
50 1. *11 90.E3 88.E3 86.E3 70.E3 68.E3 66.E3 50.E3 48.E3 46.E3
13.E3 *8 /
200 *12 80.E3 78.E3 76.E3 60.E3 58.E3 56.E3 40.E3 38.E3 36.E3
12.E3 *8 /
600 *12 70.E3 68.E3 66.E3 50.E3 48.E3 46.E3 30.E3 28.E3 26.E3
11.E3 *8 /
END MATERIAL DATA /
BEGIN DESIGN DATA /
MODE 1 /
BEGIN TABLE DATA /
BC51 60 .04 .08 .12 .30 110.E3 115.E3 120.E3 130.E3 /
BC51 120 *4 105.E3 110.E3 115.E3 125.E3 /
BC51 200 *4 100.E3 105.E3 110.E3 120.E3 /
BC51 500 *4 80.E3 85.E3 90.E3 100.E3 /
BC52 60 *4 50.E3 52.E3 54.E3 55.E3 /
BC52 200 *4 48.E3 50.E3 52.E3 53.E3 /
BC52 500 *4 25.E3 26.E3 27.E3 27.5E3 /
BS51 60 *4 70.E3 75.E3 80.E3 83.E3 /
BS51 180 *4 60.E3 65.E3 70.E3 72.E3 /
BS51 540 *4 30.E3 35.E3 40.E3 41.E3 /
BS52 60 *4 35.E3 37.5E3 40.E3 41.5E3 /
BS52 180 *4 30.E3 32.5E3 35.E3 36.E3 /
BS52 540 *4 15.E3 17.5E3 20.E3 20.5E3 /
END TABLE DATA /
SET 1 /
BEGIN PROPERTY DATA /
BEAMS .5 /
END PROPERTY DATA /
BEGIN FIXED DATA /
E117 0 0 .04 .03 .03 0 0 .04 .03 .03 /
END FIXED DATA /
BEGIN LOWER BOUND DATA /
E118 0 0 .06 0 0 0 0 .05 0 0 /
E119 0 0 .06 0 0 0 0 .06 0 0 /
E120 0 0 .07 .04 0 0 0 .06 .03 0 /
E121 .5 0 .06 .04 0 .5 0 .06 .04 0 /
E122 .5 C .09 0 0 0 0 .09 0 0 /
E123 0 0 .045 0 C 0 0 .045 0 0 /
SPARS .04 .7 *3 .5 /
END LOWER BOUND DATA /
BEGIN UPPER BOUND DATA /
E123 0 0 .15 0 0 0 0 .12 0 0 /
END UPPER BOUND DATA /
BEGIN MARGIN DATA /
E120 .15 /
E4 SPARS .20 /
N6833 .35 /
END MARGIN DATA /
BEGIN SIZING DATA /
M5 /
M51 E121 BC51 BS51 .5 /
M52 E122 BC52 B .65 /
M51 SPARS B BS52 /
END SIZING DATA /

```

BEGIN RESTRAIN SIZING DATA /
E116 /
E125 /
E4 COVERS /
BEAMS /
E124 /
E2 /
END RESTRAIN SIZING DATA /
BEGIN OPTIMIZATION DATA /
CCOVER E200 E201 /
END OPTIMIZATION DATA /
STAGE 2 1 1 /
BEGIN LOADS DATA /
CASE SYMM 10. /
CASE SYMM 20. T400 E121 /
CASE SYMM 15. T350 E122 /
CASE SYMM 10. T300 E123 /
CASE SYMM 15. E105 /
CASE SYMM 30. E107 /
CASE SYMM 30. E106 /
CASE SYMM 2000. E200 /
END LOADS DATA /
BEGIN SUPERPOSITION DATA /
CASE HEAVY 15. SYMM 15. SYMM E106 /
END SUPERPOSITION DATA /
END DESIGN DATA /
END PROBLEM DATA /

Table 209-1. Summary of Design Options Used

ELEMENT SUBSET NO.	ELEMENT TYPES	LOWER BOUND	UPPER BOUND	FIXED	SPECIFIED MARGIN	SIZING RESTRAINED	LOAD FACTOR	TEMPERATURE	COMPOSITE OPTIMIZATION
2	SPARS & COVERs				X (SPARS)	X (COVERs)			
4									
105	SPARS						15		
106							30		
107							30		
116	COVERs					X			
117				X					
118		X							
119		X							
120		X			X				
121		X					20	400°F	
122		X					15	350°F	
123		X	X					300°F	
124						X			
125						X			
—	SPARS	X							
—	BEAMs					X			
200	COVERs						2000		X

Table 209-2. Optimum Number of
Layers per Lamina

Fiber Angle	Number of Layers
0°	10
+45°	1
-45°	1
90°	48

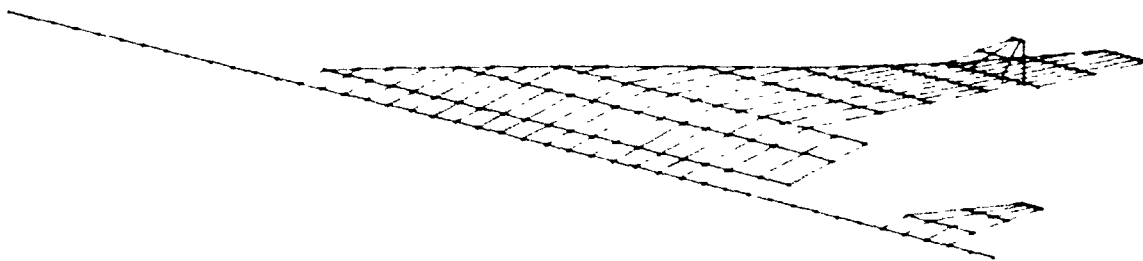


Figure 209-1. Structural Model, Design Demonstration

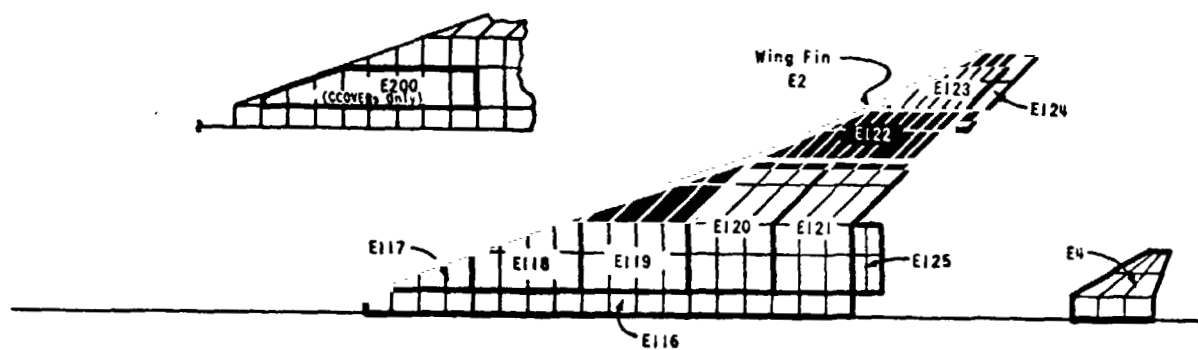


Figure 209-2. Element Subsets for Design

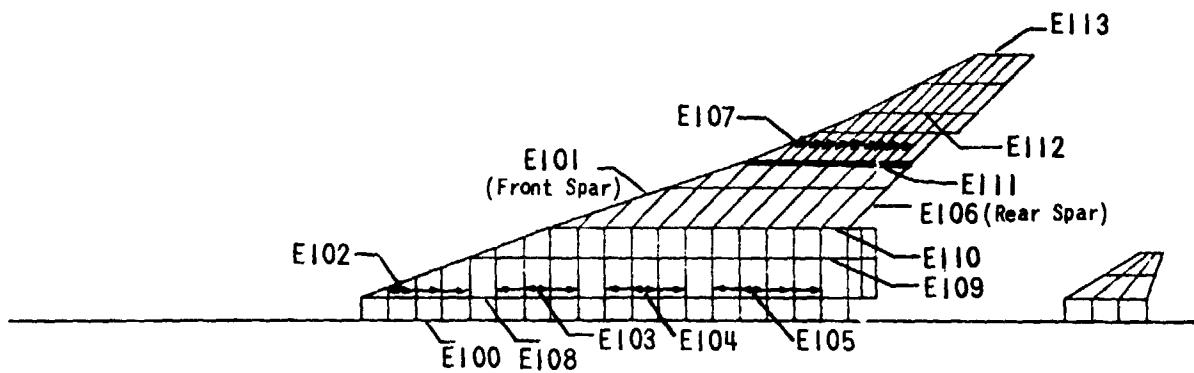


Figure 209-3. SPAR Element Subsets for Design

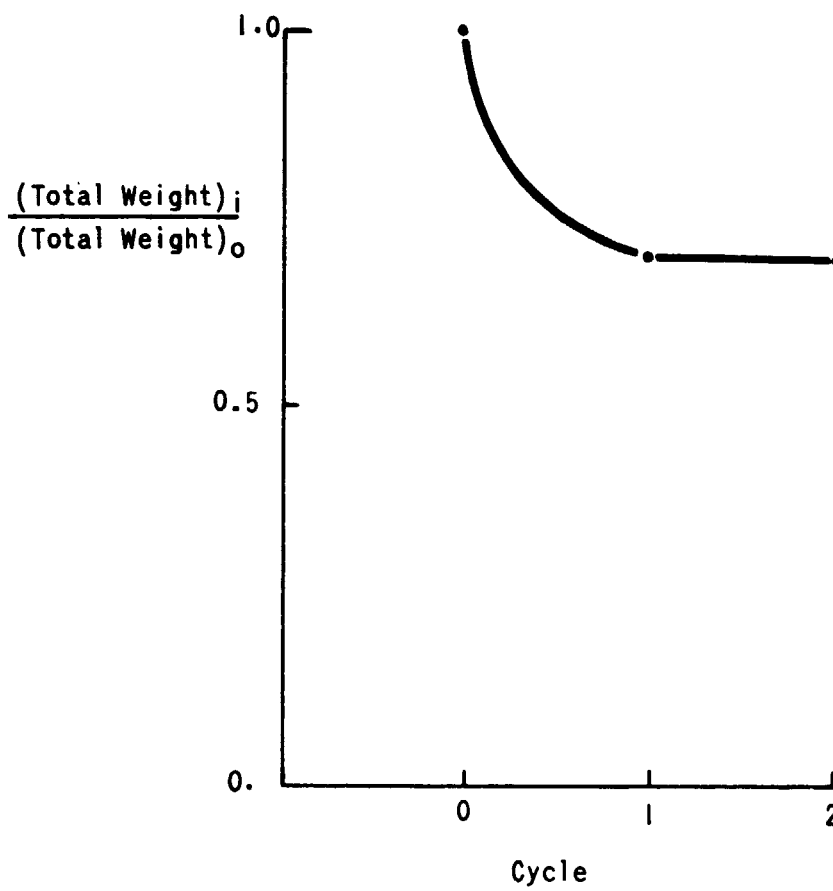


FIGURE 209-4. Total Weight vs. Cycle, Design Demonstration

T(0)U/T(0)L

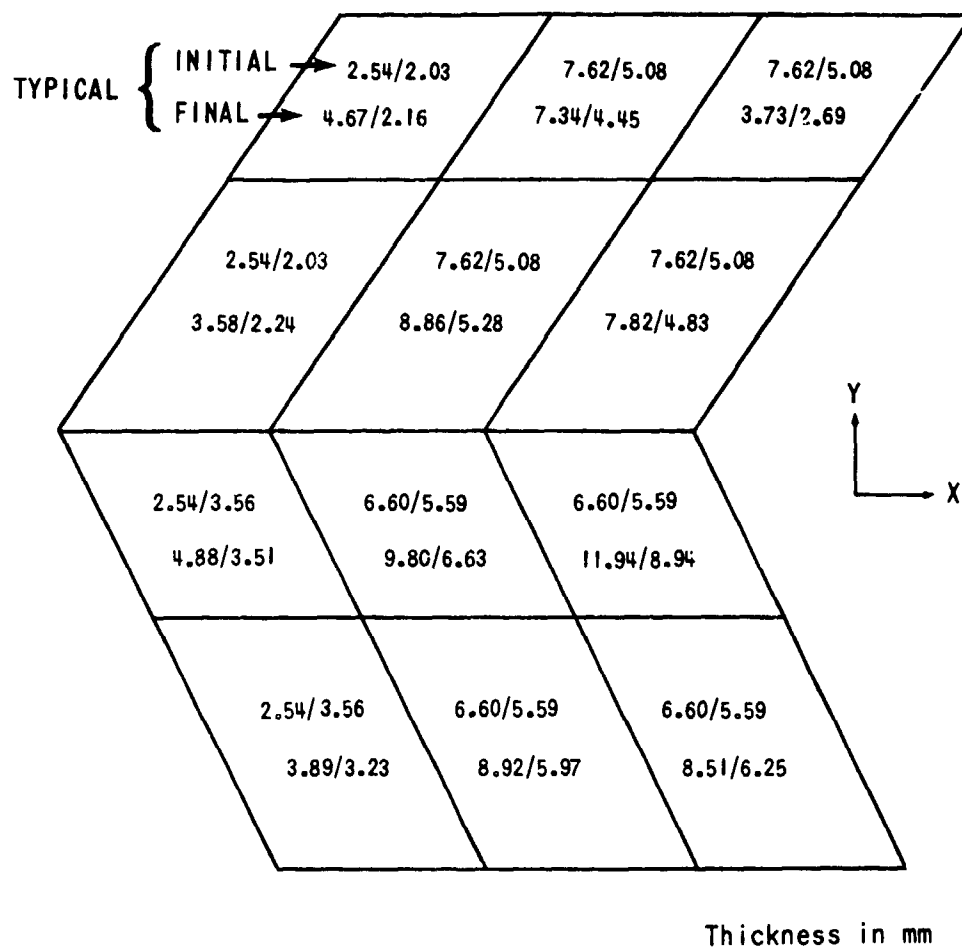


Figure 209-5. Surface Thickness Changes, Element Subset 121

PLOT ID = MARGINS. COVSMS .CYCLE = 1

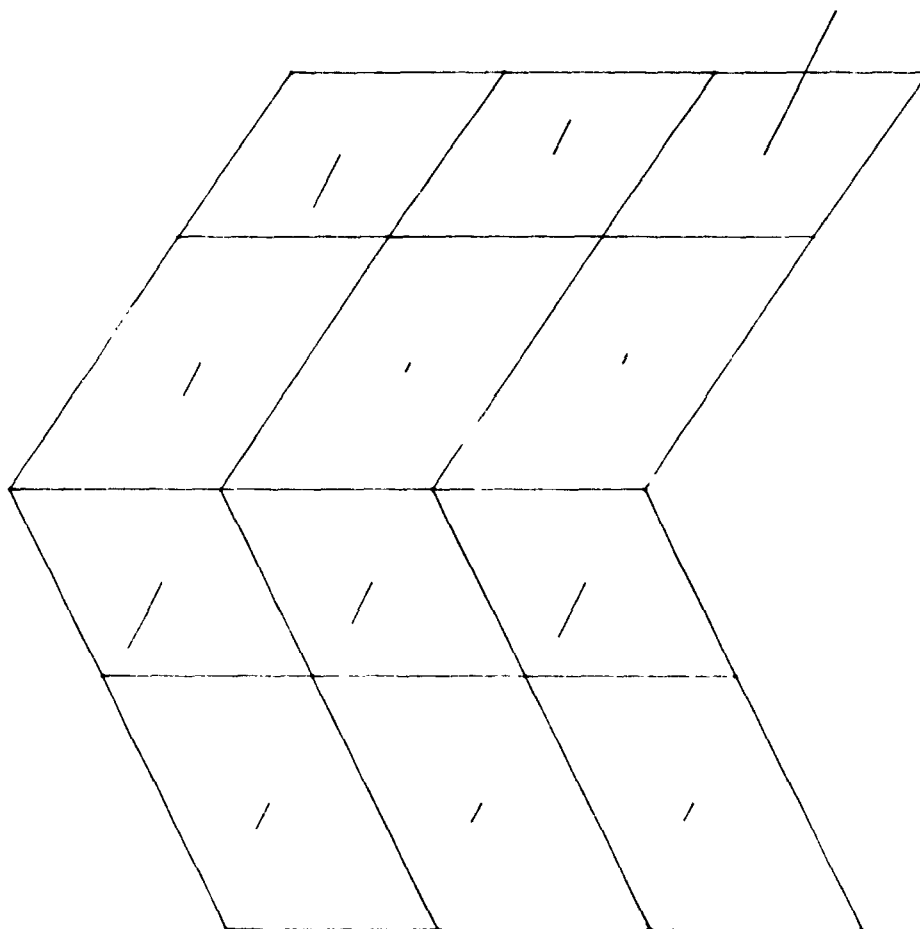


Figure 209-6. Margins of Safety, Cycle 1. Element Subset 121

PLOT 10 = MARGINS, COVSMS .CYCLE = 2

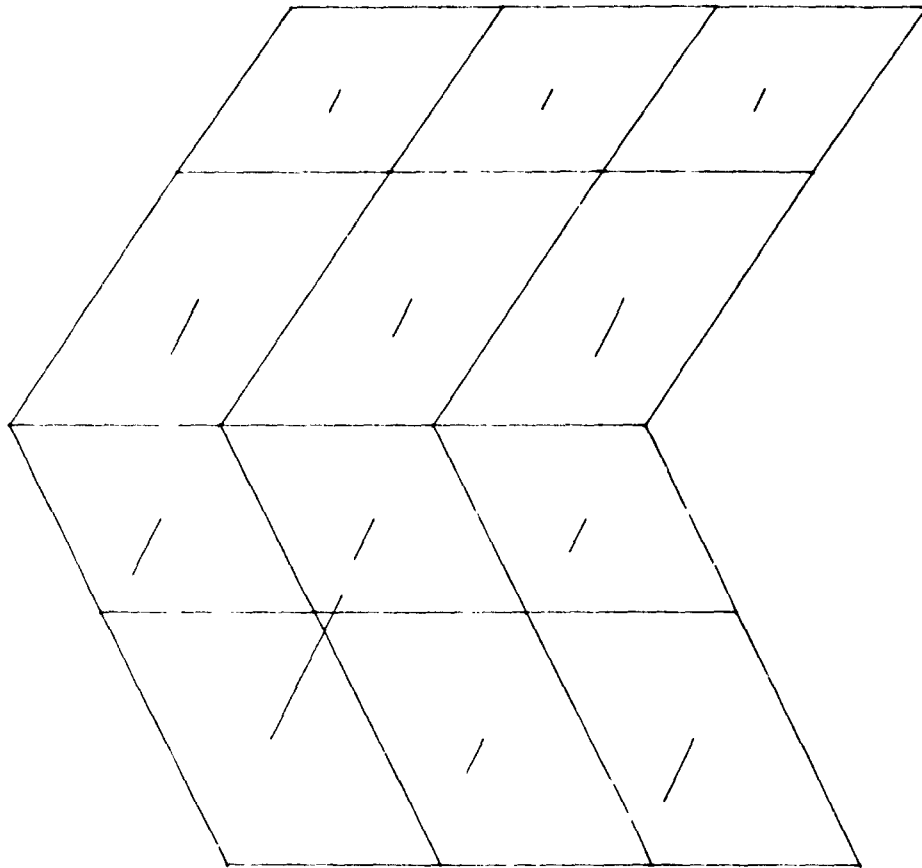


Figure 209-7. Margins of Safety, Cycle 2, Element Subset 121

210. THERMAL FULLY STRESSED DESIGN (DECK 17)

210.1 DESCRIPTION OF PROBLEM

This demonstration problem consists of a thermal fully stressed design of the well-known 25-bar transmission tower. The model and loading are based upon the information shown in reference 210-1. The loading consists of nodal loads at four nodes and thermal loads at each node. The model is shown in figure 210-1.

The design is performed iteratively and terminated when the relative weight change is less than 5%. The starting point for the design variables is unit area for all 25 ROD elements.

210.2 RESULTS

The analysis stabilized after two iterations to a relative weight change of less than 5%. The total weight compares quite favorably with that reported in reference 210-1. A plot of weight vs. design cycle is shown in figure 210-1. Thermal margins of safety for the elements on one face of the tower are shown in figure 210-3.

210.3 LISTING OF CONTROL PROGRAM AND DATA

```

BEGIN CONTROL MATRIX PROGRAM DEMO17
PROBLEM IGIDEMO17 - THERMAL DESIGN OF A 25-BAR TRUSS)

C
C PURPOSE      THE PRINCIPAL CAPABILITIES DEMONSTRATED BY THIS
C              DECK ARE
C              1. THERMAL DESIGN
C              2. PLOTS OF THERMAL MARGINS OF SAFETY
C
C AUTHOR      BJORN BACKMAN
C
C CCRE        145K (OCTAL)
C
C USER COMMON (BEGCYCL,ENDCYCL,CURCYCL,CONVERG,ISSET,ISTAGE,IPCS)
C INTEGER BEGCYCL,CURCYCL,ENDCYCL
C DIMENSION CONVERG(17)
C CONVERG(15) = .05
C CONVERG(16) = 1.0
C ENDCYCL = 5
C READ INPUT
C PRINT INPUT(NCDAL)
C PRINT INPUT(STIFFNESS)
C EXECUTE EXTRACT(EXNAME=GECM,LSUB=KGRID,ESUB=E1,ASUB=A1)
C EXECUTE GRAPHICS(IGNAME=GECM,OFFLINE=CALCOMP,TYPE=ORTH,SIZE=(15.,
C              15.),LABEL=N,RZ=20.,RY=10.,RX=0.,EXNAME=GECM)
C IF(BEGCYCL .LT. 1) BEGCYCL=1
C IF(ENDCYCL .LT. BEGCYCL) ENDCYCL=BEGCYCL
C CURCYCL = BEGCYCL
C IF(BEGCYCL .EQ. 1) GO TO 70001
C
C THIS IS A RESTART,
C LOAD PANDOM FILES FROM SAVESS4
C
C      LOAD FILES(SAVESS4=REWIND)
C      SAVE MATRIX(SAVESS4=PEWIND,MEFGRNF,D31)
C      GO TO 70002
70001 CONTINUE
C
C BEGCYCL = 1,
C COMPUTE AND PRINT INITIAL WEIGHT
C
C      EXECUTE MASS(SET=1)
70002 CONTINUE
C      CALL DESCONS
C      IF(CURCYCL .EQ. 0) CALL EXIT
C
C DESIGN CYCLES BEGCYCL THROUGH ENDCYCL
C
70003 CONTINUE
C      EXECUTE STIFFNESS(SET=1,LLMP=C.C)
C      EXECUTE MERGE(STIFFNESS,SET=1,STAGE=1,K11=11,K13=13,K33=33)
C      EXECUTE LCADS(SET=1,STAGE=1,LC=ALL,MATERIAL=CGNSTANT)
C      EXECUTE MERGE(LOADS,SET=1,STAGE=1,L11=11,L31=31)
C      IF(CURCYCL .GT. 1) GO TO 70004
C
C FIRST CYCLE, MERGE AND SAVE SUPPORT DISPLACEMENTS
C
C      EXECUTE MERGE(DISPLACEMENT,SET=1,STAGE=1,D31=31)
C      SAVE MATRIX(SAVESS4=PEWIND,MEFGRNF,D31)
70004 CONTINUE
C      EXECUTE MULTIPLY(TEMP=(L11-K13*D31))
C      EXECUTE CHOLSKY(SOLVE,K11,D11,TEMP)
C      IF(CURCYCL .EQ. ENDCYCL) GO TO 70005

```



```

BEGIN MATERIAL DATA /
MS1 .101 /
0 1.E7 .3 3.8E6 0. 1.E7 .3 3.8E6 0. 1.E7 .3 3.8E6 .0
40.E3 *=17 /
500 1.E7 .3 3.8E6 6.4E-3 1.E7 .3 3.8E6 6.4E-3 1.E7 .3 3.8E6
6.4E-3 40.E3 *=17 /
END MATERIAL DATA /
BEGIN NODAL DATA /
1 0. -25. 200. /
2 0. +25. 200. /
3 -37.5 37.5 100. /
4 37.5 37.5 100. /
5 37.5 -37.5 100. /
6 -37.5 -37.5 100. /
7 -100. 100. 0. /
8 100. 100. 0. /
9 100. -100. 0. /
10 -100. -100. 0. /
END NODAL DATA /
BEGIN STIFFNESS DATA /
BEGIN ELEMENT DATA /
ROD MS1 N1 1 2 1. /
ROD MS1 N2 1 4 1. /
ROD MS1 N3 2 3 1. /
ROD MS1 N4 1 5 1. /
ROD MS1 N5 2 6 1. /
ROD MS1 N6 2 4 1. /
ROD MS1 N7 2 5 1. /
ROD MS1 N8 1 3 1. /
ROD MS1 N9 1 6 1. /
ROD MS1 N10 3 6 1. /
ROD MS1 N11 4 5 1. /
ROD MS1 N12 3 4 1. /
ROD MS1 N13 5 6 1. /
ROD MS1 N14 3 10 1. /
ROD MS1 N15 6 7 1. /
ROD MS1 N16 4 9 1. /
ROD MS1 N17 5 8 1. /
ROD MS1 N18 4 7 1. /
ROD MS1 N19 3 8 1. /
ROD MS1 N20 5 10 1. /
ROD MS1 N21 6 9 1. /
ROD MS1 N22 6 10 1. /
ROD MS1 N23 3 7 1. /
ROD MS1 N24 5 9 1. /
ROD MS1 N25 4 8 1. /
END ELEMENT DATA /
END STIFFNESS DATA /
BEGIN BC DATA /
SET 1 STAGE 1 /
SUPPORT TX TY TZ FOR 7 8 9 10 /
END BC DATA /
BEGIN LOADS DATA /
SET 1 STAGE 1 /
BEGIN NODAL LOADS DATA /
FREEDOM FX1 FY1 FZ1 FX2 FY2 FZ2 FX3 FX6 /
1 1000. 10000. -5000. 10000. 10000. -5000. 500. 500. /
END NODAL LOADS DATA /
BEGIN NODAL THERMAL LOADS DATA /
CASE 2 /
1 2 100. /
3 TO 6 30. /
7 TO 10 -35. /
END NODAL THERMAL LOADS DATA /
END LOADS DATA /
BEGIN SUBSET DEFINITION /
SUBSETS OF STIFFNESS SET 1 /
E1 = ALL /
N1 = ALL /
N2 = 1 5 6 9 10 /
E2 = ALL IN N2 /
END SUBSET DEFINITION /

```

BEGIN DESIGN DATA /
MODE 1 /
SET 1 /
BEGIN SIZING DATA /
MS1 /
END SIZING DATA /
STAGE 1 1 0 TH1 /
BEGIN THERMAL DATA /
CASE UFF U 1. 1 1. 2 /
END THERMAL DATA /
END DESIGN DATA /
END PROBLEM DATA /

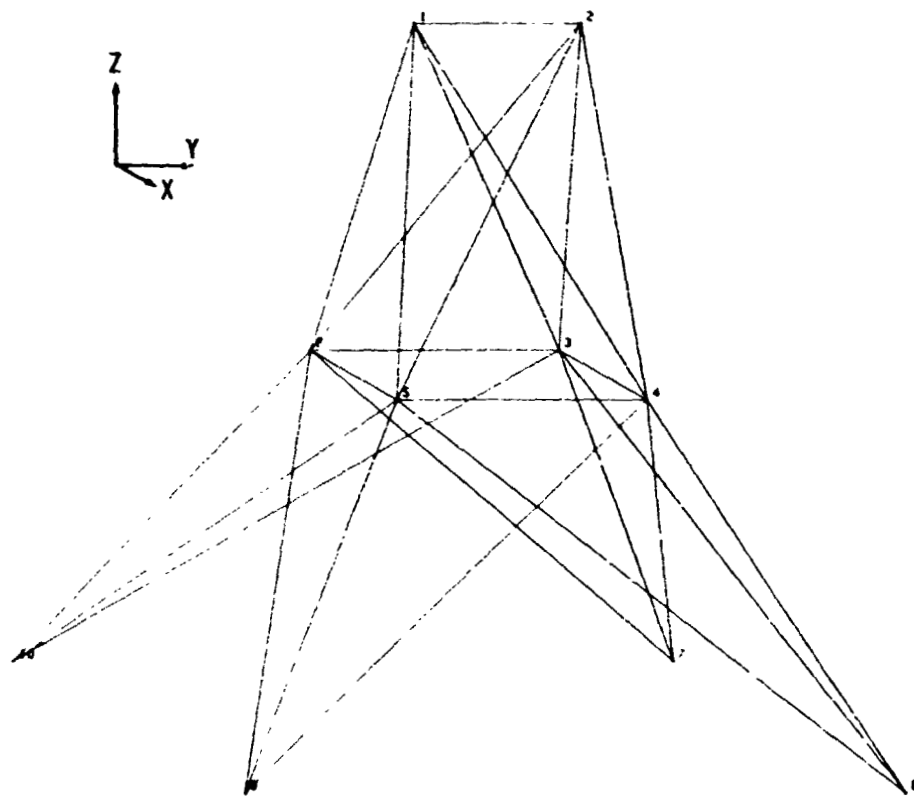


Figure 210-1. 25-Bar Transmission Tower Model

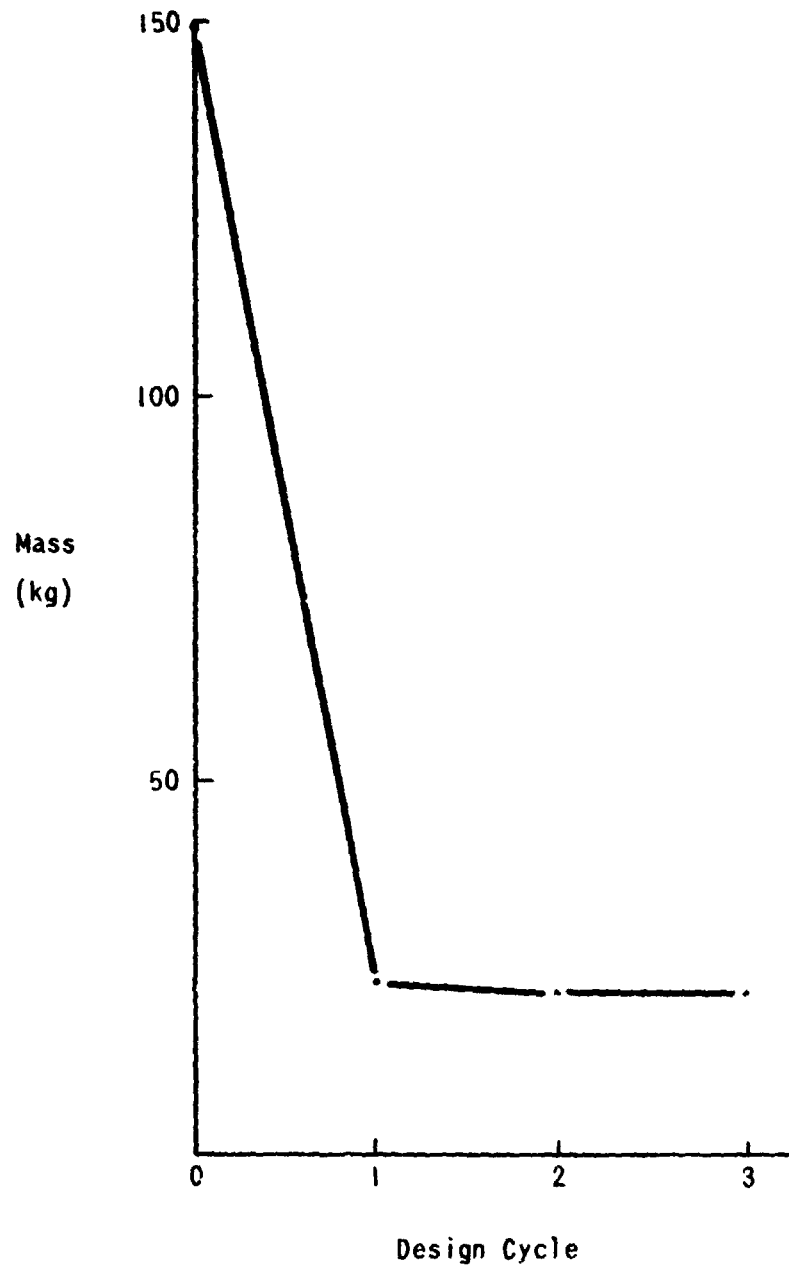


Figure 210-2. Total Mass vs. Design Cycle, 25-Bar Transmission Tower

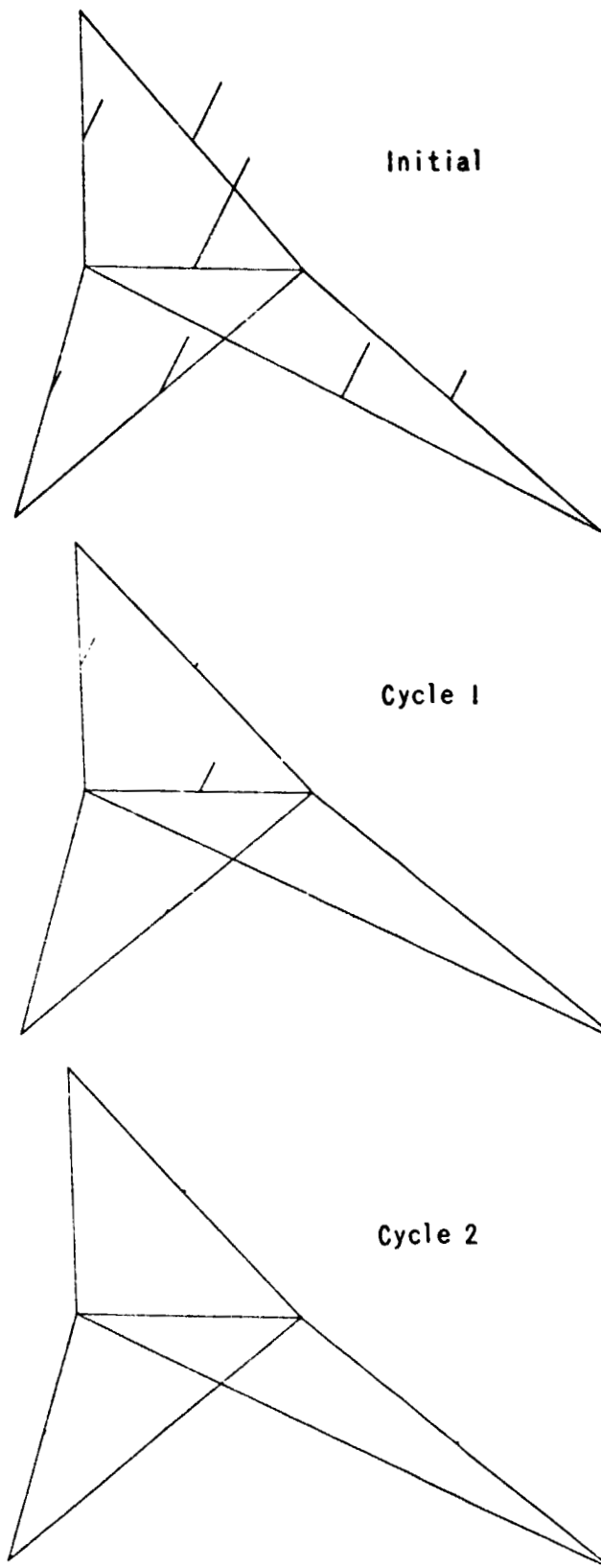


Figure 210-3. Thermal Margins of Safety, 25-Bar Transmission Tower

211. FLUTTER ANALYSIS OF AN SST AIRCRAFT (DECK 4)

211.1 DESCRIPTION OF ANALYSIS

Four separate flutter analyses of an SST aircraft are performed in this demonstration problem. The structural model, shown in figure 211-1, is the same as that described in section 203. The same degrees of freedom are retained in the vibration analysis; only the symmetric modes are considered.

The mass is modelled using mass plate elements as shown in figure 211-2. The mass of the stiffness elements is ignored.

The vibration analysis is performed using a reduced stiffness matrix and a non-diagonal reduced mass matrix produced directly by the Mass Processor.

All four flutter analyses employ the same set of generalized coordinates which are equivalent to the first twenty free-free symmetric vibration modes. The first flutter analysis, performed at Mach 0.8, is based on an aerodynamic model of the wing and tail using only the tail oscillations. Doublet Lattice airforce theory is used. Aerodynamic influence coefficients are obtained for four reduced frequencies. They are produced by FLEXAIR to obtain two sets of generalized airforces; the first set includes the effects of the flexibility of the truncated higher frequency modes of vibration, while the second set does not. V-g and V-f plots are obtained for both sets of generalized airforces. This analysis is shown schematically in figure 211-3.

The second flutter analysis is also based on the Doublet Lattice theory, but includes the wing, body and tail in the aerodynamic representation. Only the first ten generalized coordinates are used in the flutter analysis. This analysis is shown schematically in figure 211-4.

The third flutter analysis is performed at Mach 1.526 using Mach Box aerodynamics including the aerodynamic influence of the wing upon the tail. Only the lowest ten vibration modes are used. A consistent flutter speed and altitude consistent with the Mach number (matched point) is calculated. This analysis is shown schematically in figure 211-5.

The fourth flutter analysis is performed at Mach 0.8 using RH03 aerodynamics for the wing and control surfaces. Doublet Lattice aerodynamics are used for the tail with inter-surface aerodynamic interaction ignored. The flutter analysis is performed for several combinations of generalized coordinates. This analysis is shown schematically in figure 211-6.

211.2 RESULTS

Results of the flutter analyses are presented as V-q and V-f plots. Results of the first analysis are presented in figures 211-7 to 211-10. RESULTS of the second analysis are presented in figures 211-11 and 211-12.

211.3

LISTING OF CONTROL PROGRAM AND DATA

CCCCCCCCCCCC

```

EXECUTE INTERP (
L N57=(POLYNOMIAL,C77),MODE,A00=1.0,MODE,MODE,A10=10.0)
EXECUTE INTERP ( AIC=N99,
A N42=(1,CA42), DOF=1000,
D N43=(1,CA43), DOF=1000)

C
C
C   FLUTTER ANALYSIS USING DUBLAT WITH AND WITHOUT FLEXAIR

EXECUTE DUBLAT ( CASE=3, MACH=0.8, KVAL = (.005,.002,.0006,.0001))
EXECUTE FLEXAIR ( ID=FL01, DUBLAT, CASE=3, ALT=(0.0, 10000.0),
A FREEDOMS= (TZ263, RY263), SUBSET=N99)
PRINT OUTPUT (FLEXAIR, ID=FL01, ALT=0.0, KVAL= (.005,.002,.0001))
EXECUTE FLEXAIR ( ID=FL02, DUBLAT, CASE=3,
A FLUTFREQ=0.0, FREEDOMS=(TZ263, RY263), SUBSET=N99, ALT=0.0)
PRINT OUTPUT (FLEXAIR, ID=FL02)
EXECUTE ADDINT (ID=AFD, INT, FLEXAIR=FL01)
EXECUTE FLUTTER (GAFID= AFD, COND=4, VMAX=2000.0)
PRINT OUTPUT (FLUTTER, CASE=1, COND=4)
EXECUTE EXTRACT (EXNAME=FLPL4D, LSUB=VGVF, COND=4)
EXECUTE GRAPHICS (GNAME=FLPL4D, TYPE=GRAPH, X=V, Y1=G, Y2=F,
1 XMIN=0.0, XMAX=1000.0, Y1MIN=-.1, Y1MAX=.1, Y2MIN=0.0, Y2MAX=9.0,
2 SIZE=(6,6),EXNAME=FLPL4D)
EXECUTE ADDINT (ID=AFE, INT, FLEXAIR=FL02)
EXECUTE FLUTTER (GAFID= AFE, COND=5, VMAX=2000.0)
PRINT OUTPUT (FLUTTER, CASE=1, COND=5)
EXECUTE EXTRACT (EXNAME=FLPL4E, LSUB=VGVF, COND=5)
EXECUTE GRAPHICS (GNAME=FLPL4E, TYPE=GRAPH, X=V, Y1=G, Y2=F,
1 XMIN=0.0, XMAX=1000.0, Y1MIN=-.1, Y1MAX=.1, Y2MIN=0.0, Y2MAX=9.0,
2 EXNAME=FLPL4E)

```

```

C
C
C   FLUTTER ANALYSIS USING DUBLAT FOR WING, TAIL, AND BODY.
C   ADDITIONAL AIRFORCES FROM ADDINT.

PRINT INPUT (DUBLAT, CASE=2 )
EXECUTE DUBLAT (CASE=2, MACH=0.8, BREF=1000.0, QUASI=WT,
A KVAL= (5.0, 2.0, 1.0, 0.6, 0.2))
PRINT OUTPUT (DUBLAT, CASE=2, LEVEL= (1,2,3,4,5))
EXECUTE ADDINT (ID = AFB,INT,DUBLAT,CASE=2,GET=73 )
PRINT OUTPUT (ADDINT, ID=AFB, KVAL= (2.0, 1.2, 0.6, 0.3))
EXECUTE FLUTTER (GAFID=AFB, COND=2,
A STILL,NMODES=10,ITER=3,DENSITY=.0020482)
PRINT OUTPUT (FLUTTER, CASE=1, COND=2)
EXECUTE EXTRACT (EXNAME=FLPL4B, LSUB=VGVF, COND=2)
EXECUTE GRAPHICS (GNAME=FLPL4B, TYPE=GRAPH, X=V, Y1=G, Y2=F,
1 XMIN=0.,XMAX=1000.,Y1MIN=-1.,Y1MAX=1.,Y2MIN=0.,Y2MAX=10.,
2 EXNAME=FLPL4B)

```

```

C
C
C   FLUTTER ANALYSIS USING MACHBOX FOR 2 NON-COPLANAR SURFACES
C   WITH SUBSONIC LEADING EDGES
C

PRINT INPUT (MACHBOX)
EXECUTE MACHBOX ( MACH=1.5, COND=1, BREF=1000.0 ,
A KVAL = ( 10.0, 2.0, 1.0, 0.4 , 0.15 ))
PRINT OUTPUT (MACHBOX, LEVEL=(1,4))
EXECUTE ADDINT (ID=AFB,INT,MACHBOX,IGET=140)
PRINT OUTPUT (ADDINT,ID=AFB)
PRINT INPUT (FLUTTER)
EXECUTE FLUTTER (GAFID=AFB, COND=3,
B EVEC=FLUTTER, AVEC=FLUTTER,
A NMODES=10,NKF=40,MP5=5000.0,NALT=3)
PRINT OUTPUT (FLUTTER, CASE=1, COND=3)
EXECUTE EXTRACT (EXNAME=FLPL4C, LSUB=VGVF, COND=3)
EXECUTE GRAPHICS (GNAME=FLPL4C, TYPE=GRAPH, X=V, Y1=G, Y2=F,
1 XMIN=420.,XMAX=2000.,Y1MIN=-.237,Y1MAX=.568,Y2MIN=1.,Y2MAX=5.,
2 EXNAME=FLPL4C)

```

ORIGINAL PAGE IS
OF POOR QUALITY

```

C   FLUTTER ANALYSIS USING RHO3 FOR WING WITH CONTROL SURFACES AND
C   DUBLAT FOR TAIL. RESULTS COMBINED USING ADDINT.
C
PRINT INPUT (RHO3)
EXECUTE RHO3 ( MACH = 0.8,
A KVALUES = ( 0.005, 0.002, 0.001, 0.0007, 0.0004,0.0001))
PRINT OUTPUT (RHO3)
PRINT INPUT (DUBLAT )
EXECUTE DUBLAT (MACH=0.8,KVALUE=(5.0,2.0,1.0,0.7,0.4,0.1),
A BREF=1000.0, QUASI=TD )
PRINT OUTPUT (DUBLAT, LEVEL= (1,2,5))
EXECUTE ADDINT (ID= AFA,ADD,INT,RHO3,DUBLAT,IGAIN=25 )
PRINT OUTPUT (ADDINT, ID=AFA, KVAL= (.005, .001, .00076, .00025))
EXECUTE FLUTTER (GAFID=AFA, DENSITY=.0020482, GCROSS=(.03,.0,.05),
A VMIN= 500.0, VMAX=1500.0, FMIN=2.8, FMAX=3.5,
A EVAL=(1 TO 126 BY 20), EVEC=(FLUTTER, 1, 51, 101), AVEC=FLUTTER)
PRINT OUTPUT (FLUTTER, COND=1)
EXECUTE EXTRACT (EXNAME=FLPL4A, LSUB=VGVF,COND=1)
EXECUTE GRAPHICS (GNAME=FLPL4A, TYPE=GRAPH, X=V, Y1=G, Y2=F,
1 XMIN=0., XMAX=2000., Y1MIN=-.1, Y1MAX=.1, Y2MIN=0., Y2MAX=10.0,
3 EXNAME=FLPL4A)
EXECUTE GRAPHICS (GNAME=FLPL4A1, TYPE=GRAPH, X=V, Y1=G, Y2=F,
1 XMIN=500.,XMAX=1500.,Y1MIN=-.05, Y1MAX=.05, Y2MIN=2.8, Y2MAX=3.5,
2 EXNAME=FLPL4A)
E..J CONTROL PROGRAM

```

```

*/ MODE2 /
BEGIN MACHBOX DATA
LABEL DEMONSTRATION PROBLEM - BOTH SURFACES
BEGIN GEOM
BOX 12 XCENTER 2710.0
SURFACE 1
LEADING EDGE 510.0 0.0 741.0 65.1 2065.0 455.0 2487.0 594.0 2884.0 794.0
TRAILING EDGE 2715.0 0.0 2715.0 65.1 2697.0 228.0 2749.0 455.0 2874.059 594.0 +
3054.0 794.0
SURFACE 2 0.0 20.0 0.2
LEADING EDGE 2985.0 0.0 3124.0 65.1 3386.0 228.0
TRAILING EDGE 3400.0 0.0 3417.0 65.1 3464.0 228.0
END GEOM
BEGIN MODAL DATA
USE C062 WITH SURFACE 1
USE C053 WITH SURFACE 2
END MODAL DATA
END MACHBOX DATA
BEGIN RH03 DATA
BEGIN GEOMETRY DATA
MAIN SURFACE MS1
LEADING EDGE 510.0 0.0 741.0 65.1 2065.0 455.0 2487.0 594.0 2884.0 794.0
TRAILING EDGE 2715.0 0.0 2715.0 65.1 2697.0 228.0 2749.0 455.0 2874.059 594.0 +
3054.0 794.0
DOWNWASH BAR +
CHORD 0.2 -0.86 -0.64 -0.3 0.3 0.64 0.86 +
CHORD 0.45 -0.86 -0.64 -0.3 0.3 0.64 0.86 +
CHORD 0.65 -0.86 -0.64 -0.3 0.3 0.64 0.86 +
CHORD 0.78 -0.86 -0.64 -0.3 0.3 0.64 0.86 +
CHORD 0.88 -0.86 -0.64 -0.3 0.3 0.64 0.86 +
CHORD 0.95 -0.86 -0.64 -0.3 0.3 0.64 0.86
CONTROL SURFACE CS1 HINGE 2500.0 65.0 2500.0 265.0 +
MODE 1 0.0 0.0 0.0 0.0 +
MODE 2 0.0 0.0 0.0 0.0 +
MODE 3 0.0 0.0 0.0 0.0 +
MODE 4 0.0 0.0 0.0 0.0 +
MODE 5 0.0 0.0 0.0 0.0 +
MODE 6 0.0 0.0 0.0 0.0 +
MODE 7 0.0 0.0 0.0 0.0 +
MODE 8 0.0 0.0 0.0 0.0 +
MODE 9 0.0 0.0 0.0 0.0 +
MODE 10 0.0 0.0 0.0 0.0 +
MODE 11 0.0 0.0 0.0 0.0 +
MODE 12 0.0 0.0 0.0 0.0 +
MODE 13 0.0 0.0 0.0 0.0 +
MODE 14 0.0 0.0 0.0 0.0 +
MODE 15 0.0 0.0 0.0 0.0 +
MODE 16 0.0 0.0 0.0 0.0
CONTROL SURFACE CS2 HINGE 2769.0 538.0 2995.0 765.0
END GEOMETRY DATA
BEGIN MODAL DATA
USE C042 WITH MAIN SURFACE
USE C55 WITH CONTROL SURFACE CS1
USE C056 WITH CONTROL SURFACE CS2
END MODAL DATA
BEGIN OPTION DATA
LABEL DEMONSTRATION PROBLEM - TWO CONTROL SURFACES
SECTIONAL FORCES
PRESSURE REPORT
VELOCITY PROFILE DLE1 1. DTE1 1. 0.0 1.00001 0.5 1.00002 1.0 1.0
END OPTION DATA
END RH03 DATA
BEGIN DUBLAT DATA
CASE 1
BEGIN GEOMETRY DATA
LIFTING SURFACE DATA
PANEL T1 2985.0 3365.0 3386.0 3464.0 0.0 228.0 0.0 0.0

```

CHORD DIV 0.0 0.2 0.4 0.6 0.8 1.0
 SPAN DIV 0.0 0.25 0.5 0.75 1.0
 PANEL T2 3365.0 3400.0 3446.0 3464.0 0.0 228.0 0.0 0.0
 CHORD DIV 0.0 1.0
 SPAN DIV 0.0 0.25 0.5 0.75 1.0
 END GEOMETRY DATA
 BEGIN SUBSET DATA
 SUBSETS OF BOXES
 SUBSET 1 1 TO 20
 SUBSET 2 21 TO 24
 END SUBSET DATA
 BEGIN MODAL DATA
 USE COS3 WITH LIFTING SURFACE 1
 USE COS7 WITH LIFTING SURFACE 2
 END MODAL DATA
 CASE 2
 BEGIN GEOMETRY DATA
 LIFTING SURFACE DATA
 PANEL W1 741.0 2500.0 1419.8 2500.0 65.1 265.0 0.0 0.0
 CHORD DIV 0.0 0.25 0.5 0.75 1.0
 SPAN DIV 0.0 1.0
 PANEL W2 1419.8 2500.0 2029.0 2500.0 265.0 329.5 0.0 0.0
 CHORD DIV 0.0 0.25 0.5 0.75 1.0
 SPAN DIV 0.0 1.0
 PANEL W2A 2500.0 2715.0 2500.0 2715.0 265.0 329.5 0.0 0.0
 CHORD DIV 0.0 1.0
 SPAN DIV 0.0 1.0
 PANEL W3 2028.0 2500.0 2487.0 2825.0 329.5 594.0 0.0 0.0
 CHORD DIV 0.0 0.25 0.5 0.75 1.0
 SPAN DIV 0.0 0.4 0.7 0.9 1.0
 PANEL W3A 2500.0 2715.0 2825.0 2874.0 329.5 594.0 0.0 0.0
 CHORD DIV 0.0 1.0
 SPAN DIV 0.0 0.4 0.7 0.9 1.0
 PANEL W4 2487.0 2825.0 2884.0 3023.087 594.0 794.0 0.0 0.0
 CHORD DIV 0.0 0.25 0.5 0.75 1.0
 SPAN DIV 0.0 0.5 0.8 1.0
 PANEL CS1 2500.0 2715.0 2500.0 2715.0 65.1 265.0 0.0 0.0
 CHORD DIV 0.0 1.0
 SPAN DIV 0.0 1.0
 PANEL CS2 2825.0 2874.0 3023.087 3051.0 594.0 794.0 0.0 0.0
 CHORD DIV 0.0 1.0
 SPAN DIV 0.0 0.5 0.8 1.0
 PANEL WF 2487.0 2874.0 2880.0 2940.0 594.0 594.0 0.0 134.0
 CHORD DIV 0.0 0.5 1.0
 SPAN DIV 0.0 0.65 1.0
 PANEL T1 3124.0 3380.0 3386.0 3446.0 65.1 228.0 0.0 0.0
 CHORD DIV 0.0 0.5 1.0
 SPAN DIV 0.0 0.7 1.0
 PANEL T2 3380.0 3417.0 3446.0 3464.0 65.1 228.0 0.0 0.0
 CHORD DIV 0.0 1.0
 SPAN DIV 0.0 0.7 1.0
 INTERFERENCE SURFACE DATA
 BODY B1
 PANEL B1 0.0 600.0 594.0 600.0 0.0 65.1 -65.1 0.0
 CHORD DIV 0.0 1.0
 SPAN DIV 0.0 1.0
 PANEL B2 0.0 600.0 594.0 600.0 0.0 65.1 65.1 0.0
 CHORD DIV 0.0 1.0
 SPAN DIV 0.0 1.0
 PANEL B3 600.0 3654.0 600.0 3654.0 0.0 65.1 -65.1 0.0
 CHORD DIV 0.0 0.1 0.2 0.3 0.4 0.5 0.6 0.7 0.8 0.9 1.0
 SPAN DIV 0.0 1.0
 PANEL B4 600.0 3654.0 600.0 3654.0 0.0 65.1 65.1 0.0
 CHORD DIV 0.0 0.1 0.2 0.3 0.4 0.5 0.6 0.7 0.8 0.9 1.0
 SPAN DIV 0.0 1.0
 DOUBLET DATA
 BODY B1 ZDOUBLET
 AXIS DIV 0.0 600.0 3564.0
 RADII 0.0 65.1 65.1
 END GEOMETRY DATA

BEGIN SUBSET DATA
 SUBSETS OF BOXES
 SUBSET B1 1 TO 41
 SUBSET B2 42
 SUBSET B3 43 TO 45
 SUBSET B4 46 TO 49
 SUBSET B5 50 TO 53
 SUBSET B6 54 TO 55
 SUBSETS OF STRIPS
 SUBSET S1 1 15
 END SUBSET DATA
 BEGIN MODAL DATA
 USE C042 WITH LIFTING SURFACE B1
 USE C053 WITH LIFTING SURFACE B5
 USE C044 WITH LIFTING SURFACE B4
 USE C045 WITH LIFTING SURFACE B2
 USE C056 WITH LIFTING SURFACE B3
 USE C057 WITH LIFTING SURFACE B6
 USE C51 WITH BODY DOUBLET B1
 USE C51 WITH INTERF BODY B1
 END MODAL DATA
 BEGIN OPTION DATA
 VELOCITY PROFILES
 PROFILE P1 0.0 1.0 0.3 1.2 0.6 1.1 1.0 1.0
 USE P1 ON S1
 PRESSURE CORRECTIONS
 USE 0.85 0.0 AS SCALAR ON B3 B4
 END OPTION DATA
 CASE 3
 BEGIN GEOMETRY DATA
 LIFTING SURFACE DATA
 PANEL W0 510.0 2715.0 741.0 2715.0 0.0 65.1 0.0 0.0
 CHORD DIV 0.0 0.2 0.4 0.6 0.8 1.0
 SPAN DIV 0.0 1.0
 PANEL W1 741.0 2715.0 2055.0 2749.0 65.1 455.0 0.0 0.0
 CHORD DIV 0.0 0.2 0.4 0.6 0.8 1.0
 SPAN DIV 0.0 0.3 0.5 0.65 0.8 0.9 1.0
 PANEL W2 2065.0 2749.0 2437.0 2874.0 455.0 594.0 0.0 0.0
 CHORD DIV 0.0 0.2 0.4 0.6 0.8 1.0
 SPAN DIV 0.0 0.4 0.7 0.9 1.0
 PANEL W3 2437.0 2874.0 2884.0 3054.0 594.0 794.0 0.0 0.0
 CHORD DIV 0.0 0.2 0.4 0.6 0.8 1.0
 SPAN DIV 0.0 0.4 0.7 0.9 1.0
 PANEL T0 2985.0 3400.0 3124.0 3417.0 0.0 65.1 0.0 0.0
 CHORD DIV 0.0 0.2 0.4 0.6 0.8 1.0
 SPAN DIV 0.0 1.0
 PANEL T1 3124.0 3417.0 3366.0 3464.0 65.1 228.0 0.0 0.0
 CHORD DIV 0.0 0.2 0.4 0.6 0.8 1.0
 SPAN DIV 0.0 0.4 0.65 0.85 1.0
 END GEOMETRY DATA
 BEGIN SUBSET DATA
 SUBSETS OF BOXES
 SUBSET WING 1 TO 75
 SUBSET TAIL 76 TO 100
 END SUBSET DATA
 BEGIN MODAL DATA
 USE C443 WITH LIFTING SURFACE TAIL
 END MODAL DATA
 END DOUBLAT DATA
 BEGIN FLUTTER DATA
 CASE 1
 ALTITUDE 0. 10000.
 DAMPING 0. 0. 0.02 0.02 0.05
 CASE 2
 RSET 1 1 2 3 4 5 6 7 8
 RSET 2 1 2 3 4 5 6 7 8 9 10 11 12
 RSET 3 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20
 RSET 4 3 4 5 6 7 8
 CSET 1 *8 NOMINAL CASE 8
 RSET 1 2 3 4

ALT 10000.0 50000.0

CSET 2 *C WITH ADDED STIFFNESS IN MODES 3 AND 4 &
STIFF SS 3 3 TO 4 4 BY 1 1 1.2

RSET 1

END FLUTTER DATA

BEGIN NODAL DATA

*/

*/ BODY NODES

*/

1	20.	0.	0.		TO	25	980.	0.	0.		BY	2
27	1060.	C.	0.	30.0	TO	45	1780.	0.	0.	42.5	BY	2
*+1 200	0.	65.	0.	0.	TO	0	200	0.	65.		**	
45					TO	55	2180.	0.	0.	31.0	BY	2
*+1 200					TO	0	200	0.	65.		**	
55					TO	63	2500.	0.	0.	13.5	BY	2
*+1 200					TO	0	200	0.	65.		**	
65	2580.	C.	0.		TO	77	3060.	0.	0.		BY	2
79	3140.	C.	0.	3.0								
*+1 200	0.	65.		**								
81	3220.	C.	0.	6.5								
*+1 200	0.	65.		**								
83	3300.	C.	0.	7.0								
*+1 200	0.	65.		**								
85	3380.	C.	0.	2.0								
*+1 200	0.	65.		**								
87	3460.	C.	0.									
89	3540.	C.	0.									

*/

*/ WING NODES

*/

427	1060.	65.	0.	30.0	TO	435	1380.	180.	0.	17.5	BY	2
435					TO	445	1760.	180.	0.	27.5	BY	2
445					TO	455	2180.	180.	0.	25.0	BY	2
455					TO	463	2500.	180.	0.	13.0	BY	2
635	1380.	180.	0.	17.5	TO	641	1620.	265.	0.	10.0	BY	2
641					TO	655	2180.	265.	0.	22.5	BY	2
655					TO	663	2500.	265.	0.	12.5	BY	2
841	1620.	265.	0.	10.0	TO	847	1971.	380.	0.	9.0	BY	2
847					TO	855	2291.	380.	0.	17.0	BY	2
855					TO	863	2611.	380.	0.	10.0	BY	2
1047	1971.	380.	0.	9.0	TO	1051	2205.	455.	0.	8.5	BY	2
1051					TO	1059	2525.	455.	0.	15.0		
1059					TO	1063	2685.	455.	0.	8.0		
1251	2205.	455.	0.	8.5	TO	1254	2409.	538.	0.	6.5		
1254					TO	1259	2609.	538.	0.	11.0		
1259					TO	1263	2769.	538.	0.	5.5		
1454	2409.	538.	0.	6.5	TO	1456	2545.	594.	0.	5.0		
1456					TO	1459	2605.	594.	0.	7.5		
1459					TO	1463	2825.	594.	0.	3.5		
1656	2545.	594.	0.	5.0	TO	1658	2710.	680.	0.	3.0		
1658					TO	1663	2910.	680.	0.	3.0		
1858	2710.	680.	0.	3.0	TO	1860	2875.	765.	0.	1.5		
1860					TO	1863	2995.	765.	0.	2.5		

*/

*/ WING TRAILING EDGE NODES

*/

3001	2500.	65.	0.	13.5	TO	3005	2715.	65.	0.	1.0	BY	2
3101	2500.	180.	0.	13.0	TO	3105	2715.	180.	0.	1.0	**	
3201	2500.	265.	0.	12.5	TO	3205	2715.	265.	0.	1.0	**	
3405	2874.	594.	0.	1.0	TO	3605	3027.9	765.	0.	1.0		

BY 100 OF 86. 85.

*/

*/ WING FIN NODES

*/

REC	WINGFIN	0.	594.	0.	1.	594.	0.	0.	-1.	0.		
2056	2545.	.1	0.	3.5	TO	2456	2830.	100.	0.	2.5	BY	200
2058	2625.	.1	0.	3.5	TO	2458	2842.	100.	0.	3.0	**	
2061	2745.	.1	0.	4.0	TO	2461	2859.	100.	0.	3.0	**	
2063	2825.	.1	0.	4.0	TO	2463	2870.	100.	0.	3.0	**	

*/

*/ HORIZONTAL TAIL NODES

*/

RESUME GLOBAL

279					TO	679	3365.	200.	0.	2.0	BY	200
281					TO	681	3388.	200.	0.	2.5	**	
283					TO	683	3412.	200.	0.	2.5	**	
285					TO	685	3435.	200.	0.	1.0	**	

*/

*/

*/

WEIGHT PANEL NODES - BODY

6001	0.	0.	0.	TO	6016	3564.	0.	0.
6021	0.	65.	0.	TO	6036	3564.	65.	0.

*/

*/

*/

WEIGHT PANEL NODES - WING

6100	741.0	65.0	0.	TO	6220	2487.0	594.0	0.	BY	20
6100				TO	6260	2487.0	594.0	0.	BY	80
6180				TO	6240	2487.0	594.0	0.	BY	20
6260				TO	6320	2884.0	794.0	0.	BY	20
6110	2715.0	65.0	0.	TO	6170	2715.0	329.5	0.	BY	20
6189	2715.0	329.5	0.	TO	6249	2874.0	594.0	0.	BY	20
6266	2874.0	594.0	0.	TO	6326	3054.0	794.0	0.	BY	20

*/+3

6100	TO	6110
20	0	20

*/+3

6180	TO	6189
20	0	20

*/+3

6260	TO	6266
20	0	20

*/

*/

WEIGHT PANEL NODES - HORIZONTAL TAIL

6400	3124.	65.1	0.	TO	6403	3417.	65.1	0.
6410	3386.	228.0	0.	TO	6413	3464.	228.0	0.

*/

*/

*/

WEIGHT PANEL NODES - VERTICAL TAIL

6501	3374.6	0.	92.8
6502	3472.0	0.	92.8
6503	3458.7	0.	149.8
6504	3514.6	0.	149.8

*/

*/

*/

WEIGHT PANEL NODES - WING FIN

6601	2487.0	594.	0.	TO	6603	2880.0	594.	134.
6604	2874.059	594.	0.	TO	6606	2940.0	594.	134.

END NODAL DATA

BEGIN STIFFNESS DATA

BEGIN PROPERTY DATA

P1	.05	1.	*(WING FIN SPARS AND RIBS)					
P2	2.	0.	0.	.2	.2	.2	*(WING FIN ATTACHMENT BEAMS - TYPE 1)	
P3	10.	0.	0.	100.	100.	100.	*(WING FIN ATTACHMENT BEAMS - TYPE 2)	
P4	.15	.50	*(CONTROL SURFACE RIBS)					
P5	0.	*=2	100.	100.	0.	10.	*(BEAMS AT 455 RIB TO PICK UP SPARS)	

END PROPERTY DATA

BEGIN ELEMENT DATA

*/

*/

*/

WING FRONT SPAR

SPAR	M5	N2003	227	429	.12	2.				
*2		N2205	429	431	.12	2.	TO	N2605	433	435
							BY	N200	2	2
*2		N2805	435	637	.12	2.				
*2		N2007	637	639	.12	2.	TO	N3207	639	641
							BY	N200	2	2
*2		N3407	641	843	.12	2.				
*2		N3609	843	845	.12	2.	TO	N3809	845	847
							BY	N200	2	2
*2		N4009	847	1049	.12	2.				
*2		N4211	1049	1051		**				

*2	N4411	1051	1253		**				
*2	N4613	1253	1254		**				
*2	N4713	1254	1455		**				
*2	N4815	1455	1456		**				
*2	N4915	1456	1657		**				
*2	N5017	1657	1658		**				
*2	N5117	1658	1859		**				
*2	N5219	1859	1860		**				
*/									
*/ WING REAR SPAR									
*/									
SPAR	M5	N5603	263	453	.40	12.			
*2		N5605	463	663	.40	12.			
*2		N5607	663	863	.34	12.			
*2		N5609	863	1063	.34	12.			
*2		N5611	1063	1263	.30	8.			
*2		N5613	1263	1463	.30	8.			
*2		N5615	1463	1663	.30	4.			
*2		N5617	1663	1863	.30	4.			
*/									
*/ WING INTERMEDIATE SPARS									
*/									
SPAR	M5	N2203	229	429	.20	2.	TO N3603	243	443
							BY N200	2	2
*2		N3603	245	445	.36	2.			
*2		N4803	255	455	.60	12.			
*2		N5003	257	457	.24	12.	TO N5403	261	461
							BY N200	2	2
*2		N3005	437	637	.20	2.	TO N3605	443	643
							BY N200	2	2
*2		N3805	445	645	.36	2.			
*2		N4005	447	647	.20	4.	TO N4605	453	653
							BY N200	2	2
*2		N4805	455	655	.60	12.			
*2		N5005	457	657	.24	12.	TO N5405	461	661
							BY N200	2	2
*2		N3607	643	843	.20	2.	TO N3807	645	845
							BY N200	2	2
*2		N4007	647	847	.20	4.	TO N4607	653	853
							BY N200	2	2
*2		N4807	655	855	.20	8.			
*2		N5007	657	857	.20	10.	TO N5407	661	861
							BY N200	2	2
*2		N4209	849	1049	.20	4.	TO N4609	853	1053
							BY N200	2	2
*2		N4809	855	1055	.20	8.			
*2		N5009	857	1057	.20	10.	TO N5409	861	1061
							BY N200	2	2
*2		N4611	1053	1253	.12	4.	TO N4811	1055	1255
							BY N200	1	1
*2		N4911	1056	1256	.06	4.	TO N4811	1062	1262
							BY N200	1	1
*2		N4813	1255	1455	.12	4.			
*2		N4913	1256	1456	.06	4.	TO N5513	1262	1462
							BY N100	1	1
*2		N5015	1457	1657	.06	2.	TO N5515	1462	1662
							BY N100	1	1
*2		N5217	1659	1859	.06	2.	TO N5517	1662	1862
							BY N100	1	1
*/									
*/ WING IN-BODY SPARS									
*/									
SPAR	M5	N2001	27	227	1.00	10.	TO N3601	43	243
							BY N200	2	2
*2		N3801	45	245	1.80	10.	TO N4601	53	253
							BY N200	2	2
*2		N4801	55	255	3.00	60.			
*2		N5001	57	257	1.20	60.	TO N5401	61	261
							BY N200	2	2
*2		N5601	63	263	2.00	60.			

*/
 */ WING RIBS
 */

SPAR	M5	N6001	227	229	.25	4.	TO	N6035	261	263	+
							BY	N2	2	2	
*2		N6109	435	437	.30	4.	TO	N6135	461	463	+
							BY	N2	2	2	
*2		N6215	641	643	.20	3.	TC	N6235	661	663	+
							BY	N2	2	2	
*2		N6425	1051	1053	.20	4.					
*2		N6426	1053	1054	.20	4.	TO	N6435	1062	1063	
*2		N6629	1456	1457	.12	2.	TO	N6635	1462	1463	
*2		N6833	1860	1861	.30	1.4	TO	N6835	1862	1863	

*/
 */ WING COVERS
 */

COVER	M5	N7003	229	429	227	.06						
*2		N7203	229	429	431	231	.06				TO	+
		N8603	243	443	445	245		BY	N200	2	*=3	
*2		N8803	245	445	447	247	.12	.00			TO	+
		N9603	253	453	455	255		BY	N200	2	*=3	
*2		N5803	255	455	457	257	.10	.14				
*2		N10003	257	457	459	259		**				
*2		N10203	259	459	461	261	.26	.14	.22	.00		
*2		N10403	261	461	463	263		**				
*2		N7805	437	637	435		.06					
*2		N8005	437	637	639	439	.06				TO	+
		N9605	453	653	655	455		BY	N200	2	*=3	
*2		N9805	455	655	657	457	.10	.14				
*2		N10005	457	657	659	459		**				
*2		N10205	459	659	661	461	.26	.14	.22	.00		
*2		N10405	461	661	663	463		**				
*2		N8407	643	843	641		.06					
*2		N8607	643	843	845	645	.06				TO	+
		N9607	653	853	855	655		BY	N200	2	*=3	
*2		N9807	655	855	857	657	.10	.08				
*2		N10007	657	857	859	659		**				
*2		N10207	659	859	861	661	.30	.14	.20	.00		
*2		N10407	661	861	863	663		**				
*2		N9609	849	1049	847		.06					
*2		N9809	849	1049	1051	851	.06				TO	+
		N9609	853	1053	1055	855		BY	N200	2	*=3	
*2		N9809	855	1055	1057	857	.10	.08				
*2		N10009	857	1057	1059	859		**				
*2		N10209	859	1059	1061	861	.30	.14	.20	.00		
*2		N10409	861	1061	1063	863		**				
*2		N9611	1053	1253	1051		.30	.14	.22	.12		
*2		N9611	1053	1253	1254	1054	.30	.14	.22	.12	TO	+
		N10511	1052	1262	1263	1063		BY	N100	1	*=3	
*2		N9713	1255	1455	1254		.30	.14	.22	.12		
*2		N9813	1255	1455	1456	1256	.30	.14	.22	.12	TO	+
		N10513	1262	1462	1463	1263		BY	N100	1	*=3	
*2		N9915	1457	1657	1456		.08					
*2		N10015	1457	1657	1658	1458	.08				TO	+
		N10515	1462	1662	1663	1463		BY	N100	1	*=3	
*2		N10117	1659	1859	1658		.08					
*2		N10217	1659	1859	1860	1660	.08				TO	+
		N10517	1662	1862	1863	1663		BY	N100	1	*=3	

*/
 */ WING IN-BODY COVERS
 */

COVER	M5	N7001	27	227	229	29	.30					
		N8601	43	243	245	45		BY	N200	2	*=3	
*2		N8801	45	245	247	47	.60				TO	+
		N9601	53	253	255	55		BY	N200	2	*=3	
*2		N9801	55	255	257	57	.70					
*2		N10001	57	257	259	59	.70					
*2		N10201	59	259	261	61	1.30	.70	1.10	.00		
*2		N10401	61	261	263	63		**				

*/

*/ WING FIN SPARS

*/
 SPAR M5 N11001 2056 2256 P1
 *2 N11003 2256 2456 *
 *2 N11201 2058 2258 *
 *2 N11203 2258 2458 *
 *2 N11501 2061 2261 *
 *2 N11503 2261 2461 *
 *2 N11701 2063 2263 *
 *2 N11703 2263 2463 *

*/ WING FIN RIBS

*/
 SPAR M5 N12001 2256 2258 P1
 *2 N12003 2258 2261 *
 *2 N12005 2261 2263 *
 *2 N12201 2456 2458 *
 *2 N12203 2458 2461 *
 *2 N12205 2461 2463 *

*/ WING FIN COVERS

*/
 COVER M5 N13001 2056 2256 2258 2058 .05
 *2 N13003 2058 2258 2261 2061 *
 *2 N13005 2061 2261 2263 2063 *
 *2 N13201 2256 2456 2458 2258 *
 *2 N13203 2258 2458 2461 2261 *
 *2 N13205 2261 2461 2463 2263 *

*/ WING FIN ATTACHMENT BEAMS

*/
 BEAM M5 N20001 1456 2056 1463 P2
 *2 N20003 1458 2058 1463 *
 *2 N20005 1461 2061 1463 *
 *2 N20007 1463 2063 1461 *
 *2 N21001 1456 1458 P3
 *2 N21003 1458 1461 *
 *2 N21005 1461 1463 *

*/ WING TRAILING EDGE CONTROL SURFACE RIBS

*/
 SPAR M5 N101 263 3003 P4
 **2 0 0 2 200 100 0
 *2 N102 3003 3005 *
 **2 0 0 2 100 100 0
 *2 N108 1463 3405 *
 **2 0 0 1 200 100 *

*/ WING TRAILING EDGE CONTROL SURFACE COVERS

*/
 COVER M5 N151 263 463 3103 3003 .10
 *2 N153 463 663 3203 3103 *
 *2 N152 3003 3103 3105 3005 *
 *2 N154 3103 3203 3205 3105 *
 *2 N156 1463 1663 3505 3405 *
 **1 0 0 1 200 200 100 100 *

*/ HORIZONTAL TAIL SPARS

*/
 SPAR M5 N14003 279 479 .10 1.2
 *2 N14005 479 679 **
 *2 N14103 281 481 .05 1.8
 *2 N14105 481 681 **
 *2 N14203 283 483 .05 1.6
 *2 N14205 483 683 **
 *2 N14303 285 485 .20 2.6
 *2 N14305 485 685 **

*/

*/ HORIZONTAL TAIL RIBS

```

*/
  SPAR  M5  N14401    279  281    .15   2.0 TO N14405    283  285
                        BY  N2              2    2
    *2    N14501    479  481    .10   1.2 TO N14505    483  485
    *2    N14601    679  681    .10   1.2 TO N14605    683  685
                                           BY  N2              2    2

```

*/ HORIZONTAL TAIL IN-BODY SPARS

```

*/
  SPAR  M5  N14001    79  279    .50   6.0
    *2    N14101    91  281    .25   9.0
    *2    N14201    83  283    .25   8.0
    *2    N14301    85  285    1.00  13.0

```

*/ HORIZONTAL TAIL COVERS

```

*/
  COVER  M5  N15003    279  479  481  281    .16
**+2    0    0      200      2  *3      0.
  COVER  M5  N15005    479  679  681  481    .07
**+2    0    0      200      2  *3      0.

```

*/ HORIZONTAL TAIL IN-BODY COVERS

```

*/
  COVER  M5  N15001    79  279  281    81    .80
                        N15401    83  283  285    85    BY  N200      2    *3

```

*/ BODY BEAMS

```

*/
  BEAM  M5  N1001      1    3    5.    0.  *3  16000.  10.  0.  *3  30000.
**+30  0    0      2      2    2    5.  *4  14000.   5.  *4  14000.
    *2    N1063      63    65  160.  *4  450000.  148.  *4  416000.
**+12  0    0      2      2    2  -12.  *4  -34000. -12.  *4  -34000.

```

*/ BEAMS AT 455 RIB TO PICK UP DISCONTINUED SPARS

```

*/
  BEAM  M5  N30002    1053  1054    P5
**+4    0    0      2      2      *
  BEAM  M5  N30011    1063  1062    P5
**+4    0    0      -2     -2     -2    *

```

END ELEMENT DATA
 END STIFFNESS DATA
 BEGIN MASS DATA
 BEGIN CONDITION DATA
 STAGE 1 CONDITION 1
 END CONDITION DATA
 BEGIN MASS ELEMENT DATA

```

  PLATE F2  B-1    6001  6002  6022    3495.
  PLATE      B-2    6002  6003  6023  6022  5955.
  PLATE      B-3    6003  6004  6024  6023  2589.
  PLATE      B-4    6004  6005  6025  6024  3440.
  PLATE      B-5    6005  6006  6026  6025  5420.
  PLATE      B-6    6006  6007  6027  6026  3280.
  PLATE      B-7    6007  6008  6028  6027  3306.
  PLATE      B-8    6008  6009  6029  6028  4346.
  PLATE      B-9    6009  6010  6030  6029  4507.
  PLATE      B-10   6010  6011  6031  6030  4486.
  PLATE      B-11   6011  6012  6032  6031  3619.
  PLATE      B-12   6012  6013  6033  6032  4730.
  PLATE      B-13   6013  6014  6034  6033  3982.
  PLATE      B-14   6014  6015  6035  6034   947.
  PLATE      B-15   6015  6016  6036  6035  1788.
  PLATE      VT-1   6501  6502  6504  6503   600.
  PLATE      W-1    6100  6101  6121  6120   766.
  PLATE      W-2    6101  6102  6122  6121  1151.
  PLATE      W-3    6102  6103  6123  6122  1667.
  PLATE      W-4    6103  6104  6124  6123  1112.
  PLATE      W-5    6104  6105  6125  6124  1190.
  PLATE      W-6    6105  6106  6126  6125  1659.
  PLATE      W-7    6106  6107  6127  6126  1988.

```

PLATE	W-8	6107	6108	6126	6127	2467.
PLATE	W-9	6108	6109	6129	6128	1335.
PLATE	W-10	6109	6110	6130	6129	339.
PLATE	W-11	6120	6121	6141	6140	795.
PLATE	W-12	6121	6122	6142	6141	1415.
PLATE	W-13	6122	6123	6143	6142	813.
PLATE	W-14	6123	6124	6144	6143	1259.
PLATE	W-15	6124	6125	6145	6144	1249.
PLATE	W-16	6125	6126	6146	6145	1720.
PLATE	W-17	6126	6127	6147	6146	1494.
PLATE	W-18	6127	6128	6148	6147	1888.
PLATE	W-19	6128	6129	6149	6148	498.
PLATE	W-20	6129	6130	6150	6149	126.
PLATE	W-21	6140	6141	6161	6160	508.
PLATE	W-22	6141	6142	6162	6161	1279.
PLATE	W-23	6142	6143	6163	6162	536.
PLATE	W-24	6143	6144	6164	6163	532.
PLATE	W-25	6144	6145	6165	6164	559.
PLATE	W-26	6145	6146	6166	6165	1055.
PLATE	W-27	6146	6147	6167	6166	1405.
PLATE	W-28	6147	6148	6168	6167	1953.
PLATE	W-29	6148	6149	6169	6168	274.
PLATE	W-30	6149	6150	6170	6169	172.
PLATE	W-31	6180	6181	6201	6200	614.
PLATE	W-32	6181	6182	6202	6201	1286.
PLATE	W-33	6182	6183	6203	6202	562.
PLATE	W-34	6183	6184	6204	6203	786.
PLATE	W-35	6184	6185	6205	6204	1386.
PLATE	W-36	6185	6186	6206	6205	1849.
PLATE	W-37	6186	6187	6207	6206	1649.
PLATE	W-38	6187	6188	6208	6207	421.
PLATE	W-39	6188	6189	6209	6208	255.
PLATE	W-40	6200	6201	6221	6220	207.
PLATE	W-41	6201	6202	6222	6221	497.
PLATE	W-42	6202	6203	6223	6222	692.
PLATE	W-43	6203	6204	6224	6223	765.
PLATE	W-44	6204	6205	6225	6224	816.
PLATE	W-45	6205	6206	6226	6225	843.
PLATE	W-46	6206	6207	6227	6226	687.
PLATE	W-47	6207	6208	6228	6227	136.
PLATE	W-48	6208	6209	6229	6228	94.
PLATE	W-49	6220	6221	6241	6240	136.
PLATE	W-50	6221	6222	6242	6241	522.
PLATE	W-51	6222	6223	6243	6242	516.
PLATE	W-52	6223	6224	6244	6243	536.
PLATE	W-53	6224	6225	6245	6244	555.
PLATE	W-54	6225	6226	6246	6245	580.
PLATE	W-55	6226	6227	6247	6246	704.
PLATE	W-56	6227	6228	6248	6247	119.
PLATE	W-57	6228	6229	6249	6248	91.
PLATE	W-58	6260	6261	6281	6280	289.
PLATE	W-59	6261	6262	6282	6281	306.
PLATE	W-60	6262	6263	6283	6282	244.
PLATE	W-61	6263	6264	6284	6283	507.
PLATE	W-62	6264	6265	6285	6284	116.
PLATE	W-63	6265	6266	6286	6285	76.
PLATE	W-64	6280	6281	6301	6300	216.
PLATE	W-65	6281	6282	6302	6301	144.
PLATE	W-66	6282	6283	6303	6302	245.
PLATE	W-67	6283	6284	6304	6303	365.
PLATE	W-68	6284	6285	6305	6304	86.
PLATE	W-69	6285	6286	6306	6305	71.
PLATE	W-70	6300	6301	6321	6320	184.
PLATE	W-71	6301	6302	6322	6321	160.
PLATE	W-72	6302	6303	6323	6322	126.
PLATE	W-73	6303	6304	6324	6323	273.
PLATE	W-74	6304	6305	6325	6324	66.
PLATE	W-75	6305	6306	6326	6325	66.
PLATE	HT-1	6400	6401	6411	6410	283.
PLATE	HT-2	6401	6402	6412	6411	212.

PLATE	HT-3	6402	6403	6413	6412	522.
PLATE	WF-1	6601	6602	6605	6604	500.
PLATE	WF-2	6602	6603	6606	6605	400.

*/ PLATES REPRESENTING FUEL

PLATE F2	F-1	6102	6103	6123	6122	129.6
PLATE	F-2	6103	6104	6124	6123	8637.2
PLATE	F-3	6104	6105	6125	6124	12852.9
PLATE	F-4	6106	6107	6127	6126	5531.1
PLATE	F-5	6107	6108	6128	6127	6919.3
PLATE	F-6	6108	6109	6129	6128	107.1
PLATE	F-7	6124	6125	6145	6144	442.8
PLATE	F-8	6125	6126	6146	6145	5450.7
PLATE	F-9	6126	6127	6147	6146	6537.8
PLATE	F-10	6128	6129	6149	6148	2604.5
PLATE	F-11	6129	6130	6150	6149	4011.2
PLATE	F-12	6140	6141	6161	6160	5762.0
PLATE	F-13	6144	6145	6165	6164	1128.9
PLATE	F-14	6145	6146	6166	6165	2470.2
PLATE	F-15	6147	6148	6168	6167	1825.8
PLATE	F-16	6148	6149	6169	6168	4994.1
PLATE	F-17	6149	6150	6170	6169	2341.4
PLATE	F-18	6180	6181	6201	6200	3598.6
PLATE	F-19	6184	6185	6205	6204	268.5
PLATE	F-20	6185	6186	6206	6205	1691.6
PLATE	F-21	6186	6187	6207	6206	3248.9
PLATE	F-22	6187	6188	6208	6207	2531.0
PLATE	F-23	6188	6189	6209	6208	4235.0
PLATE	F-24	6200	6201	6221	6220	775.4
PLATE	F-25	6204	6205	6225	6224	457.0
PLATE	F-26	6205	6206	6226	6225	1190.8
PLATE	F-27	6206	6207	6227	6226	1393.2
PLATE	F-28	6207	6208	6228	6227	1501.2
PLATE	F-29	6208	6209	622	6228	1555.2
PLATE	F-30	6220	6221	6241	6240	140.4
PLATE	F-31	6224	6225	6245	6244	54.0
PLATE	F-32	6225	6226	6246	6245	442.8
PLATE	F-33	6226	6227	6247	6246	658.8
PLATE	F-34	6227	6228	6248	6247	646.0
PLATE	F-35	6228	6229	6249	6248	583.2

*/ PLATES REPRESENTING PAYLOAD

PLATE F2	P-1	6002	6003	6023	6022	680.
PLATE	P-2	6003	6004	6024	6023	2295.
PLATE	P-3	6004	6005	6025	6024	3585.
PLATE	P-4	6005	6006	6026	6025	2200.
PLATE	P-5	6006	6007	6027	6026	3390.
PLATE	P-6	6007	6008	6028	6027	3475.
PLATE	P-7	6008	6009	6029	6028	2965.
PLATE	P-8	6009	6010	6030	6029	2040.
PLATE	P-9	6010	6011	6031	6030	2125.
PLATE	P-10	6011	6012	6032	6031	2125.
PLATE	P-11	6012	6013	6033	6032	1190.

END MASS ELEMENT DATA
 BEGIN FACTOR DATA
 EXCLUDE STIFFNESS ELEMENTS
 END FACTOR DATA
 END MASS DATA
 BEGIN SUBSET DEFINITION
 SUBSETS OF NODAL SET 1

*/
 */ SUBSETS FOR PLOTS
 */
 N1 = 1 TO 3605 / NODES FOR STIFFNESS MODEL
 N2 = 6001 TO 6606 / NODES FOR MASS MODEL

*/
 */ SUBSETS FOR AERODYNAMICS
 */

N51 = 1 7 13 19 27 45 55 63 67 75 79 83 85 89
 N42 = 227 237 245 255 263 435 441 445 451 455 463 641 649 655 659 663 +
 847 851 855 859 863 1051 1055 1059 1063 1254 1259 1263 1459 +
 1463 1658 1661 1663 1859 1860 1861 1863

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N43 = 279 283 285 479 483 485 679 683 685
 N53 = 83 283 483 683
 N44 = 2058 2061 2261 2458 2461
 N45 = 263 3003 3005 463 3103 3105 663 3203 3205
 N55 = 263 463 663
 N46 = 1463 3405 1663 3505 1863 3605
 N56 = 1463 1663 1863
 N57 = 285 485 685
 N67 = 485
 N81 = 3003 3103 3203
 N82 = 3005 3105 3205
 N83 = 3405 3505 3605
 N91 = 641 649 663
 N99 = N42 U N43
 N63 = 663 863 1063 1263 1463 1863
 N64 = 655 855 1055
 N65 = 435 641 847 1051 1254 1456 1658 1859
 N66 = 659 659 1059 1259 1459
 N61 = 63 263 463 663
 N68 = 55 255 455 655
 N69 = 245 445
 N70 = 227 435
 N62 = N63 U N64 U N65 U N66 U N61 U N68 U N69 U N70
 SUBSETS OF STIFFNESS SET 1
 */
 */ SUBSETS FOR PLOTS
 */
 E1 = ALL
 SUBSETS OF MASS SET 1
 */
 */ SUBSETS FOR PLOTS
 */
 E2 = ALL
 END SUBSET DEFINITION
 BEGIN BC DATA
 STAGE 1 *(FOR VIBRATION/FLUTTER ANALYSIS)
 ORDER RETAIN BY INTERNALID
 SUPPORT ASYM IN SURFACE 2
 SUPPORT TX FOR 89
 RETAIN TZ FOR 1 7 13 19 27 45 55 63 67 73 79 85 89
 RETAIN TZ FOR 227 237 245 255 435 441 445 451 455
 RETAIN TZ FOR 641 645 649 655 659 847 851 855 859 863 1051 1055 1059 1063
 RETAIN TZ FOR 1254 1259 1456 1459 1658 1661 1859 1860 1861
 RETAIN TZ FOR 3003 3005 3103 3105 3203 3205
 RETAIN TZ FOR 3305 3405 3505 3605
 RETAIN TZ FOR 279 479 679
 RETAIN TY FOR 2058 2061 2258 2261 2458 2461
 RETAIN TZ PX RY FOR 263 463 663 1263 1463 1663 1863 285 485 685 83 +
 283 483 683
 END BC DATA
 END PROBLEM DATA

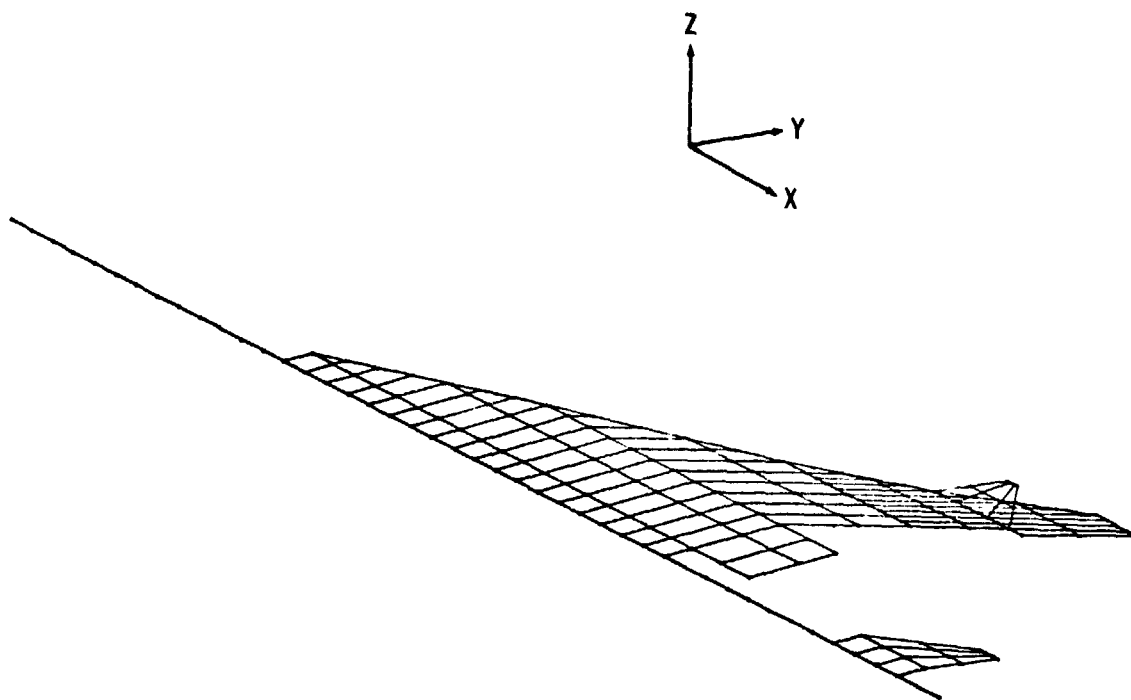


Figure 211-1. Structural Model for Flutter Demonstration

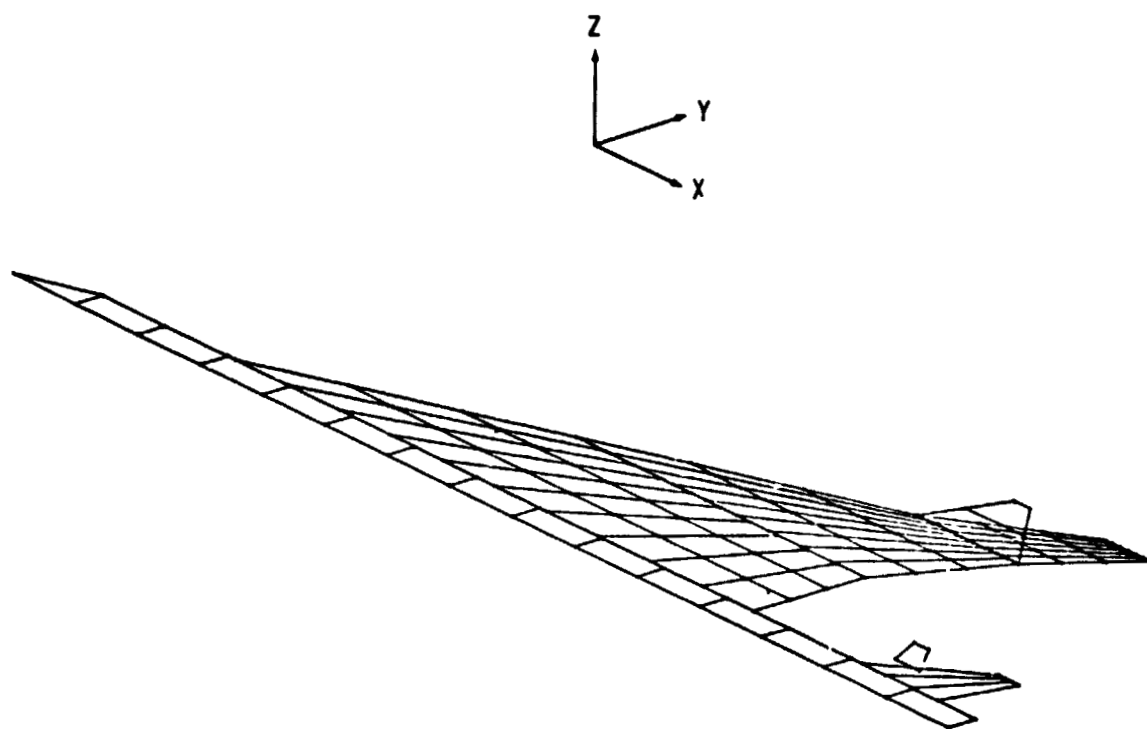


Figure 211-2. Mass Model for Flutter Demonstration

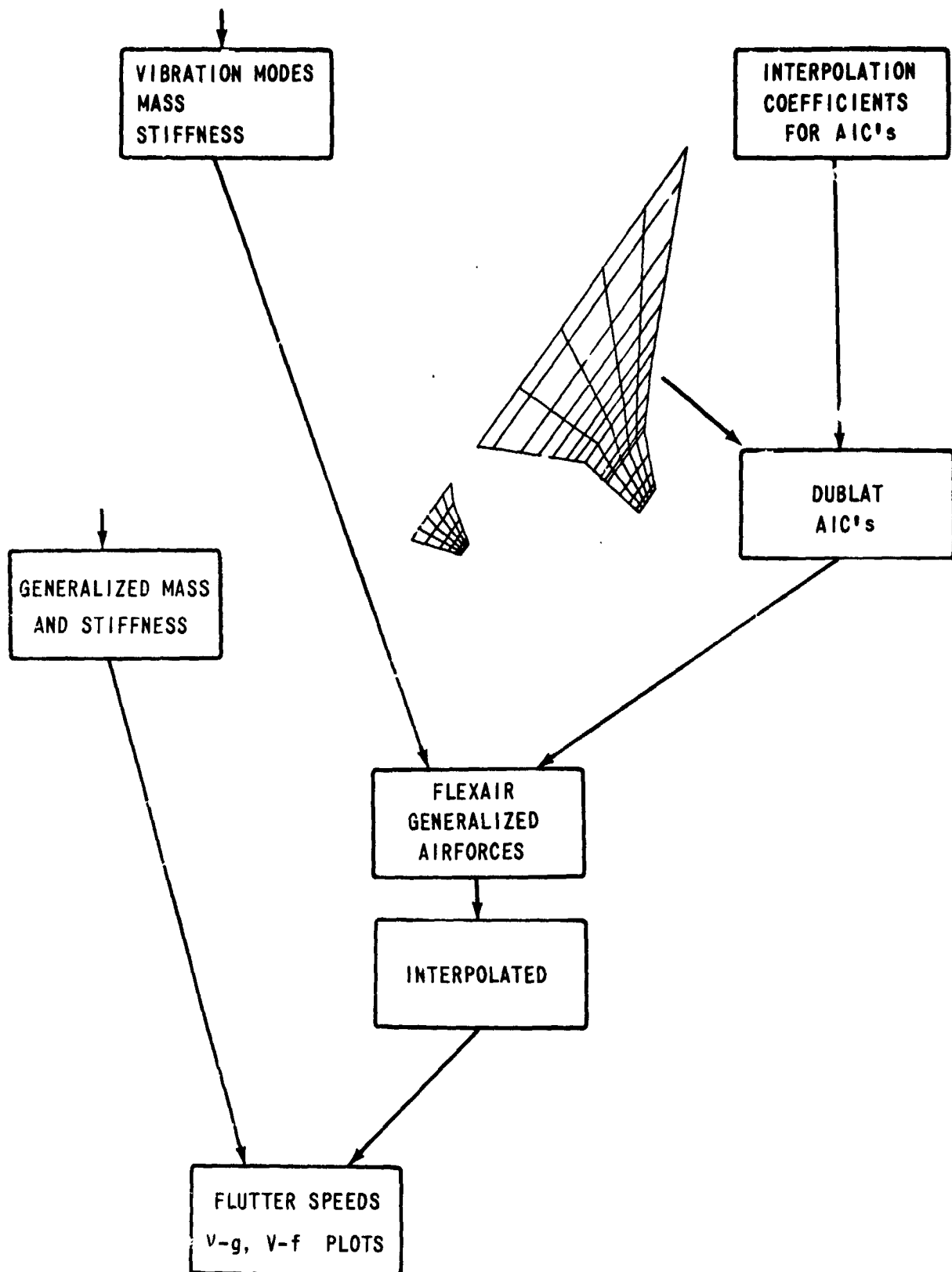


Figure 211-3. First Flutter Analysis, Mach = 0.8 Using Aerodynamic Influence Coefficients

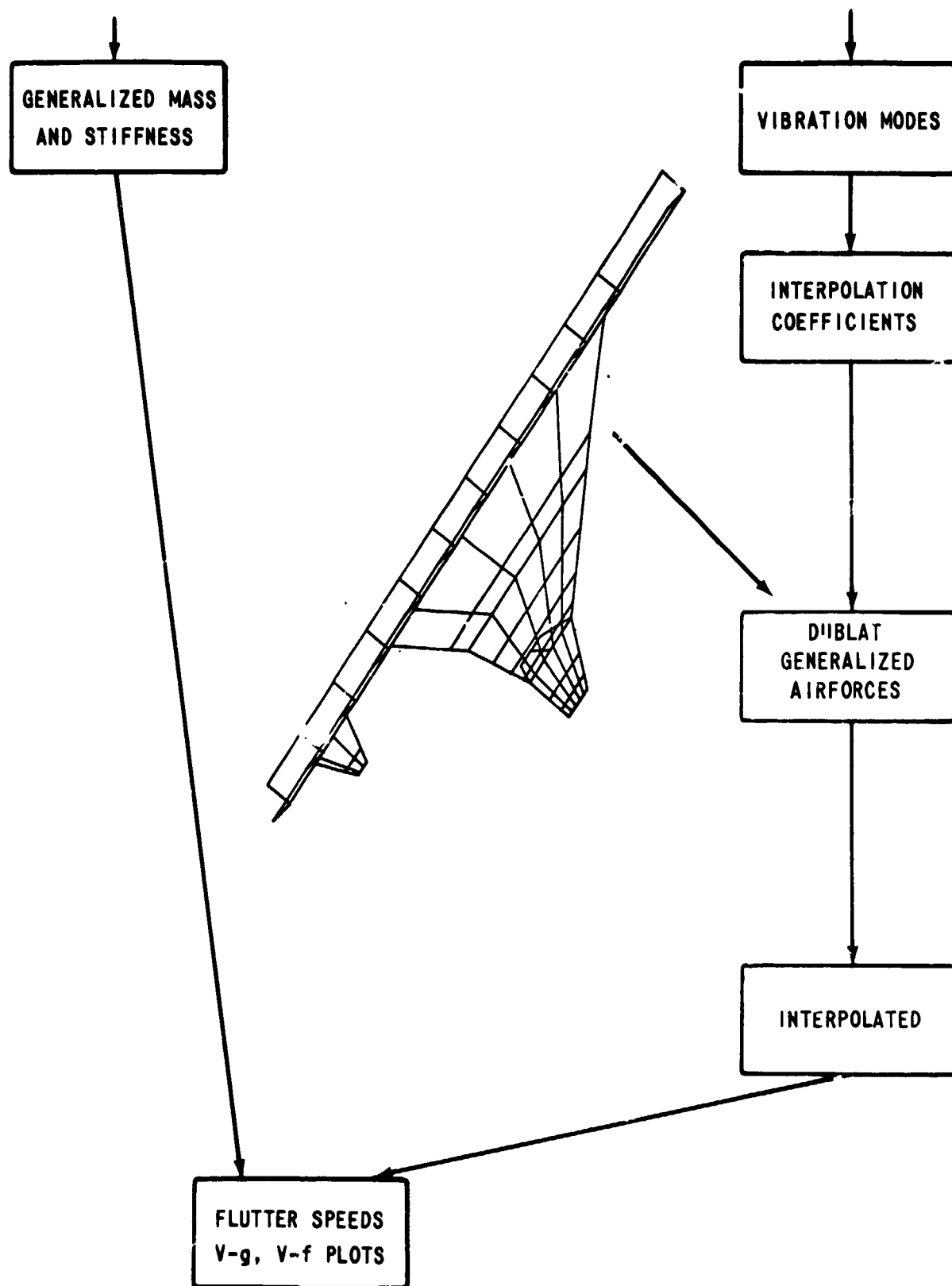


Figure 211-4. Second Flutter Analysis, Mach=0.8

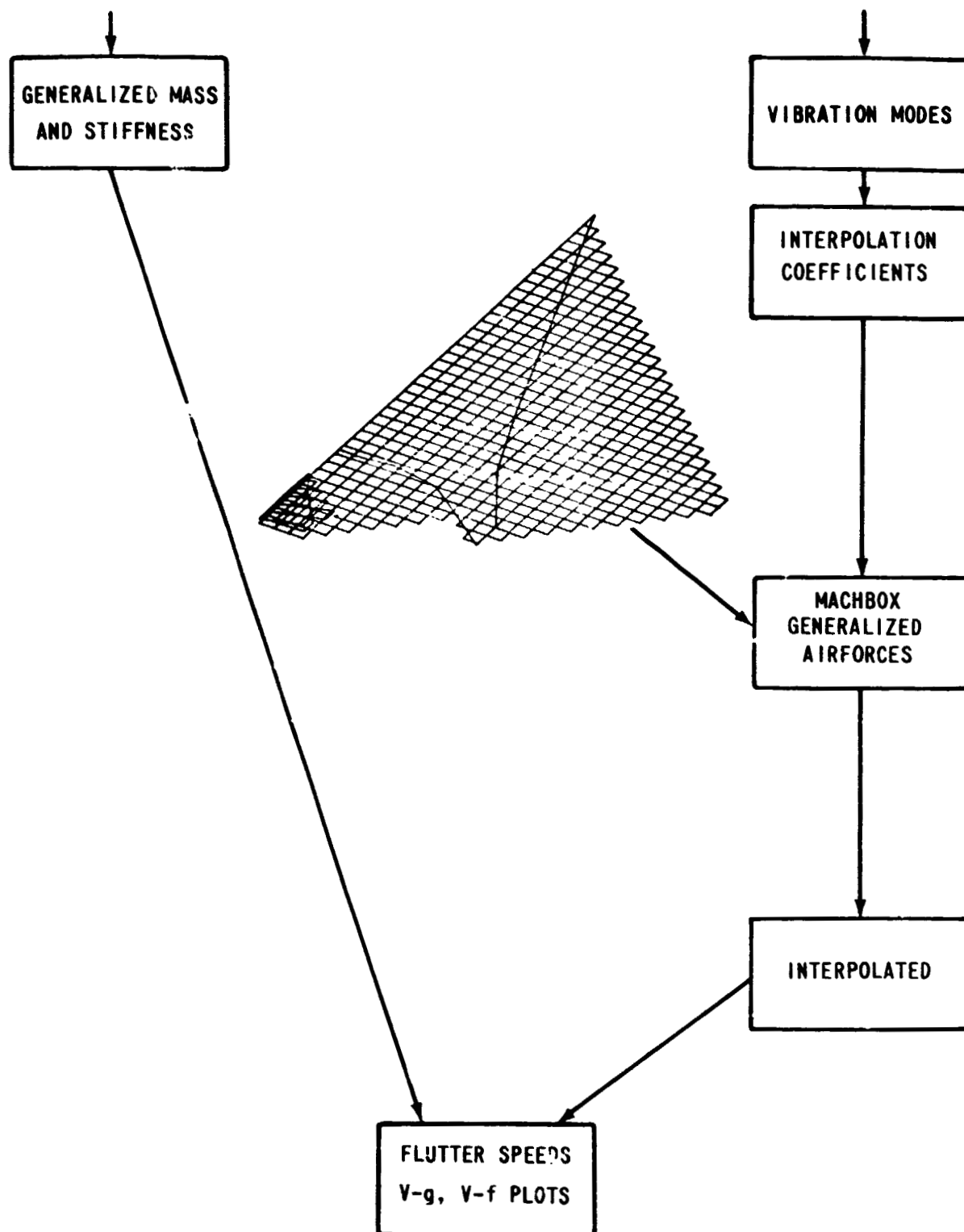


Figure 211-5. Third Flutter Analysis, Mach = 1.526

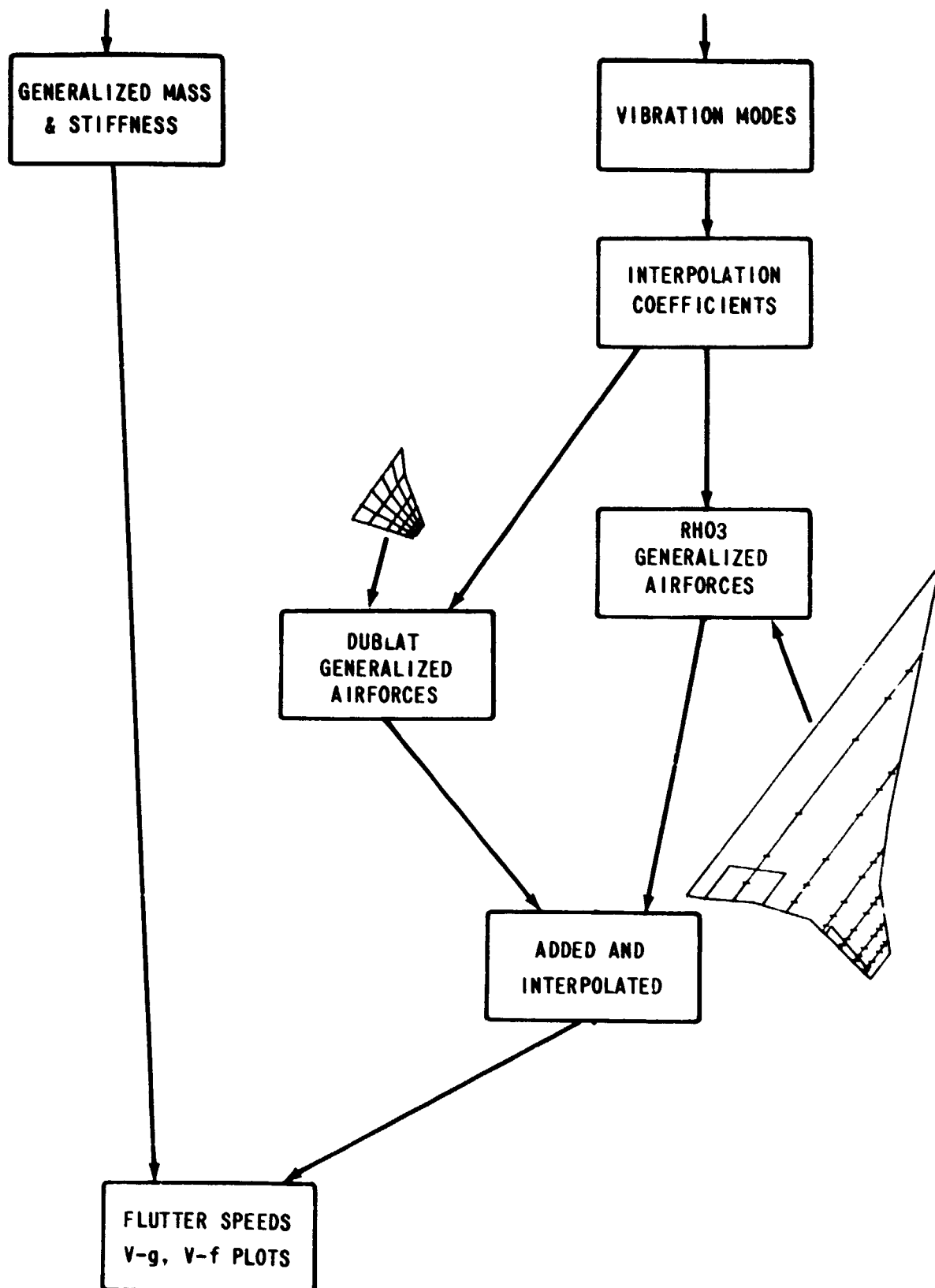


Figure 211-6. Fourth Flutter Analysis, Mach= 0.8

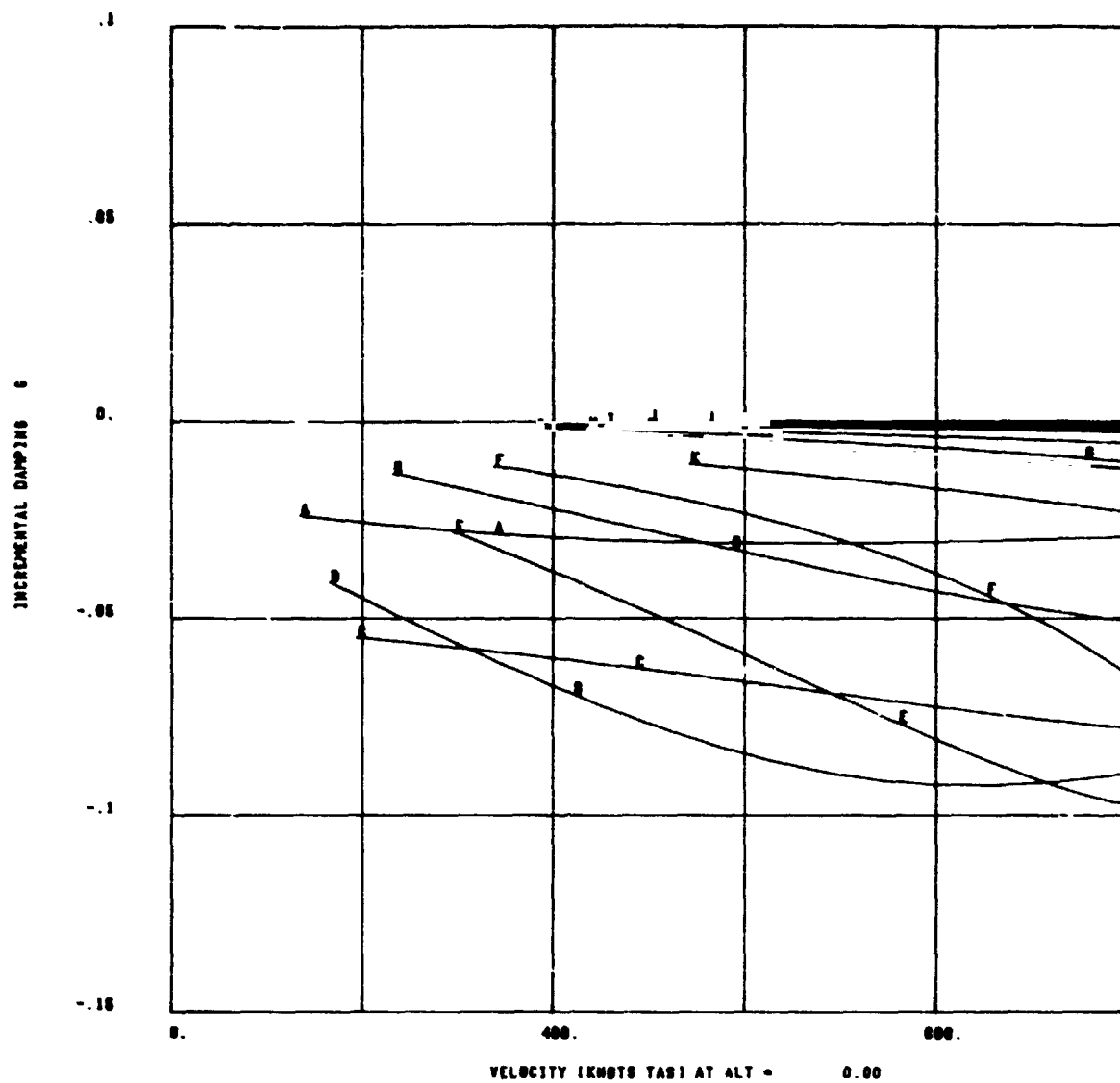


Figure 211-7. V-g Plot, First Flutter Analysis Including Residual Flexibility Effects

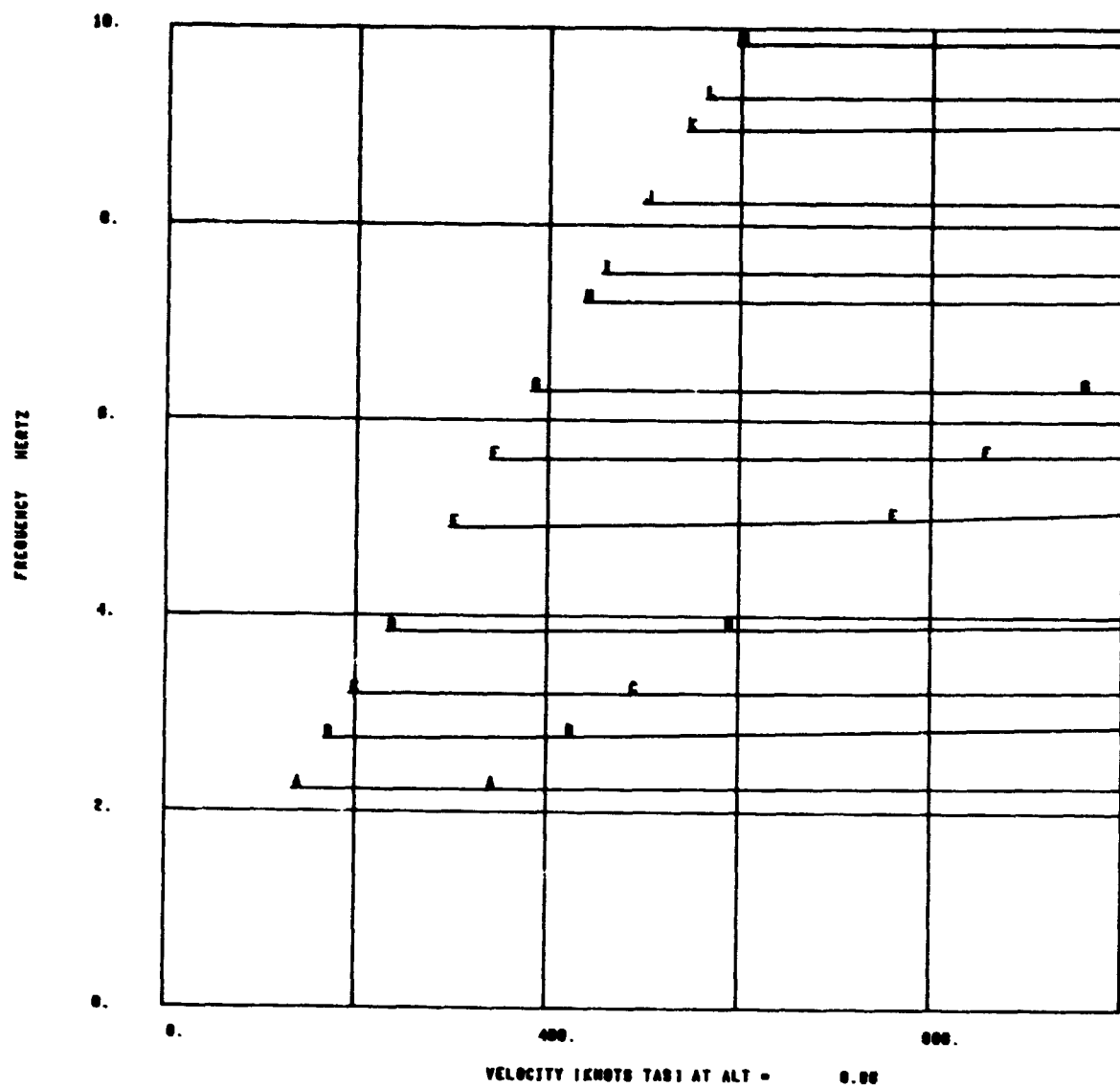


Figure 211-8. V-f Plot, First Flutter Analysis Including Flexibility Effects

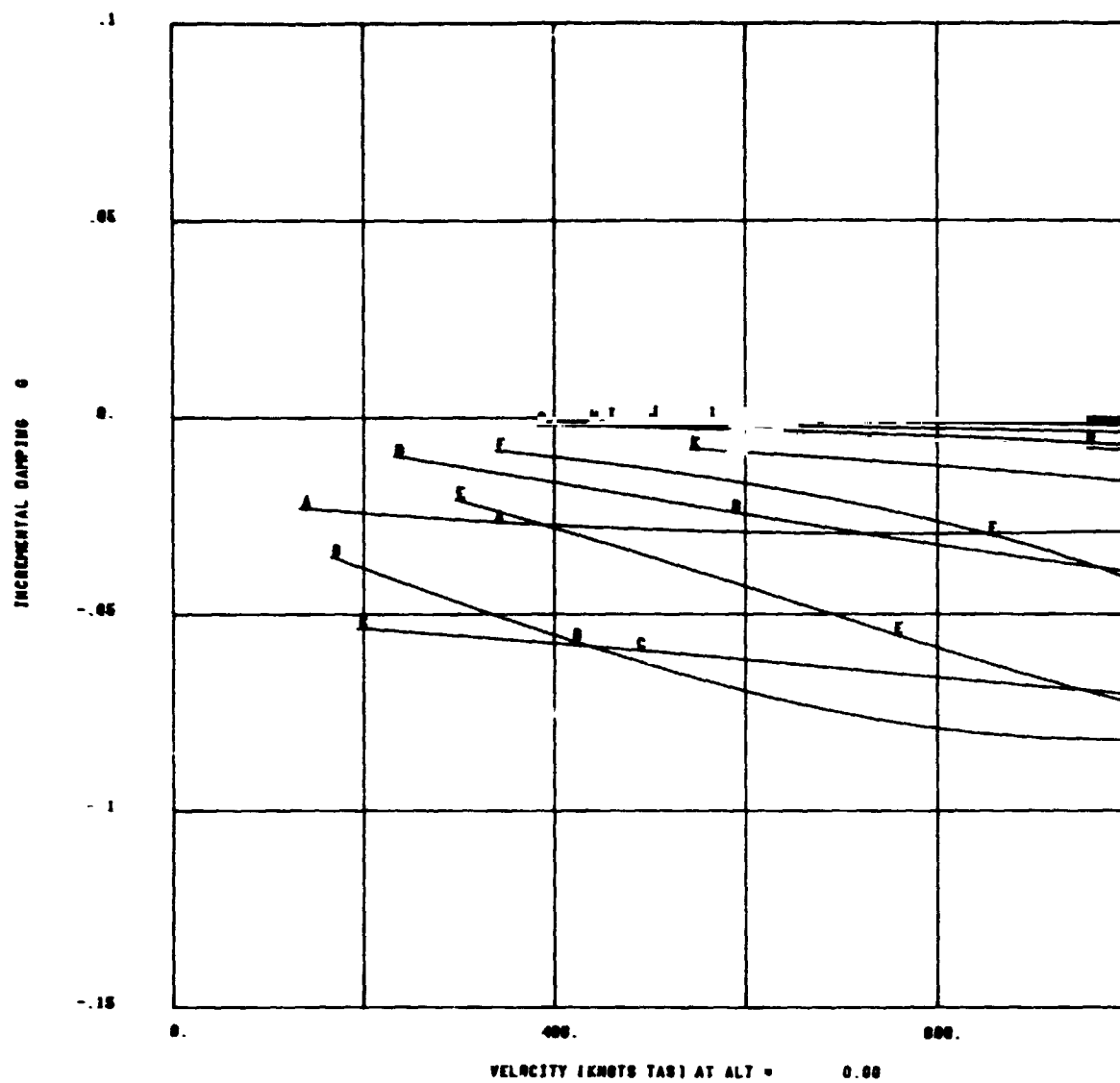


Figure 211-9. V-g Plot, First Flutter Analysis Without Residual Flexibility Effects

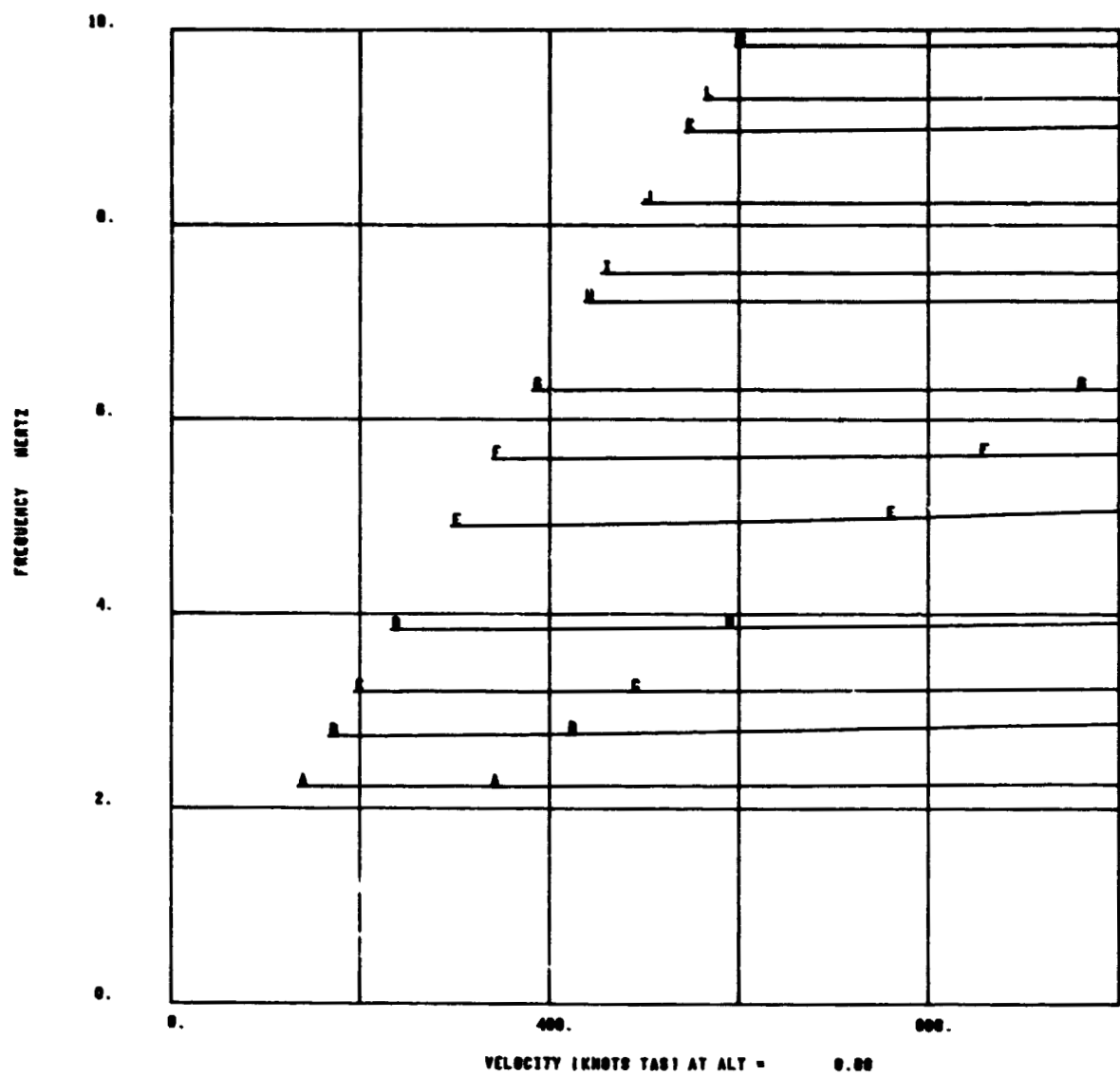


Figure 211-10. V-f Plot, First Flutter Analysis Without Residual Flexibility Effects

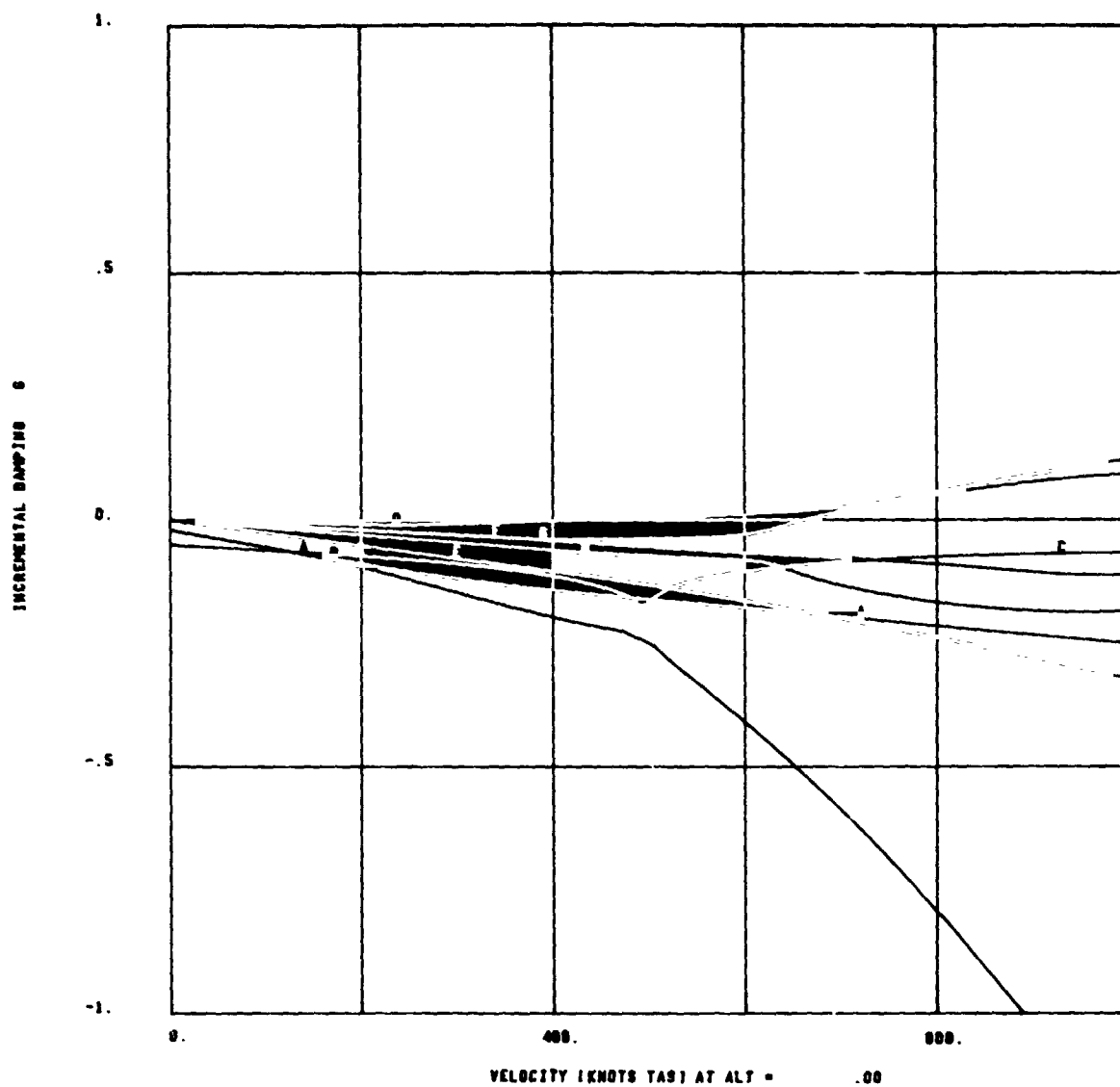


Figure 211-11. V-g Plot, Second Flutter Analysis

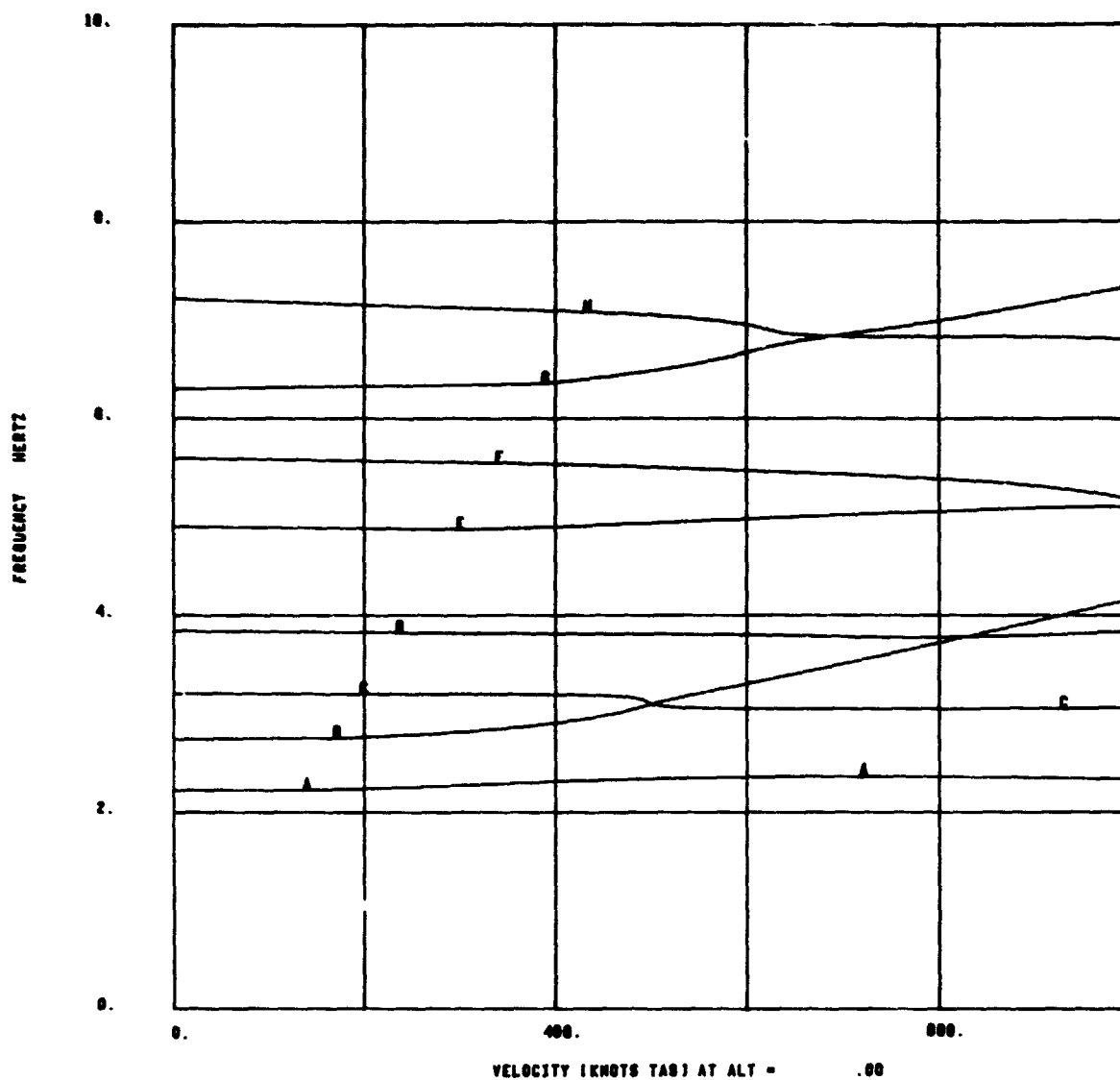


Figure 211-12. V-f Plot Second Flutter Analysis

212. FLUTTER ANALYSIS OF A T-TAIL AIRCRAFT (DECK 14)

212.1 DESCRIPTION OF ANALYSIS

This problem demonstrates the subsonic flutter analysis of the empennage of a T-tail aircraft, the YC-14. The structural model, shown in figure 212-1, is comprised of BEAM and ROD elements. All mass is defined as concentrated masses and a nondiagonal mass matrix is produced directly by the Mass Processor. The X-Y plane is defined as a plane of anti-symmetry and the empennage is cantilevered from the forward end. The model is described in more detail in reference 212-1.

Doublet Lattice aerodynamics, modified to match experimentally obtained steady state aerodynamic derivatives, are used. The aerodynamic modelling is shown in figure 212-2.

212.2 RESULTS

The five lowest natural frequencies obtained in this problem are compared with experimental values from reference 212-1 in table 212-1. Flutter analysis results are presented in the form of V-g and V-f graphs in figures 212-3 and 212-4. The experimental flutter speed is 123 knots.

C
C
C
C
C
C
C
C
C
C

X
X

```

BEGIN MATERIAL DATA /
M51 0.0 /
70 10.4E6 .30 4.0E6 0.0 /
*/ BODY AND FIN SPAR MATERIAL PROPERTIES /
M60 0.0 /
70 5.2E6 .3 2.0E6 0.0 / .5 STIFFNESS FOR BODY-FIN
*/ STABILIZER SPAR STIFFNESS /
M70 0.0 /
70 10.4E6 .3 4.0E6 0.0 /
END MATERIAL DATA /
BEGIN NODAL DATA /
*/ MID BODY SPAR NODES /
REC BODYSM 49.0 0.0 12.112 100. 0.0 12.112 49.0 0.0 20. /
50 0.0 0.0 0.0 /
501 0.0 1.0 0.0 / ROOT NODE PITCH
502 1.0 0.0 0.0 / ROOT NODE ROLL
503 0.0 0.0 1.0 / ROOT NODE YAW
51 2.24 0.0 0.0 /
52 4.48 0.0 0.0 /
53 6.72 0.0 0.0 /
54 8.96 0.0 0.0 /
55 9.80 0.0 0.0 /
56 11.20 0.0 0.0 /
57 12.88 0.0 0.0 /
58 14.56 0.0 0.0 /
801 0.0 0.0 -1.0 /
811 11.20 0.0 -1.0 /
*/ AFT BODY SPAR NODES /
REC BODYSA 49.26225 0.0 9.360988 63.56 0.0 12.112 49.0 0.0 12.112 /
59 16.77 0.0 0.0 /
60 19.98 0.0 0.0 /
61 21.189 0.0 0.0 /
62 21.399 0.0 0.0 /
63 25.409 0.0 0.0 /
64 27.427 0.0 0.0 /
65 29.444 0.0 0.0 /
66 31.454 0.0 0.0 /
67 33.236 0.0 0.0 /
68 35.018 0.0 0.0 /
69 36.808 0.0 0.0 /
70 38.583 0.0 0.0 /
71 40.40 0.0 0.0 /
72 42.25 0.0 0.0 /
73 40.40 0.0 1.36 / BASE OF FIN SPAR MOUNT
74 41.40 0.0 1.36 /
75 42.25 0.0 1.36 /
77 45.50 0.0 0.0 /
771 45.50 -3.5 0.0 /
772 45.50 3.5 0.0 /
78 48.55 0.0 -0.6 /
821 23.399 0.0 -1.0 /
831 31.454 0.0 -1.0 /
841 38.583 0.0 -1.0 /
*/ FIN SPAR NODES /
REC FINSPL 91.33 0.0 21.905 97.48 0.0 35.094 85. 0.0 35. /
76 0.0 0.0 0.0 /
101 0.0 0.0 0.0 /
102 1.087 0.0 0.0 /
103 1.782 0.0 0.0 /
104 2.863 0.0 0.0 /
105 3.740 0.0 0.0 /
106 5.18 0.0 0.0 /
107 6.45 0.0 0.0 /
108 7.497 0.0 0.0 /
109 8.27 0.0 0.0 /
110 9.14 0.0 0.0 /
111 10.587 0.0 0.0 /
112 11.44 0.0 0.0 /
113 12.904 0.0 0.0 /
114 13.676 0.0 0.0 /
115 14.552 0.0 0.0 /

```

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REC FINSPU 87.88069 0.0 24.15718 97.4798 0. 35.0936 85. 0. 35. /
 116 15.824 0.0 0.0 /
 117 16.574 0.0 0.0 /
 118 17.331 0.0 0.0 /
 119 18.152 0.0 0.0 /
 120 19.084 0.0 0.0 /
 121 19.475 0.0 0.0 /
 122 17.454 0.0 1.34 / LOWER PIVOT FOR STABILIZER LEAD SCREW
 1221 17.40 0.0 0.0 / STAB PITCH MECH ATT. TO FIN SPAR.
 123 19.475 1.0 0.0 /
 124 19.475 -1.0 0.0 /
 */ STABILIZER PIVOT MECHANISM /
 RESUME GLOBAL /
 125 101.858 1.0 40.082 /
 126 101.858 -1.0 40.082 /
 127 101.858 .675 40.082 /
 128 101.858 -.675 40.082 /
 129 100.758 .675 40.082 /
 130 100.758 -.675 40.082 /
 131 100.758 0.0 40.082 /
 131 101.108 0.0 40.082 / STABILIZER ROLL-YAW-PITCH MECHANISM
 132 100.358 0.0 40.082 /
 133 99.108 0.0 40.082 /
 134 98.388 0.0 40.082 /
 135 102.608 0.0 40.082 /
 136 102.608 0.0 41.249 /
 360 101.858 .675 41.082 /
 361 101.858 -.675 41.082 /
 362 102.858 .675 40.082 /
 363 102.858 -.675 40.082 /
 364 101.858 .675 40.082 /
 365 101.858 -.675 40.082 /
 */ FUSELAGE SHELL CGS /
 80 54.67 0.0 12.06 / SECT 6
 81 65.95 0.0 12.81 / SECT 7
 82 76.04 0.0 15.02 / SECT 8
 83 83.72 0.0 16.50 / SECT 9
 84 96.09 0.0 18.29 / SECT 10-11
 */ SPAR CG /
 85 54.44 0.0 12.11 / SPAR SECT 6
 86 65.49 0.0 12.49 / SPAR SECT 7
 87 75.97 0.0 14.50 / SPAR SECT 8
 88 83.58 0.0 15.56 / SPAR SECT 9
 89 89.00 0.0 17.08 / SPAR SECT 10-11
 */ OTHER ITEMS /
 79 98.16 0.0 17.94 / TRIM MOTOR
 90 50.79 0.0 9.45 / SECT 6 BASIC WT
 91 68.85 0.0 10.33 / SECT 76 BASIC WT
 92 90.17 0.0 19.55 / 1270-50 BODY-FIN CONNECTION
 */ FIN SECTION CG LOCATIONS /
 203 91.86 0.0 23.21 /
 207 96.09 0.0 26.78 /
 212 98.56 0.0 31.77 /
 218 100.44 0.0 37.21 /
 221 103.89 0.0 40.31 /
 500 130. 0.0 30. / ORIENTATION NODE
 */ HORIZONTAL STABILIZER NODES /
 REC STAB 101.858 0.0 41.249 201.858 0.0 41.249 101.858 6.993 141.2449 / 4ANH
 RESUME GLOBAL /
 150 101.858 0.0 41.249 / STAB SPAR ROOT
 REC HTAIL 101.858 0.0 41.249 201.858 -4.76975 41.249 101.858 6.993
 141.249 / 4DEG ANHEDRIAL
 ANALYSIS FRAME STAB /
 1501 0.0 .2 0.0 /
 151 0.0 1.261 0.0 /
 152 0.0 2.698 0.0 /
 153 0.0 4.135 0.0 /
 154 0.0 5.571 0.0 /
 155 0.0 7.008 0.0 /
 156 0.0 8.059 0.0 /


```

157 0.0 9.075 0.0 /
158 0.0 10.162 0.0 /
159 0.0 11.072 0.0 /
160 0.0 11.914 0.0 /
161 0.0 13.105 0.0 /
162 0.0 14.016 0.0 /
163 0.0 15.137 0.0 /
164 0.0 16.118 0.0 /
165 0.0 17.169 0.0 /
166 0.0 18.221 0.0 /
167 0.0 19.202 0.0 /
168 0.0 20.323 0.0 /
169 0.0 21.144 0.0 /
170 0.0 22.425 0.0 /
171 10.0 15.0 0.0 / ORIENTATION NODE
*/ STABILIZER PANEL-SPAR CG NODES /
REC STABCG 0.0 0.0 41.249 100. 0.0 41.249 0.0 6.993 141.249 /
252 103.6300 2.6400 0.0 /
254 103.4850 5.5350 0.0 /
257 103.887 8.761 0.0 /
261 104.1900 12.7600 0.0 /
265 104.2100 16.9200 0.0 /
269 103.9850 21.8400 0.0 /
RESUME GLOBAL /
ANALYSIS FRAME GLOBAL /
250 101.71 0.0 40.63 /
REC M1 91.33 0.0 21.905 97.48 0.0 35.094 85.0 0.0 35.0 /
9999 0. 0. 0. /
RESUME GLOBAL /
END NODAL DATA /
BEGIN STIFFNESS DATA /
BEGIN PROPERTY DATA /
P1 1.0 **2 20.0 1.0 1.0 / RIGID ELEMENT PROPERTY
P2 .013 **2 20.0 .132E-4 **1 111100. / FWD RIGID SHELL LINKS
P3 1.0 **2 20. 1. 1. 100. / AFT ATTACHMENT OF BODY SHELLS
END PROPERTY DATA /
BEGIN ELEMENT DATA /
*/ ELEMENTS FOR MID BODY SPAR /
BEAM Z60 N50 50 51 2.6269 **2 .815796 .695927 .568320
2.6491 **2 .816595 .705220 .599445 /
*2 N501 50 501 20. **2 7.0 500. 500. 110. / PITCH SPRING-ROOT
*2 N502 50 502 20. **2 2.385 500. 500. 110. / ROLL SPRING ROOT
*2 N503 50 503 58 20. **2 6.45 500. 500. 110. / YAW SPRING ROOT
*2 N51 51 52 2.6491 **2 .816595 .705220 .599445
2.6551 **2 .817135 .699525 .613247 /
*2 N52 52 53 2.6551 **2 .817135 .699525 .613247
2.6330 **2 .809515 .684153 .576283 /
*2 N53 53 54 2.6330 **2 .809515 .684153 .576283
2.5034 **2 .737986 .655574 .500569 /
*2 N54 54 55 2.5034 **2 .737986 .655574 .500569
2.3667 **2 .630967 .647414 .447574 /
*2 N55 55 56 2.3667 **2 .630967 .647414 .447574
2.0209 **2 .390787 .621922 .356925 /
*2 N56 56 57 1.2524 **2 .453769 .621646 .356187
1.1928 **2 .420834 .595791 .325931 /
*2 N57 57 58 1.1928 **2 .420834 .595791 .325931
1.1295 **2 .387686 .566946 .294410 /
*/ NOMINAL AFT BODY SPAR ELEMENTS /
BEAM Z60 N58 58 59 1.3246 **2 .372488 .567341 .294149
1.2313 **2 .331577 .525907 .255716 /
*2 N59 59 60 1.2313 **2 .331577 .525907 .255016
1.1440 **2 .295293 .479277 .224486 /
*2 N60 60 61 1.1440 **2 .295293 .479277 .224486
1.0588 **2 .262771 .432032 .195999 /
*2 N61 61 62 1.0588 **2 .262771 .432032 .195999
.9776 **2 .233375 .389427 .169770 /
*2 N62 62 63 .9776 **2 .233375 .389427 .169770
.9035 **2 .207377 .353343 .147466 /
*2 N63 63 64 .9035 **2 .207377 .353343 .147466
.8390 **2 .184461 .323113 .130984 /

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*2	N64	64 65	.8390	*2	.184401	.323113	.130984
			.7836	*2	.165980	.297177	.117099 /
*2	N65	65 66	.7836	*2	.165980	.297177	.117099
			.7305	*2	.147913	.272751	.106055 /
*2	N66	66 67	.7305	*2	.147913	.272751	.106055
			.6887	*2	.133266	.254542	.098681 /
*2	N67	67 68	.6887	*2	.133266	.254542	.098681
			.6554	*2	.123573	.239385	.091087 /
*2	N68	68 69	.7228	*2	.118307	.239431	.091145
			.6945	*2	.111666	.227279	.085127 /
*2	N69	69 70	.6945	*2	.111666	.227279	.085127
			.6688	*2	.104231	.218352	.080636 /
*2	N70	70 71	.6688	*2	.104231	.218352	.080636
			.4620	*2	.099621	.054947	.077282 /
*2	N71	71 72	.4620	*2	.099621	.054947	.077282
			.455	*2	.098064	.055313	.074358 /
*2		72 77	.0745	*2	.01336	.00668	.00668 /
*2		77 78	.0745	*2	.01336	.00668	.00668 /
*2		77 771	.04925	*2	.00766	.002370	.009413 /
*2		77 772	.04925	*2	.00766	.002370	.009413 /
*/ NOMINAL FIN SPAR ELEMENTS /							
BEAM 260 N101		101 102 500	.2911	*2	.020029	.009823	.038493
			.2909	*2	.020031	.009746	.038400 /
*2	N102	102 103 500	.2729	*2	.017623	.009780	.038224 /
			.2719	*2	.017525	.009681	.037999 /
*2	N103	103 104 500	.4039	*2	.016419	.009918	.038120 /
			.4015	*2	.016248	.009734	.037279 /
*2	N104	104 105 500	.4015	*2	.016248	.009734	.037279
			.3990	*2	.016077	.009651	.036283 /
*2	N105	105 106 500	.3990	*2	.016077	.009651	.036283
			.3943	*2	.015792	.009535	.036248 /
*2	N106	106 107 500	.3943	*2	.015792	.009535	.036248
			.3906	*2	.015567	.009437	.036234 /
*2	N107	107 108 500	.3906	*2	.015567	.009437	.036234
			.3880	*2	.015407	.009355	.036195 /
*2	N108	108 109 500	.3880	*2	.015407	.009355	.036195
			.3865	*2	.015288	.009322	.036125 /
*2	N109	109 110 500	.3865	*2	.015288	.009322	.036125
			.3844	*2	.015125	.009242	.036078 /
*2	N110	110 111 500	.3844	*2	.015125	.009242	.036078
			.3815	*2	.014907	.009145	.036003 /
*2	N111	111 112 500	.3815	*2	.014907	.009145	.036003
			.3781	*2	.014637	.009033	.029247 /
*2	N112	112 113 500	.3781	*2	.014637	.009033	.029247
			.3759	*2	.014479	.008954	.028646 /
*2	N113	113 114 500	.3759	*2	.014479	.008954	.028646
			.3744	*2	.014369	.008922	.028235 /
*2	N114	114 115 500	.3744	*2	.014369	.008922	.028235
			.3723	*2	.014213	.008844	.027715 /
*2	N115	115 116 500	.3723	*2	.014213	.008844	.027715
			.3686	*2	.014029	.008409	.027266 /
*2	N116	116 117 500	.3686	*2	.014029	.008409	.027266
			.3541	*2	.013917	.008112	.018519 /
*2	N117	117 118 500	.3541	*2	.013917	.008112	.018519
			.3466	*2	.013769	.007849	.015641 /
*2	N118	118 1221 500	.3466	*2	.013769	.007849	.015641
			.3466	*2	.013769	.007849	.015641 /
*2	N123	1221 119 500	.3466	*2	.013769	.007849	.015641
			.3062	*2	.011182	.007548	.008782 /
*2	N119	119 120 500	.3062	*2	.011182	.007548	.008782
			.2650	*2	.008361	.003163	.003737 /
*2	N120	120 121 500	.2650	*2	.008361	.003163	.003737 /
*/ ELEMENTS FOR FIN SPAR MOUNT /							
BEAM 260		71 73 500	P1	/			
*2		73 74	P1	/			
*2		74 75	P1	/			
*2		72 75 500	P1	/			
*2		76 101 500	P1	/			
*2		74 76 500	.378	*2	.220340	.139503	.1 / 1210-50

*/ ELEMENTS FOR PITCH-ROLL-YAW MECHANISM /

```

BEAM 260 N123 121 123 P1 /
*2 N124 121 12 P1 /
*2 N125 123 125 .2 *2 .0033470 .0010420 .0106670
      .075 *2 .003000 .001465 .0123800 /
*2 N126 124 126 *12 /
*2 N160 127 360 362 P1 /
*2 N161 128 361 363 P1 /
*2 364 360 362 1.0 *2 .00058 1.0 1.0 10. /
*2 365 361 363 1.0 *2 .00058 1.0 1.0 10. /
*2 N162 127 362 360 P1 /
*2 N164 128 363 361 P1 /
*2 364 362 360 1.0 *2 .00037 1.0 1.0 10. /
*2 365 363 361 1.0 *2 .00037 1.0 1.0 10. /
*2 N127 125 364 1.0 *2 20. 1.0 1.0 111. /
*2 N128 126 365 1.0 *2 20. 1.0 1.0 1000111. /
*2 N129 129 127 .074 *2 .0023775 .000309 .00995
      .049 *2 .001109 .0003395 .0018156 / ROLL CAGE
*2 N130 130 128 *12 /
*2 130 137 P1 /
*2 129 137 P1 /
*2 137 131 P1 /
*2 137 132 P1 /
*2 N132 132 133 .1845 *2 .004577 .002093 .003844 /PITCH SPRING
*2 N133 133 134 1.0 *2 20.0 .125 .125 /
ROD 260 N122 122 134 .01615 / LEAD SC-EW
BEAM 260 131 135 .2547 *2 .006738 .002697 .011277 /-2 SPRING
*2 N136 135 136 500 1.0 *2 20.0 .125 .125 /
*2 N1361 136 150 1.0 *2 20.0 .125 .125 /
*2 N1351 135 150 1.0 *2 20.0 .125 .125 /
*/ MASS ATTACHMENT AFMS /
BEAM 21 N80 56 80 P3 /
*2 N801 80 801 P1 /
*2 801 50 80 P2 /
*2 N81 62 81 P3 /
*2 N811 81 811 P1 /
*2 811 56 81 P2 /
*2 N82 66 82 P3 /
*2 N821 82 821 P1 /
*2 821 62 82 P2 /
*2 N83 70 83 P3 /
*2 N831 83 831 P1 /
*2 831 66 83 P2 /
*2 771 84 P3 /
*2 772 84 P3 /
*2 N841 84 841 P1 /
*2 841 70 84 P2 /
*/ STABILIZER ELEMENT DATA /
BEAM 270 150 1501 171 1.0 *2 20. 1. 1. /
BEAM 270 1501 151 171 1.0 *2 20. 1. 1. .2543 *2 .006348 .003096 .01544 /
*2 N151 151 152 171 .2543 *2 .006348 .003096 .015440
      .2456 *2 .005999 .002715 .013552 /
*2 N152 152 153 171 .2456 *2 .005999 .002715 .013552
      .2445 *2 .005537 .002316 .011436 /
*2 N153 153 154 171 .2445 *2 .005537 .002316 .011436
      .2249 *2 .005132 .001973 .009842 /
*2 N154 154 155 171 .2249 *2 .005132 .001973 .009842
      .2098 *2 .004613 .001631 .008158 /
*2 N155 155 156 171 .2098 *2 .004613 .001631 .008158
      .1887 *2 .003967 .001415 .006221 /
*2 N156 156 157 171 .1887 *2 .003967 .001415 .006221
      .1836 *2 .003253 .001238 .007143 /
*2 N157 157 158 171 .1836 *2 .003253 .001238 .007143
      .1659 *2 .002741 .001092 .005447 /
*2 N158 158 159 171 .1659 *2 .002741 .001092 .005447
      .1570 *2 .002446 .000986 .004986 /
*2 N159 159 160 171 .1570 *2 .002446 .000986 .004986
      .1494 *2 .002200 .000899 .004474 /
*2 N160 160 161 171 .1494 *2 .002200 .000899 .004474
      .1402 *2 .001923 .000797 .003980 /

```

```

*2      N161      161 162 171 .1402 **2 .001923 .000797 .003980
               .1332 **2 .001711 .000738 .003680 /
*2      N162      162 163 171 .1332 **2 .001711 .000738 .003680
               .1266 **2 .001527 .000682 .003389 /
*2      N163      163 164 171 .1266 **2 .001527 .000682 .003389
               .1201 **2 .001352 .000625 .003110 /
*2      N164      164 165 171 .1201 **2 .001352 .000625 .003110
               .1131 **2 .001184 .000558 .002794 /
*2      N165      165 166 171 .1131 **2 .001184 .000558 .002794
               .1071 **2 .001025 .000526 .002619 /
*2      N166      166 167 171 .1071 **2 .001025 .000526 .002619
               .1015 **2 .000903 .000482 .002386 /
*2      N167      167 168 171 .1015 **2 .000903 .000482 .002386
               .0953 **2 .000778 .000430 .002135 /
*2      N168      168 169 171 .0953 **2 .000778 .000430 .002135
               .0906 **2 .000683 .000401 .001985 /
*2      N169      169 170 171 .0906 **2 .000683 .000401 .001985
               .0830 **2 .000546 .000344 .001707 /

```

```

END ELEMENT DATA /
END STIFFNESS DATA /
BEGIN BC DATA /
SUPPORT SYMM IN SURFACE 2 THROUGH 50 /
SUPPORT TX TY TZ RX RY RZ FOR 50 501 502 503 /
FREE RX RY RZ FOR 50 /
RETAIN TY RX RZ FOR 51 53 56 59 60 62 64 66 68 70 71 77 78 /
RETAIN TY RX RZ FOR 80 81 82 93 94 74 /
RETAIN TY RX RZ FOR 103 107 112 118 121 /
RETAIN TX TY TZ RX RY RZ FOR 1501 152 154 157 161 165 169 /
END BC DATA /

```

```

BEGIN MASS DATA /
BEGIN CONDITION DATA /
STAGE 1 CONDITION 1 0 C 1 /
END CONDITION DATA /
BEGIN CONCENTRATED MASS DATA 1 /

```

```

*/ FIN MASS DATA /
FINP1 103 203 I=M1 .1591 .3415 .8430 .6080 /
FINP2 107 207 I=M1 .2029 .9505 5.0475 4.3955 /
FINP3 112 212 I=M1 .2459 .7300 4.8615 4.5360 /
FINP4 118 218 I=M1 .3666 1.0165 5.7665 5.1225 /
FINP5 121 221 I=M1 .2543 1.2115 4.4285 3.6400 /

```

```

*/ BODY MASS DATA /
ABSEC6SH 80 .3125 15.0625 12.5485 14.7025 /
ABSEC7SH 81 .2875 12.5555 11.5425 12.2730 /
ABSEC8SH 82 .1115 3.3330 2.6840 3.0415 /
ABSEC9SH 83 .1570 3.2900 2.8550 3.2485 /
ABSEC10SH 84 .1215 1.3095 8.6950 9.4100 /
ABSEC6SP 53 85 1.4360 .7255 14.7140 14.8205 /
ABSEC7SP 59 86 .8935 .9550 9.6910 9.7735 /
ABSEC8SP 64 87 .3440 .2420 1.9250 1.8990 /
ABSEC9SP 68 88 .2495 .1525 1.0920 1.0865 /
ABSEC10SP 71 89 .1210 .0675 .4190 .4025 /
BASIC6 51 90 1.2965 5.5090 .7155 2.8245 /
BASIC7 60 91 .2840 .4665 .3615 .1490 /
VTATT 74 92 .2000 .8530 .6980 .2750 /
MOTOR 78 79 .1507 .0165 .0935 .0935 /
MOTOR SUP 77 .1068 .23025 .58005 .4973 /
SEC6ATT 56 .0005 .00005 .00005 .00005 /
SEC7ATT 62 .0005 .00005 .00005 .00005 /
SEC8ATT 66 .0005 .00005 .00005 .00005 /
SEC9ATT 70 .0005 .00005 .00005 .00005 /

```

```

*/ STABILIZER MASS DATA /
SPANEL0 1501 250 .29335 .1465 .2634 .23855 /
SPANEL1 152 252 .247 .269222 1.527759 1.716580 /
SPANEL2 154 254 .1858 .173 1.08849 1.169249 /
SPANEL3 157 257 .2419 .398 1.26 1.56522 /
SPANEL4 161 261 .2609 .368475 .821968 1.129243 /
SPANEL5 165 265 .1961 .269449 .526398 .759347 /
SPANEL6 169 269 .1489 .275112 .342002 .574814 /

```

```

END CONCENTRATED MASS DATA /
BEGIN FACTOR DATA /

```

```

EXCLUDE STIFFNESS ELEMENTS /
  END FACTOR DATA /
  END MASS DATA /
BEGIN SUBSET DEFINITION /
SUBSETS OF STIFFNESS SET 1 /
N001 = 59 60 62 64 66 68 70 71 77 / BCOY
N002 = 74 103 107 112 118 121 / FIN
N003 = 1501 152 154 157 161 165 169 / STAR
N004 = ALL / PLOT SET
  EXCLUDE 500 171 FROM N004 /
E004 = ALL / ELEMENT PLOT SET
END SUBSET DEFINITION /
BEGIN DUBLAT DATA /
CASE 1 /
BEGIN GEOMETRY DATA /
LIFTING SURFACE DATA /
PANEL HTAIL 98.155 110.454 101.107 107.257 0.0 23.062 41.249 39.6363 /
CHORD DIV 0. .1 .2 .4 .62 .81 1.0 /
SPAN DIV 0. .1 .2 .3 .4 .5 .6 .7 .8 .9 1.0 /
PANEL TAILF 93.15 114.37 93.15 113.278 0. 0. 43.5 41.249 /
CHORD DIV 0. .1 .2487 .310 .3709 .4931 .6275 .7436 .8597 1.0 /
SPAN DIV 0. .5 1.0 /
PANEL TAILU 93.15 113.278 93.15 112. 0. 0. 41.249 38.5 /
CHORD DIV 0. .1 .2487 .310 .3709 .4931 .6275 .7436 .8597 1.0 /
SPAN DIV 0. .5 1.0 /
PANEL TAILM 93.15 112. 91.55 110.45 0. 0. 38.5 35.094 /
CHORD DIV 0. .1 .2487 .310 .3709 .4931 .6275 .7436 .8597 1.0 /
SPAN DIV 0. .5 1.0 /
PANEL TAILL 91.55 110.45 85.404 104.280 0. 0. 35.094 21.905 /
CHORD DIV 0. .1 .2487 .310 .3709 .4931 .6275 .7436 .8597 1.0 /
SPAN DIV 0. .125 .25 .375 .50 .625 .75 .875 1.0 /
INTERFERENCE SURFACE DATA /
BODY ABODY /
PANEL TOPBD 60.2 111.1 60.2 111.1 0. 1.45 21.905 21.905 /
CHORD DIV 0. .0 .2365 .3919 .4952 .5323 .5874 .6101 .6327 .6780
.7279 .7709 .8140 .8660 1.0 /
SPAN DIV 0. 1.0 /
PANEL USIDE 60.2 111.1 60.2 111.1 1.450 3.5 21.905 19.855 /
CHORD DIV 0. .0 .2365 .3919 .4952 .5323 .5874 .6101 .6327 .6780
.7279 .7709 .8140 .8660 1.0 /
SPAN DIV 0. 1.0 /
PANEL VSIDE 60.2 111.1 60.2 111.1 3.5 3.5 19.855 16.955 /
CHORD DIV 0. .0 .2365 .3919 .4952 .5323 .5874 .6101 .6327 .6780
.7279 .7709 .8140 .8660 1.0 /
SPAN DIV 0. 1.0 /
PANEL LSIDE 60.2 111.1 60.2 111.1 3.5 1.450 16.955 14.905 /
CHORD DIV 0. .0 .2365 .3919 .4952 .5323 .5874 .6101 .6327 .6780
.7279 .7709 .8140 .8660 1.0 /
SPAN DIV 0. 1.0 /
PANEL BOTBD 60.2 111.1 60.2 111.1 1.45 0. 14.905 14.905 /
CHORD DIV 0. .0 .2365 .3919 .4952 .5323 .5874 .6101 .6327 .6780
.7279 .7709 .8140 .8660 1.0 /
SPAN DIV 0. 1.0 /
DOUBLET DATA /
BODY ABODY 0. 18.247 YDOUBLET /
AXIS DIV 60.2 72.24 87.15 85.404 87.2916 90.0985 91.2556 92.4061
94.7118 97.2487 99.44 101.6317 104.28 111.1 /
RADII 0.1 2. 3.5 3.5 3.5 3.5 3.5 3.5 3.5 3.5 3.5 3.5 0.1 /
END GEOMETRY DATA /
BEGIN SUBSET DATA /
SUBSETS OF BOXES /
SUBSET S1 1 TO 6 /
SUBSET S2 7 TO 60 /
SUBSET F1 61 TO 78 /
SUBSET F2 79 TO 87 /
SUBSET F3 88 TO 96 /
SUBSET F4 97 TO 141 /
SUBSET F5 142 TO 186 /
SUBSET UPBDD 187 TO 199 BY 1 /
SUBSET USBDD 200 TO 212 BY 1 /
SUBSET SIBDD 213 TO 225 BY 1 /

```

```

SUBSET LSBOD 226 TO 238 BY 1 /
SURSET BOPUD 239 TO 251 BY 1 /
SUBSETS OF STRIPS /
SUBSET SS1 1 /
SUBSET SS2 2 /
SURSET SS3 3 /
SUBSET SS4 4 /
SUBSET SS5 5 /
SUBSET SS6 6 /
SUBSET SS7 7 /
SUBSET SS8 8 /
SUBSET SS9 9 /
SUBSET SS10 10 /
SUBSET FS1 11 /
SUBSET FS2 12 /
SUBSET FS3 13 /
SUBSET FS4 14 /
SUBSET FS5 15 /
SUBSET FS6 16 /
SUBSET FS7 17 /
SUBSET FS8 18 /
SUBSET FS9 19 /
SUBSET FS10 20 /
SUBSET FS11 21 /
SUBSET FS12 22 /
SUBSET FS13 23 /
SUBSET FS14 24 /
END SUBSET DATA /
BEGIN MODAL DATA /
USE C0002 WITH LIFTING SURFACE F1 F2 F3 F4 F5 /
USE C0003 WITH LIFTING SURFACE S1 S2 /
USE C0001 WITH INTERF BODY ABODY /
USE C0001 WITH BODY DOUBLET ABODY /
END MODAL DATA /
BEGIN OPTION DATA /
VELOCITY PROFILES /
PROFILE VPROH DLE1 160. DTE1 -64. 0. 0. .005 .843 .0125 1. .025 1.095
.05 1.17 .075 1.166 .1 1.153 .125 1.14 .15 1.14 .175 1.14 .2 1.145
.25 1.149 .3 1.158 .35 1.158 .4 1.153 .5 1.127 .6 1.086 .7 1.039
.75 1.02 .8 1.005 .85 .99 .9 .964 .95 .927 .975 .954 .99 .742 1. 0. /
PROFILE VPROF DLE1 160. DTE1 -64. 0. 0. .005 .775 .0125 1. .025 1.118
.05 1.204 .075 1.192 .1 1.17 .125 1.158 .15 1.155 .175 1.158 .2 1.162
.25 1.166 .3 1.17 .35 1.17 .4 1.166 .5 1.14 .6 1.091 .7 1.044 .75 1.02
.8 1.005 .85 .975 .9 .938 .95 .90 .975 .877 .99 .854 1. 0. /
USE VPROH ON SS1 SS2 SS3 SS4 SS5 SS6 SS7 SS8 SS9 SS10 /
USE VPROF ON FS1 FS2 FS3 FS4 FS5 FS6 FS7 FS8 FS9 FS10 FS11 FS12 FS13
FS14 /
PRESSURE CORRECTIONS /
USE .4092 0.0 AS SCALAR ON S1 /
USE .8930 0.0 AS SCALAR ON S2 /
USE .775 0.0 AS SCALAR ON F2 /
USE .8700 0.0 AS SCALAR ON F3 /
END OPTION DATA /
END DOUBLET DATA /
BEGIN AFI DATA /
CASE 1 /
BEGIN GEOMETRY DATA /
MAIN SURFACE HTAIL /
LEADING EDGE 98.155 0.0 41.249 101.107 23.062 39.6363 /
TRAILING EDGE 110.454 0.0 41.249 107.257 23.062 39.6363 /
STRIP FRACTIONS .1 .2 .3 .4 .5 .6 .7 .8 .9 /
MAIN SURFACE VTAIL /
LEADING EDGE 93.15 0.0 43.5 93.15 0.0 38.5 91.55 0.0 35.094
85.404 0.0 21.905 /
TRAILING EDGE 114.37 0.0 43.5 113.278 0.0 41.249 112.0 0.0 38.5
110.45 0.0 35.094 104.28 0.0 21.905 /
STRIP DISTANCES 1.1255 3.6255 6.703 10.0546 11.7033 13.3519 15.0005
16.649 18.2978 19.9464 /
END GEOMETRY DATA /
BEGIN MODAL DATA /
USE C0002 WITH MAIN SURFACE VTAIL /

```

USE C0003 WITH MAIN SURFACE HTAIL /
END MODAL DATA /
END AFI DATA /
BEGIN FLUTTER DATA /
CASE 1 /
ALTITUDE 0.0 /
END FLUTTER DATA /
END PROBLEM DATA /

**Table 212-1. Natural Frequencies,
YC-14 Empennage**

(1) Mode Number	Frequency (Hertz)		(4)
	(2) Experimental	(3) ATLAS	$\frac{(3)-(2)}{(2)} \times 100$ (%)
1	4.87	4.90	0.6
2	6.90	6.77	-1.9
3	11.30	11.22	-0.7
4	26.60	28.62	7.6
5	41.55	41.98	1.0

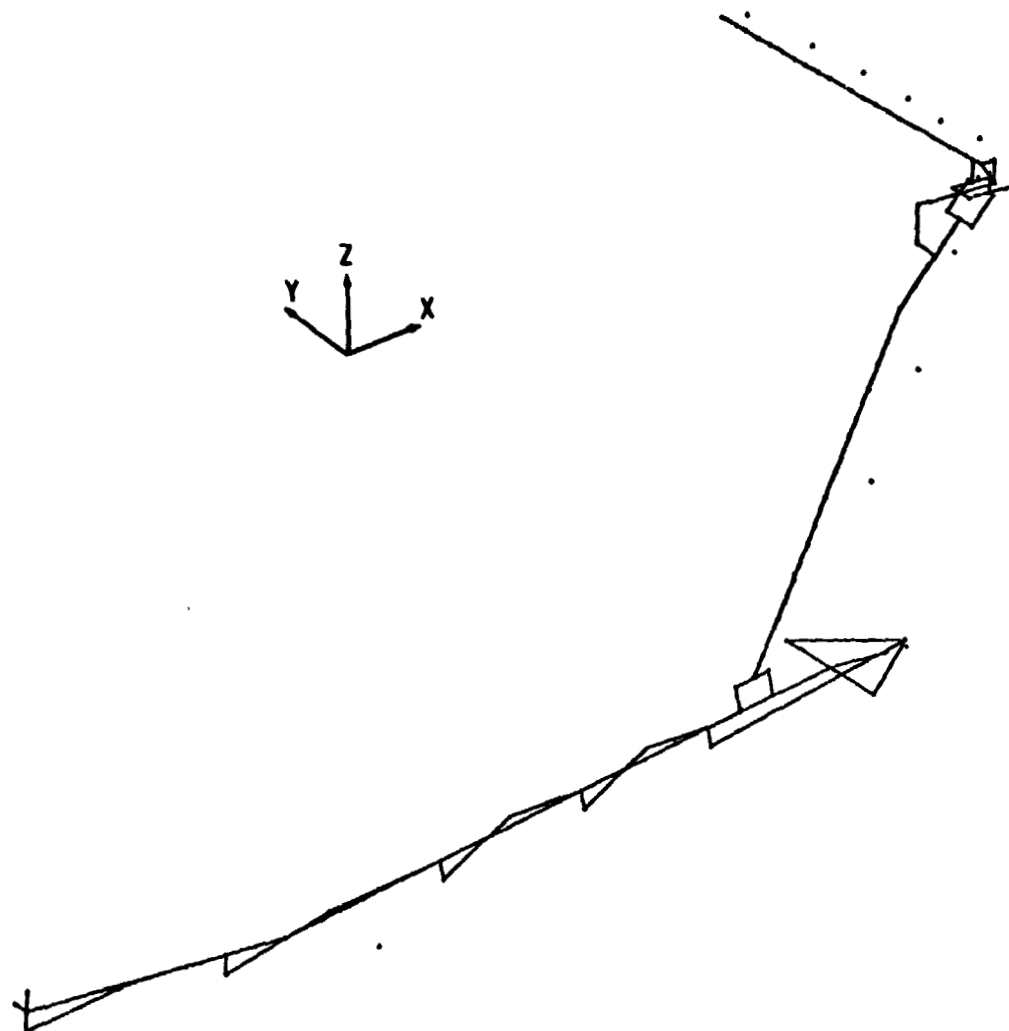


Figure 212-1. Structural Model, YC-14 Empennage

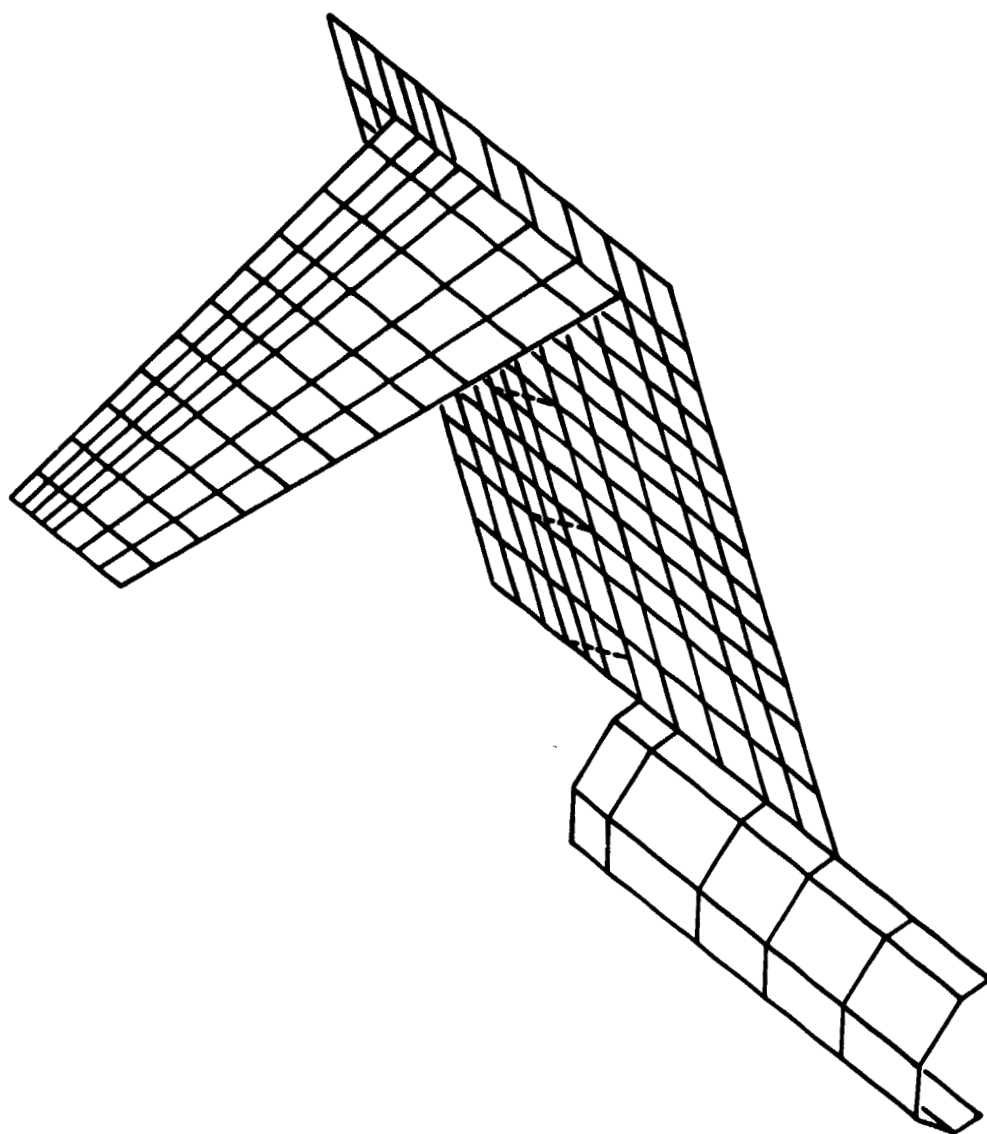


Figure 212-2. Aerodynamic Modeling for YC-14 Empennage Surfaces

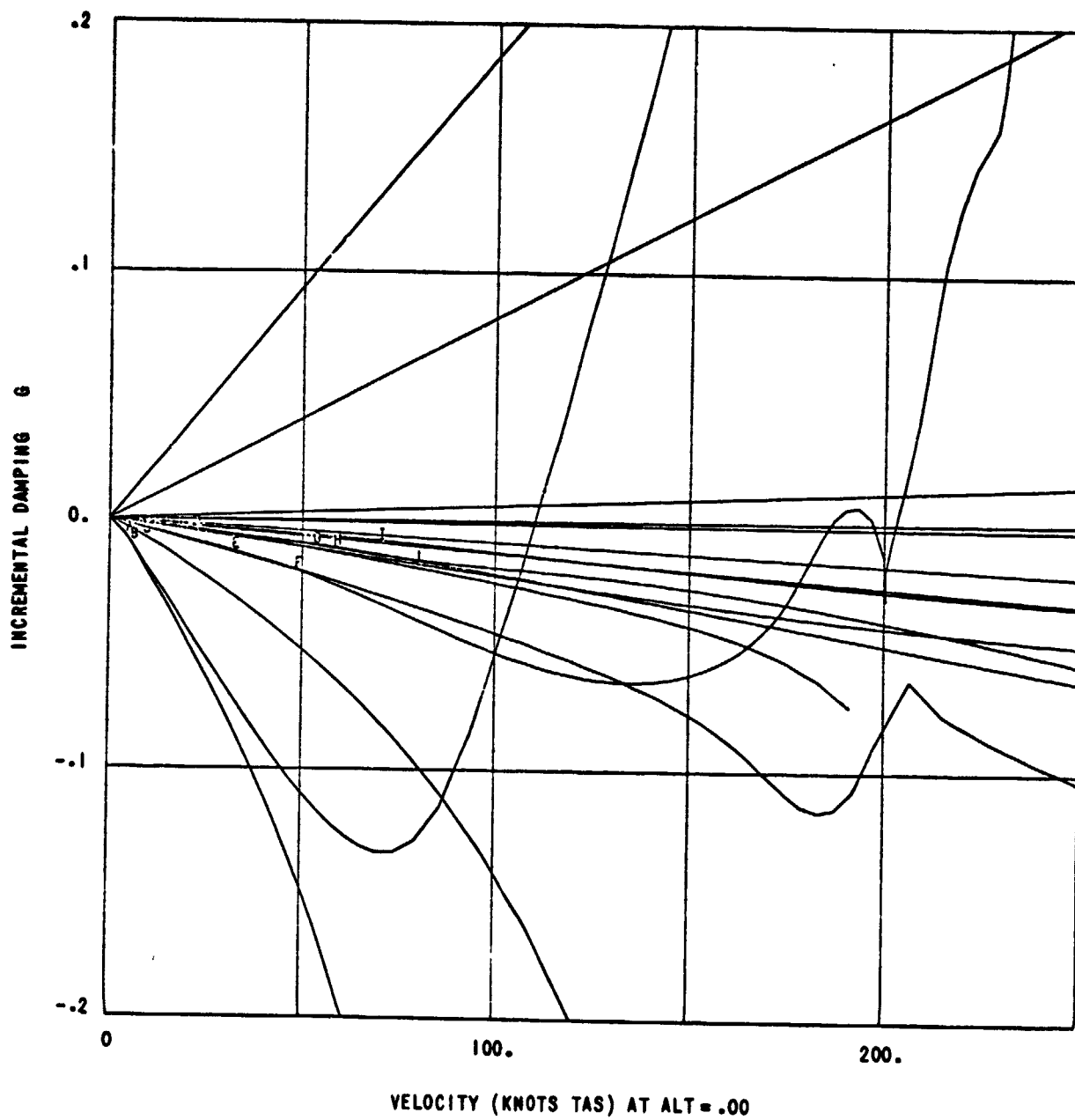


Figure 212-3. V-g Plot, YC-14 Empennage

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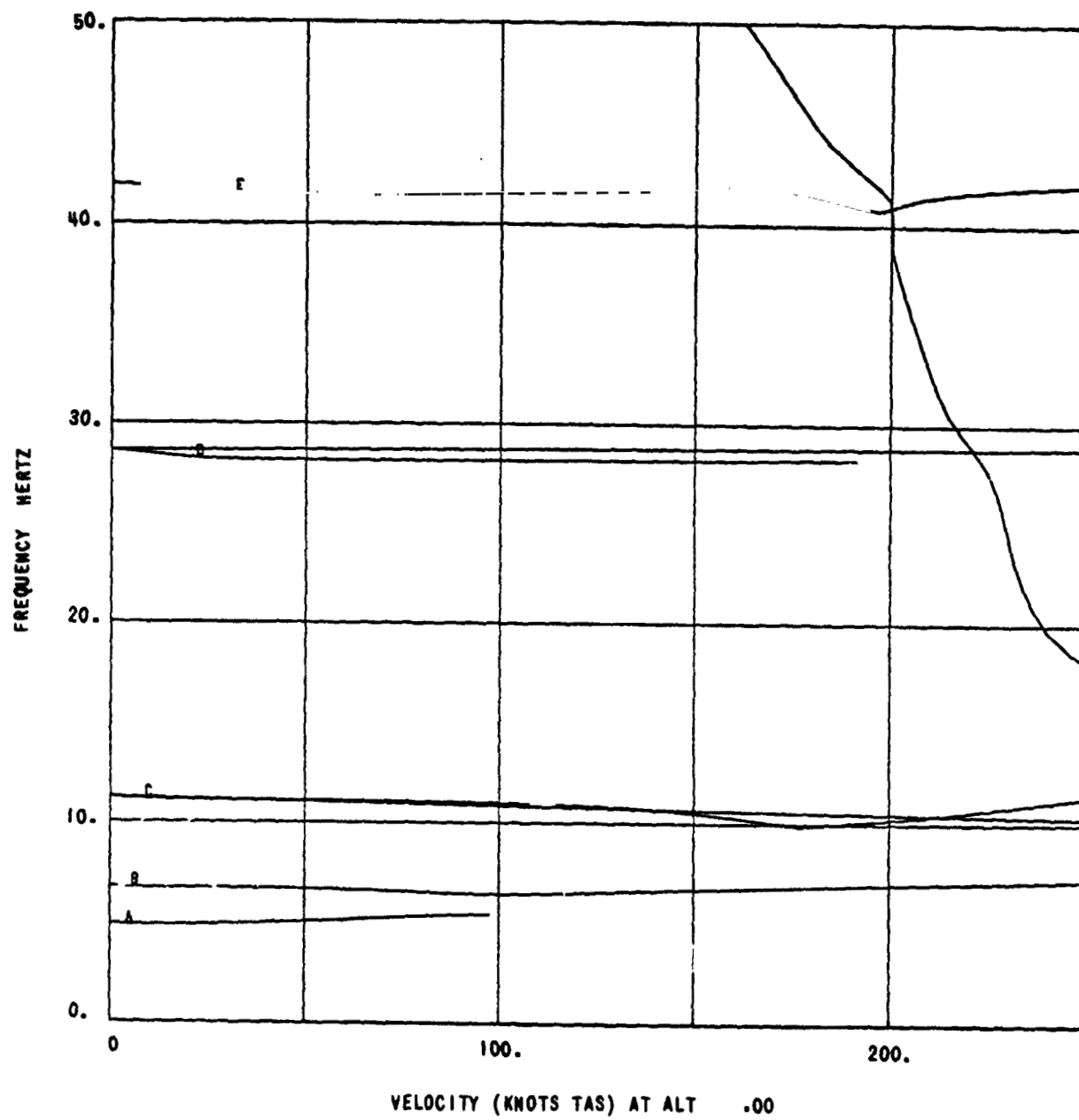


Figure 212-4. V-f Plot, YC-14 Empennage

213. 3D STRESS ANALYSIS OF A ROTATING DISK (DECK 12)

213.1 DESCRIPTION OF ANALYSIS

A 3D stress analysis is performed on a rotating disk subjected to the following loads:

- Inertia loads due to angular velocity and acceleration
- Pressure in central hole and on rim
- Thermal loading

The disk is shown in figure 213-1. Rotation is about an axis perpendicular to the plane of the disk. The pressures act in the plane of the disk and are uniform through the thickness of the disk. Two thermal loadcases are applied: a uniform temperature increase and a temperature increase varying linearly in the radial direction and uniform through the thickness.

A 30° sector of the disk is modelled using 20-node BRICK elements. Only one-half of the thickness is modelled and symmetry enforced upon the mid-surface. The model is shown in figure 213-2.

213.2 RESULTS

Radial and tangential stress components due to constant angular velocity, ω , are presented in figure 213-3. The solid lines represent the theory of elasticity solution (ref. 213-1).

Shear stresses due to angular acceleration, α , are presented in figure 213-4. The solid line represents the theory of elasticity solution (ref. 213-2).

Radial and tangential stress components due to pressure loading in the bore and on the rim are presented in figures 213-5 and 213-6, respectively. The solid lines represent the theory of elasticity solution (ref. 213-1).

Element stresses due to the uniform temperature increase are zero within the accuracy of the computer. Displacements are also exact within machine accuracy. Radial and tangential stress components due to the radial temperature gradient are presented in figure 213-7. The solid lines represent the theory of elasticity solution (ref. 213-1).

213.3 LISTING OF CONTROL PROGRAM AND DATA

```

BEGIN CONTROL PROGRAM DEMO12
PROBLEM ID(DEMO12 - 3D STRESS ANALYSIS OF A ROTATING DISK)

C
C PURPOSE      THE PRINCIPAL CAPABILITIES DEMONSTRATED BY THIS
C              DECK ARE
C              1. 3D STRESS ANALYSIS
C              2. THERMAL LOADING
C              3. INERTIA LOADING
C
C CORE        140K (OCTAL)
C
C AUTHOR      R. A. SAMUEL
C
READ INPUT(MODE2)
PRINT INPUT (NODAL)
PRINT INPUT(MATERIAL)
PRINT INPUT(STIFFNESS)
PRINT INPUT(BC)
PRINT INPUT(LOADS)
EXECUTE EXTRACT(EXNAME=DISK,LSUB=KGRID,ESUB=E1,NSUB=N1)
EXECUTE GRAPHICS(GNAME=BRICKS,OFFLINE=CALCOMP,RZ=30,RX=0,RY=20,
X      TYPE=ORTH,SIZE=(20.,20.),LABEL=E,EXNAME=DISK)
EXECUTE MASS(OPTION=4)
PERFORM STRESS
PRINT OUTPUT(LOADS)
PRINT OUTPUT(DISP,CYL)
PRINT OUTPUT(STRESS)
PRINT OUTPUT(REACTIONS,EQCHK)
PRINT INPUT(BC,STAGE=2)
PRINT INPUT(LOADS,STAGE=2)
EXECUTE LOADS(STAGE=2)
EXECUTE MERGE(STIFFNESS,STAGE=2,KK11=11,KK13=13)
EXECUTE MERGE(LOADS,STAGE=2,LL11=11,LL31=31)
EXECUTE CHOLESKY(SOLVE,KK11,DD11,LL11)
EXECUTE STRESS(STAGE=2,D1=DD11)
EXECUTE MULTIPLY(RR31=[-LL31+KK13(T)*DD11])
PRINT OUTPUT(LOADS,L11=LL11,L31=LL31,STAGE=2)
PRINT OUTPUT(DISP,STAGE=2,CYL)
PRINT OUTPUT(STRESS,STAGE=2)
PRINT OUTPUT(REACTIONS,R31=RR31,EQCHK,STAGE=2)
PURGE FILES(STIFRNF,STRERNF,LOADRNF)
EXECUTE STIFFNESS(BIGBRICK)
EXECUTE LOADS
EXECUTE STRESS(D1=DD11)
PRINT OUTPUT(STRESS)
PRINT OUTPUT(STRESS,BIGBRICK=NODAL)
EXECUTE LOADS(STAGE=2)
EXECUTE STRESS(STAGE=2,D1=DD11)
PRINT OUTPUT(STRESS,STAGE=2)
PRINT OUTPUT(STRESS,STAGE=2,BIGBRICK=NODAL)
END CONTROL PROGRAM

```

```

BEGIN MATERIAL DATA
M51 .1
-200 11.3E6 .3 4.34E6 -.003
400 9.3E6 .3 3.58E6 .003
END MATERIAL DATA
BEGIN NODAL DATA
ANALYSIS FRAME INPUT
CYL CAN 0. 0. 0., 5. 0. 0., 0. 0. 5.
1 .375 0. 0. TO 3 .375 30. 0.
**2 11 .5 0. 0. 0 11 .5 0. 0.
**2 11 1. 0. 0. 0 11 1. 0. 0.
**1 11 1.375 0. 0. 0 11 1.375 0. 0.
141 .375 0. .15 TO 143 .375 30. .15
**2 11 .5 0. 0. 0 11 .5 0. 0.
**2 11 1. 0. 0. 0 11 1. 0. 0.
**1 11 1.375 0. 0. 0 11 1.375 0. 0.
8 .625 0. 0. TO 9 .625 30. 0.
**1 11 .5 0. 0. 0 11 .5 0. 0.
**1 11 .75 0. 0. 0 11 .75 0. 0.
**1 11 1. 0. 0. 0 11 1. 0. 0.
**1 11 1.125 0. 0. 0 11 1.125 0. 0.
148 .625 0. .15 TO 149 .625 30. .15
**1 11 .5 0. 0. 0 11 .5 0. 0.
**1 11 .75 0. 0. 0 11 .75 0. 0.
**1 11 1. 0. 0. 0 11 1. 0. 0.
**1 11 1.125 0. 0. 0 11 1.125 0. 0.
71 .375 0. .075 TO 73 .375 30. .075 BY 2
**2 11 .5 0. 0. 0 11 .5 0. 0. **
**2 11 1. 0. 0. 0 11 1. 0. 0. **
**1 11 1.375 0. 0. 0 11 1.375 0. 0. **
RESUME GLOBAL
210 0. 0. -1.
211 0. 0. 1.
212 -9.7 -.26 .075
REORDER FROM 212
END NODAL DATA
BEGIN STIFFNESS DATA
BEGIN ELEMENT DATA
BRICK M51 1 3 143 141 12 14 154 152 2 73 142 71 13 84 153 82 8 9 149 148
**4 0 0 11 **19
BEAM N200 210 211 1 1.
END ELEMENT DATA
END STIFFNESS DATA
BEGIN BC DATA
SET 1 STAGE 1 / SYMMETRIC BC
SUPPORT TZ FOR 210
SUPPORT TT FOR 1 TO 143
SUPPORT ASYM IN SURFACE 3 THROUGH 1
SET 1 STAGE 2 / ANTISYMMETRIC BC
SUPPORT TR FOR 1 TO 198
SUPPORT ASYM IN SURFACE 3 THROUGH 1
SUPPORT TT FOR 1 TO 3 71 73 141 TO 143
SUPPORT TZ FOR 210
END BC DATA
BEGIN LOAD DATA
LOAD CASE ID INTPRES ** PRESSURE IN HOLE *
LOAD CASE ID RIMPRES ** PRESSURE ON RIM *
LOAD CASE ID OMEGA ** CONSTANT OMEGA = 2000 *
LOAD CASE ID TTERM ** UNIFORM DELTA(T) *
LOAD CASE ID TIRMLIN ** DELTA(T) = 120*R - 270 *
LOAD CASE ID BEARLD ** AXIAL LOAD ON BEAM *
BEGIN INERTIA LOAD DATA
AXIS 210 211
CASE OMEGA
2000.
END INERTIA LOAD DATA
BEGIN ELEMENT LOAD DATA
DIRECTION ELEMENT -1. 0. 0.
CASE INTPRES
1 1 10000.
CASE RIMPRES
5 2 789.
END ELEMENT LOAD DATA

```

```

BEGIN ELEMENT THERMAL LOAD DATA
  CASE THERM
    1 TO 5 200.
END ELEMENT THERMAL LOAD DATA
BEGIN NODAL THERMAL LOAD DATA
  CASE THRMLIN
    1 TO 3 71 73 141 TO 143 -225.
    8 9 148 149 -195.
    12 TO 14 82 84 152 TO 154 -165.
    19 20 155 160 -135.
    23 TO 25 93 95 163 TO 165 -105.
    30 31 170 171 -45.
    34 TO 36 104 106 174 TO 176 15.
    41 42 181 182 75.
    45 TO 47 115 117 185 TO 187 135.
    52 53 192 193 210.
    56 TO 58 126 128 196 TO 198 300.
END NODAL THERMAL LOAD DATA
BEGIN NODAL LOAD DATA
  CASE BEAML0
    211 FZ 1000.
END NODAL LOAD DATA
SET 1 STAGE 2
  LOAD CASE 10 ALPHA ** ALPHA = 5000 *
  BEGIN INERTIA LOAD DATA
    AXIS 210 211
    CASE ALPHA
      0. 5000.
  END INERTIA LOAD DATA
END LOADS DATA
BEGIN SUBSET DEFINITION
  SUBSETS OF STIFFNESS SET 1
    E1 = BRICKS
    N1 = ALL
    EXCLUDE 212 FROM N1
END SUBSET DEFINITION
END PROBLEM DATA

```


ν = Poisson's ratio
 ρ = Mass density
 ω = Angular velocity
 α = Angular acceleration
 T = Temperature
 β = Coefficient of thermal expansion

$a = 0.00953 \text{ m (0.375 in.)}$

$b = 0.121 \text{ m (4.75 in.)}$

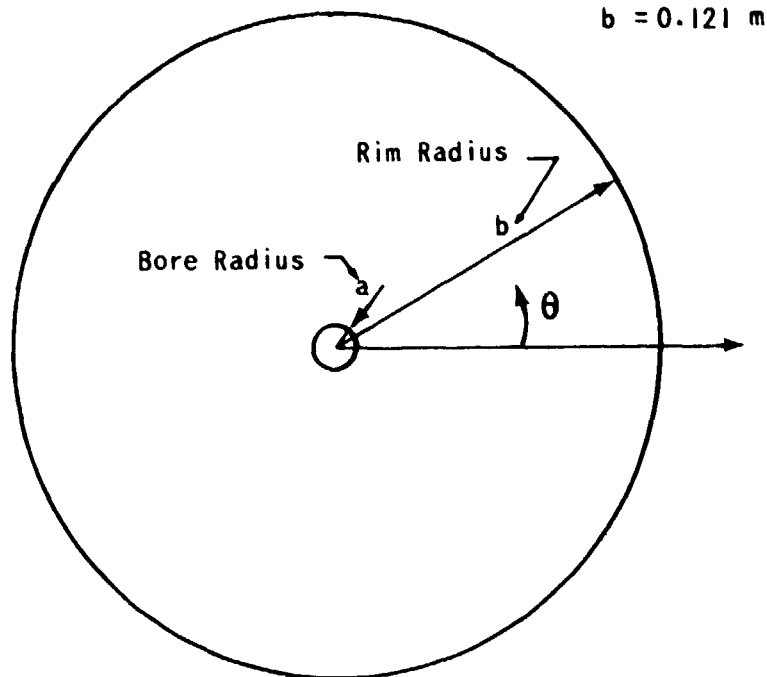


Figure 213-1. Disk

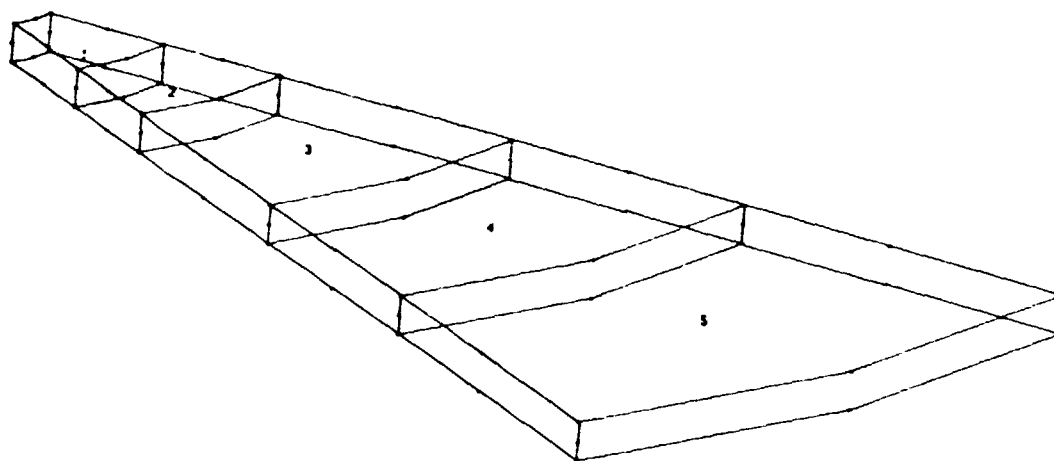


Figure 213-2. Model of Disk Segment

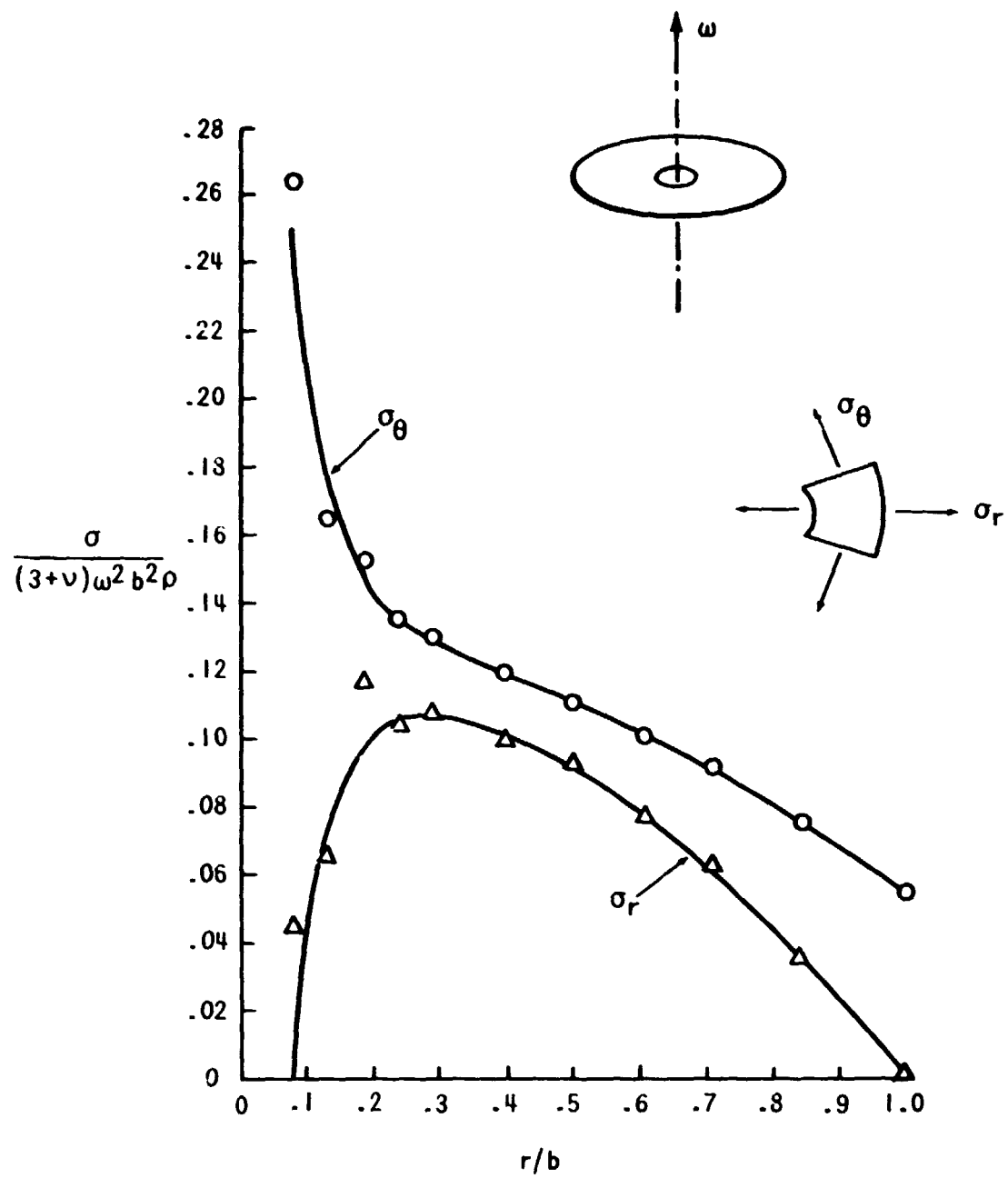


Figure 213-3. Stresses Due to Angular Velocity

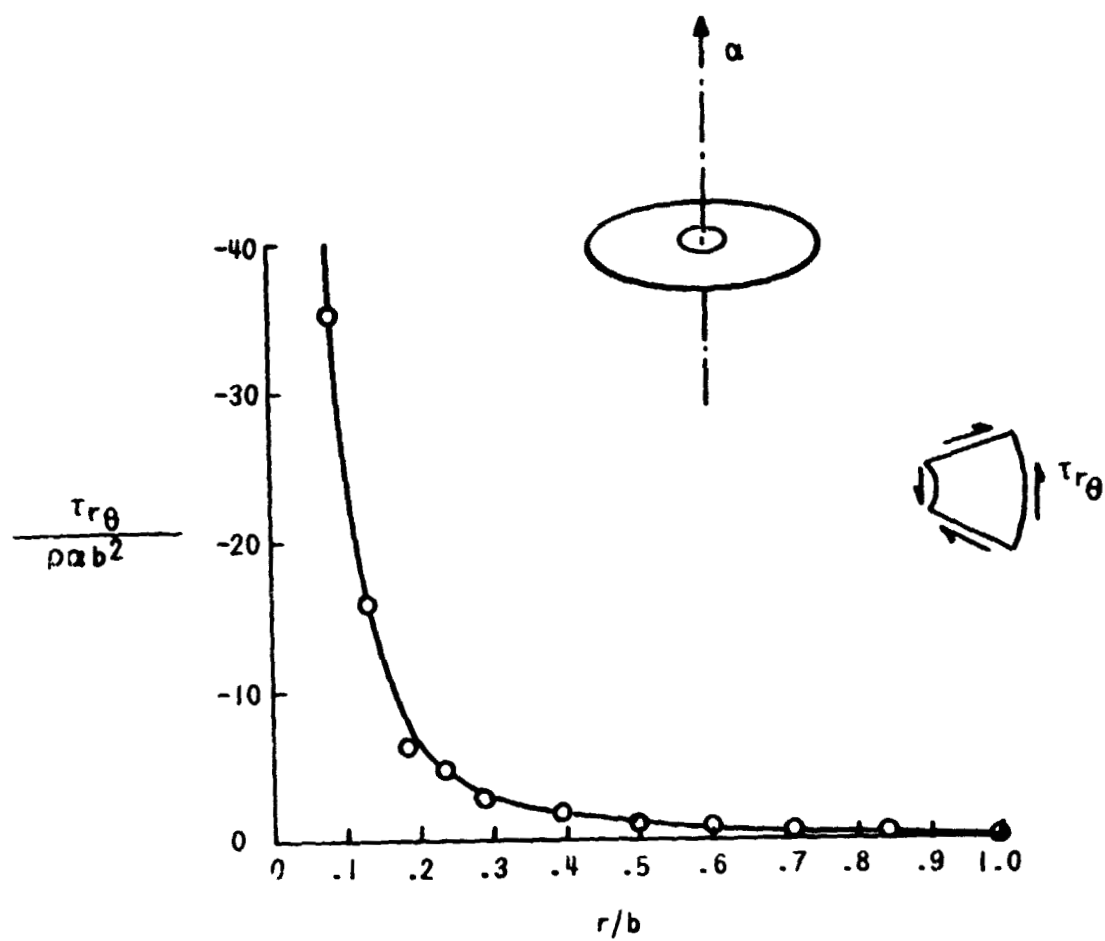


Figure 213-1. Stresses Due to Angular Acceleration

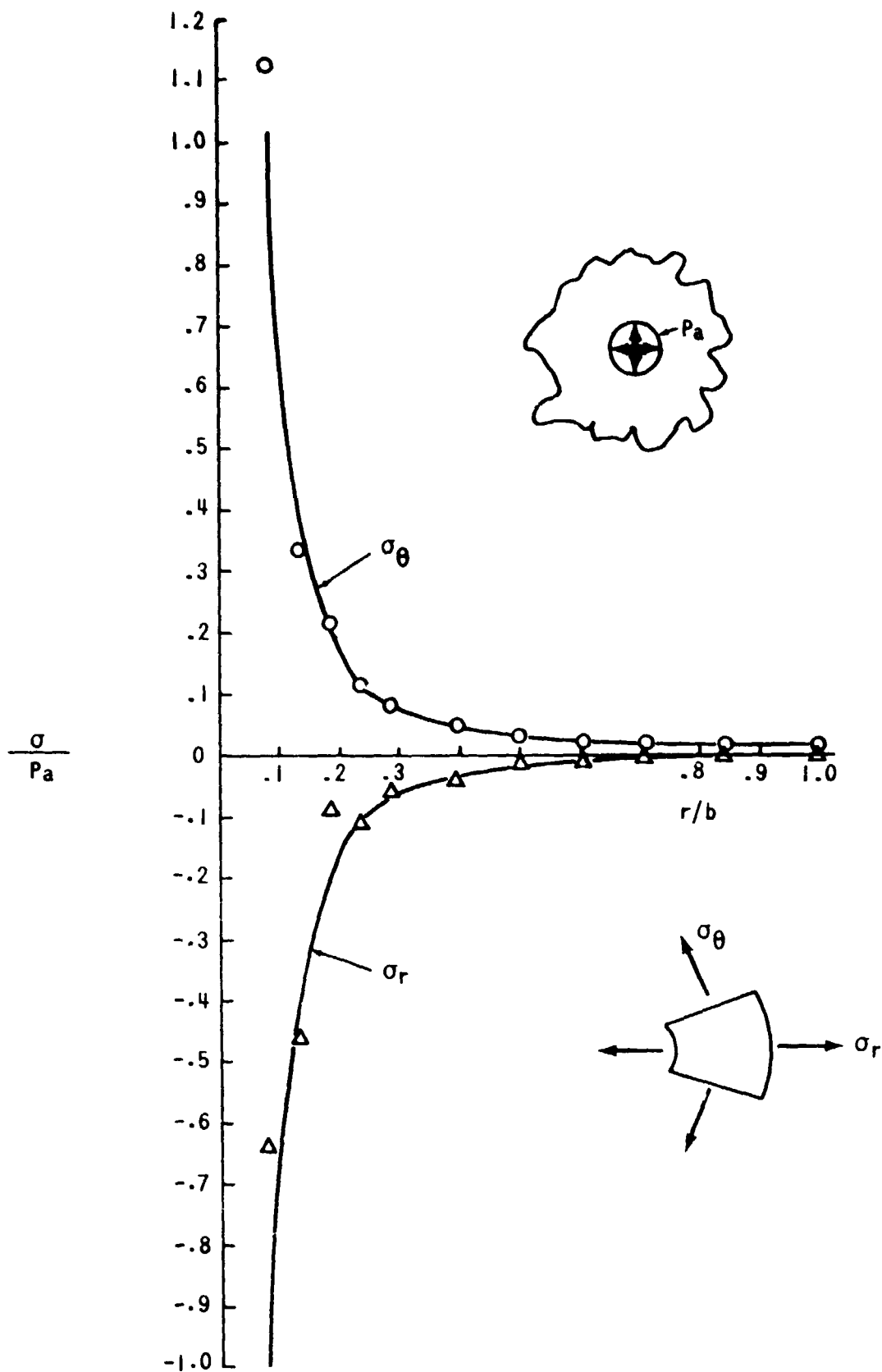


Figure 213-5. Stresses Due to Bore Pressure

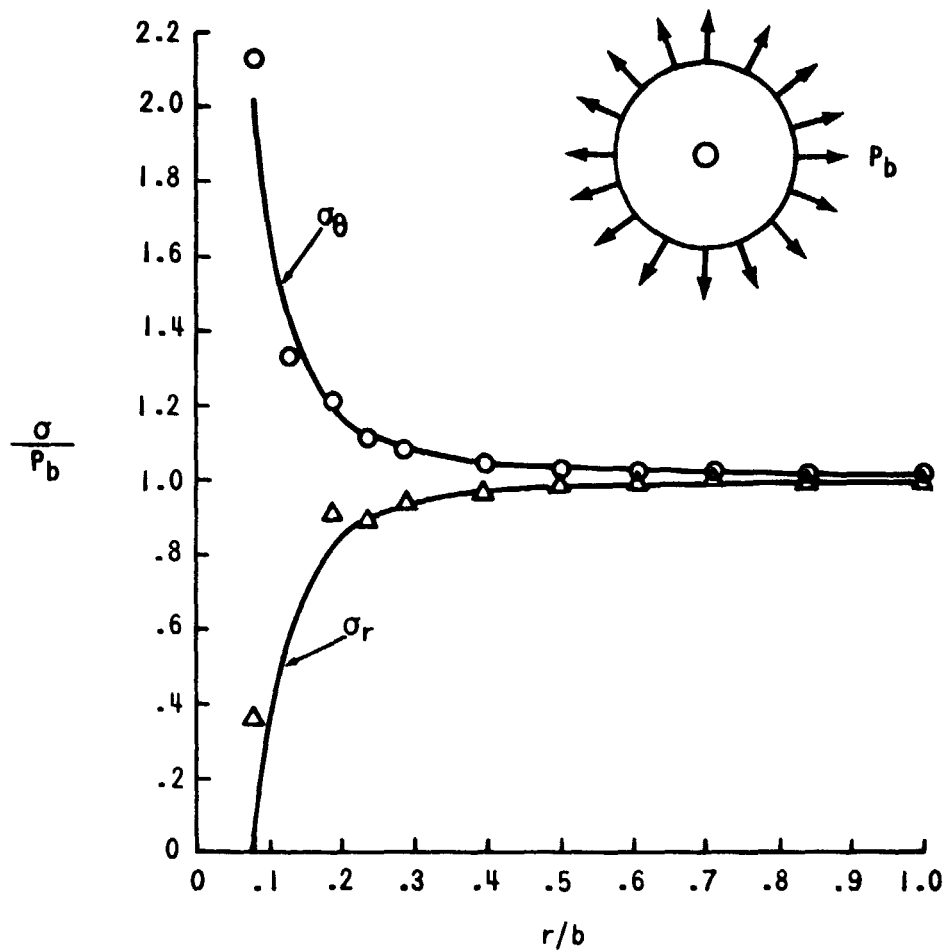
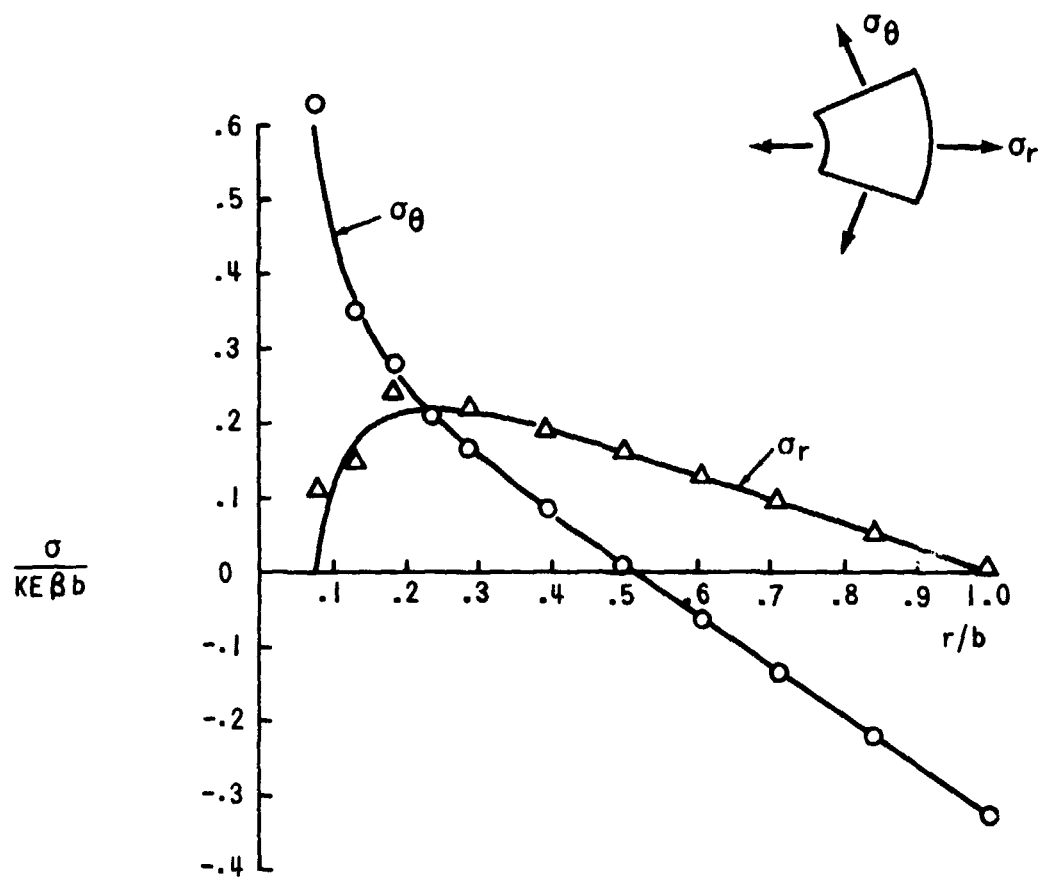


Figure 213-6. Stresses Due to Rim Pressure



Linear thermal gradient from center to rim,
 $\Delta T = Kr$

Figure 213-7. Stresses Due to Thermal Loading

301. ATLAS/FLEXSTAB INTERFACES (DECKS 5 AND 6)

301.1 DESCRIPTION OF DEMONSTRATION

The method used to demonstrate the ATLAS-to-FLEXSTAB and FLEXSTAB-to-ATLAS interfaces is shown schematically in figure 301-1. The structural model is shown in figure 301-2. The body is modelled using BEAMS for the frames, RODs for stringers and SPLATES for the surfaces. The wing is modelled using SPAR and COVER elements. All mass is obtained from a separate mass model consisting of mass PLATE elements and concentrated masses. The mass model is shown in figure 301-3. Symmetric and antisymmetric boundary conditions are imposed in the plane $Y=0$.

A reduced flexibility matrix is generated for each boundary condition stage. A diagonal mass matrix is produced directly by the Mass Processor. The interface routines MASSFIL and FLEXFIL are then executed to create the FLEXSTAB input tape NASTAP.

The FLEXSTAB system is executed, producing nodal loads for two symmetric conditions on the SDSS output tape. These nodal loads are read by the interface routine STREFIL and written onto the file DATARNF. The nodal loads are read from DATARNF by the Loads Preprocessor and used to perform an ATLAS stress analysis.

In addition to the stress analysis, the Mass Processor is executed to produce panel weights corresponding to the FLEXSTAB aerodynamic panels. These panel weights, together with airloads data from the SDSS output tape, are used by the routine VAMAT to calculate net shear, moment and torsion at various cuts along the wing and body. These net loads for each condition are searched by the routine VAMSCN to obtain the minimum and maximum values at each cut.

301.2 RESULTS

FLEXSTAB detected no errors while reading the ATLAS-generated NASTAP tape. The airloads calculated by FLEXSTAB appeared reasonable. No errors were detected by ATLAS while using the FLEXSTAB-generated SDSS tape. Displacements and stresses appeared reasonable.

Comparison of the VAMAT and VAMSCN results confirmed that the correct maxima and minima were found. The body bending moment, as calculated by VAMAT, is shown in figure 301-3.

301.3 LISTING OF CONTROL PROGRAM AND DATA

```

C BEGIN CONTROL MATRIX PROGRAM DEMO05
C PROBLEM ID (DEMO05 - ATLAS-TO-FLEXSTAB INTERFACE)
C
C PURPOSE      THE PRINCIPAL CAPABILITIES DEMONSTRATED BY THIS
C               DECK ARE
C               1. ATLAS-TO-FLEXSTAB INTERFACE
C               2. PLOTS OF MASS MODEL
C
C AUTHOR       F. P. GRAY
C
C CORE         13CK (OCTAL)
C
C DIMENSION FET (100,3),FETS(550)
C
C READ INPUT
C PRINT INPUT(NODAL)
C PRINT INPUT(STIFFNESS)
C PRINT INPUT(MASS)
C EXECUTE EXTRACT(EXNAME=STIF,LSUB=KGRIC,ESUB=E1,NSUB=N5)
C EXECUTE GRAPHICS(GNAME=GEOM,TYPE=(ORTH,POINT),SIZE=(30.,20.),
X      OFFLINE=GERBER,RZ=30.,RX=0.,RY=20.,EXNAME=STIF)
C EXECUTE EXTRACT(EXNAME=MASS,LSUB=MGPID,ESUB=E4,NSUB=N6)
C EXECUTE GRAPHICS(GNAME=GEOM,TYPE=(ORTH,POINT),SIZE=(30.,20.),
X      RZ=30.,RX=0.,FY=20.,EXNAME=MASS)
C EXECUTE MASS(OPTION=2)
C PERFORM F-REDUCE(STAGE=1,[K]=[K1],[FRED]=[FLEX1])
C PERFORM F-REDUCE(STAGE=2,[K]=[K2],[FRED]=[FLEX2])
C PRINT INPUT(BC)
C CALL FILEADD(FET,MULTRNF,MASSRNF,DATARNF)
C CALL FETADD(SAVESSF,FETS,550,1,0,IKR)
C REWIND SAVESSF
C N=1
C CALL MASSFIL(7LMOC001A,N,N)
C CALL FLEXFIL(5LFLEX1)
C CALL FLEXFIL(5LFLEX2)
C END

```

```

BEGIN NODAL DATA /
1 20. 0. 1. TO 9 340. 0. 65. BY 2 /
101 20. 0. -1. TO 109 340. 0. -65. BY 2 /
201 20. 1. 0. TO 209 340. 65. 0. BY 2 /
11 420. 0. 65. TO 83 3300. 0. 65. BY 2 /
111 420. 0. -65. TO 189 3540. 0. -65. BY 2 /
211 420. 65. 0. TO 225 980. 65. 0. BY 2 /
265 2580. 65. 0. TO 277 3060. 65. 0. BY 2 /
287 3460. 65. 0. TO 289 3540. 65. 0. BY 2 /
*/ WING COORDINATES /
227 1060. 65. 0. 26.25 TO 245 1780. 65. 0. 36.35 BY 2 /
245 TO 255 2180. 65. 0. 28.8 BY 2 /
255 TO 263 2500. 65. 0. 12.0 BY 2 /
327 1060. 65. 0. 26.25 TO 341 1620. 265. 0. 8.85 BY 2 /
445 1780. 195. 0. 22.65 TO 455 2180. 195. 0. 20.15 BY 2 /
541 1620. 265. 0. 8.85 TO 551 2205. 455. 0. 5.75 BY 2 /
651 2205. 455. 0. 5.75 TO 656 2545. 594. 0. 3.2 /
756 2545. 594. 0. 3.2 TO 760 2875. 765. 0. .95 /
760 TO 763 2995. 765. 0. 1.85 /
341 TO 355 2180. 255. 0. 20.15 BY 2 /
355 TO 363 2500. 265. 0. 11.25 BY 2 /
551 TO 559 2525. 455. 0. 10.0 /
559 TO 563 2685. 455. 0. 5.0 /
656 TO 659 2665. 594. 0. 4.85 /
659 TO 663 2825. 594. 0. 2.45 /
*/ HORIZONTAL TAIL /
279 3140. 65. 0. 1.80 /
779 3140. 65. 0. 1.80 TO 979 3365. 200. 0. 1.25 BY 100 /
281 3220. 65. 0. 4.25 /
781 3220. 65. 0. 4.25 TO 981 3388. 200. 0. 1.75 BY 100 /
283 3300. 65. 0. 4.55 /
783 3300. 65. 0. 4.55 TO 983 3412. 200. 0. 1.80 BY 100 /
285 3380. 65. 0. 1.40 /
785 3380. 65. 0. 1.40 TO 985 3435. 200. 0. .80 BY 100 /
*/ VERTICAL TAIL /
REC REC1 0. 0. 0. 1. 0. 0. 0. -1. 0. /
95 3380. 65. 0. 3.25 /
87 3460. 65. 0. 2.40 /
1085 3460. 140. 0. 1.50 /
1087 3500. 140. 0. 1.80 /
*/ WING FIN /
1156 2545. .1 -594. 2.40 TO 1356 2830. 100. -594. 1.80 BY 100 /
1158 2625. .1 -594. 2.40 TO 1358 2842. 100. -594. 1.90 BY 100 /
1161 2745. .1 -594. 2.80 TO 1361 2850. 100. -594. 1.95 BY 100 /
1163 2825. .1 -594. 2.80 TO 1363 2870. 100. -594. 2.05 BY 100 /
RESUME GLOBAL
89 3540. 0. 65. /
*/ WEIGHT PANELS - BODY /
6001 0. 0. 0. TO 6016 3564. 0. 0. /
6021 0. 65. 0. TO 6036 3564. 65. 0. /
*/ WEIGHT PANELS - WING /
6100 741.0 65.0 0. TO 6220 2487.0 594.0 0. BY 20 /
6100 TO 6260 2487.0 594.0 0. BY 80 /
6180 TO 6240 2487.0 594.0 0. BY 20 /
6260 TO 6320 2884.0 794.0 0. BY 20 /
6110 2715.0 65.0 0. TO 6170 2715.0 329.5 0. BY 20 /
6189 2715.0 329.5 0. TO 6249 2874.0 594.0 0. BY 20 /
6266 2874.0 594.0 0. TO 6326 3054.0 794.0 0. BY 20 /
6100 TO 6110 /
**3 20 0 20 /
6180 TO 6189 /
**3 20 0 20 /
6260 TO 6266 /
**3 20 0 20 /
*/ WEIGHT PANELS - HOR TAIL /
6400 3124. 65.1 0. TO 6403 3417. 65.1 0. /
6410 3386. 228.0 0. TO 6413 3464. 228.0 0. /
END NODAL DATA /

```

```

BEGIN STIFFNESS DATA /
BEGIN ELEMENT DATA /
*/ WING SPARS /
SPAR M5      227 329      .06 1. /
SPAR M5      247 447      .10 2.0 TO 253 553 BY 2 2 /
SPAR M5      329 331      .06 1. TO 339 341 BY 2 2 /
SPAR M5      341 543      .06 1. /
SPAR M5      543 545      .06 1. TO 549 551 BY 2 2 /
SPAR M5      551 653      .06 1. /
SPAR M5      653 655      .06 1. /
SPAR M5      655 656      .06 1. /
SPAR M5      656 757      .06 1. /
SPAR M5      757 758      .06 1. TO 759 760 /
SPAR M5      263 363      .20 6. /
SPAR M5      363 563      .17 6. /
SPAR M5      563 663      .15 4. /
SPAR M5      663 763      .15 2. /
SPAR M5      229 329      .1 1. TO 243 343 BY 2 2 /
SPAR M5      245 445      .18 1. /
SPAR M5      445 345      .18 1. /
SPAR M5      447 347      .1 2. TO 453 353 BY 2 2 /
SPAR M5      255 455      .3 6. /
SPAR M5      455 353      .3 6. /
SPAR M5      257 357      .12 6. TO 261 361 BY 2 2 /
SPAR M5      343 543      .1 1. TO 345 545 BY 2 2 /
SPAR M5      347 547      .1 2. TO 353 553 BY 2 2 /
SPAR M5      355 555      .1 4. /
SPAR M5      357 557      .1 5. TO 361 561 BY 2 2 /
SPAR M5      553 653      .06 2. TO 555 655 BY 2 2 /
SPAR M5      556 656      .03 2. TO 562 662 /
SPAR M5      657 757      .03 1. TO 662 762 /
*/ WING RIBS /
SPAR M5      445 447      .17 2. TO 453 455 BY 2 2 /
SPAR M5      341 343      .10 1.5 TO 361 363 BY 2 2 /
SPAR M5      551 553      .10 2. TO 553 555 BY 2 2 /
SPAR M5      555 556      .10 2. TO 562 563 /
SPAR M5      656 657      .06 1. TO 662 663 /
SPAR M5      760 761      .15 .7 TO 762 763 /
*/ WING COVERS /
COVER M5      229 329 227      .03 /
COVER M5      229 329 331 231 .03 TO 241 341 343 243 BY 2 **3 /
COVER M5      243 343 445 245 .03 /
COVER M5      445 345 343      .03 /
COVER M5      245 247 447 445 .06 .0 TO 253 255 455 453 BY 2 **3 /
COVER M5      445 345 347 447 .03 TO 453 353 355 455 BY 2 **3 /
COVER M5      255 455 357 257 .05 .07 /
COVER M5      455 355 357      .05 .07 /
COVER M5      257 357 359 259 .05 .07 /
COVER M5      259 359 361 261 .13 .07 .11 .0 TO 261 361 363 263 BY 2 **3 /
COVER M5      343 543 341      .03 /
COVER M5      343 543 545 345 .03 TO 353 553 555 355 BY 2 **3 /
COVER M5      355 555 557 357 .05 .04 TO 357 557 559 359 BY 2 **3 /
COVER M5      359 559 561 361 .15 .07 .10 .0 TO 361 561 563 363 BY 2 **3 /
COVER M5      553 653 551      .15 .07 .11 .06 /
COVER M5      553 653 655 555 .15 .07 .11 .06 /
COVER M5      555 655 656 556 .15 .07 .11 .06 TO 562 662 663 563 /
COVER M5      657 757 656      .04 /
COVER M5      657 757 758 658 .04 TO 662 762 763 663 /
*/ HORIZONTAL TAIL /
SPAR M5      279 879 .05 .6 /
SPAR M5      879 979 .05 .6 /
SPAR M5      281 881 .025 .9 /
SPAR M5      881 981 .025 .9 /
SPAR M5      283 883 .025 .8 /
SPAR M5      883 983 .025 .8 /
SPAR M5      285 885 .10 1.3 /
SPAR M5      885 985 .10 1.3 /
SPAR M5      879 881 .05 .6 TO 883 885 BY 2 2 /
SPAR M5      979 981 .05 .6 TO 983 985 BY 2 2 /
COVER M5      279 879 881 281 .08 /
**2 0 0 2 **3 0. /
COVER M5      879 979 981 881 .035 /
**2 0 0 2 **3 0. /
*/ WING FIN /

```

SPAR M5 1156 1256 .025 .5 TO 1256 1356 BY 100 100 /
 SPAR M5 1158 1258 .025 .5 TO 1258 1358 BY 100 100 /
 SPAR M5 1161 1261 .025 .5 TO 1261 1361 BY 100 100 /
 SPAR M5 1163 1263 .025 .5 TO 1263 1363 BY 100 100 /
 SPAR M5 1256 1258 .025 .5 TO 1356 1358 BY 100 100 /
 SPAR M5 1258 1261 .025 .5 TO 1358 1361 BY 100 100 /
 SPAR M5 1261 1263 .025 .5 TO 1361 1363 BY 100 100 /
 COVER M5 1156 1256 1258 1158 .025 TO 1256 1356 1358 1258
 BY 100 100 100 100 /
 COVER M5 1158 1258 1261 1161 .025 TO 1258 1358 1361 1261
 BY 100 100 100 100 /
 COVER M5 1161 1261 1263 1163 .025 TO 1261 1361 1363 1263
 BY 100 100 100 100 /
 */ VERTICAL TAIL /
 COVER M5 85 1085 1087 87 .0 0.035 /
 BEAM M5 85 1085 0.5 0.1 0.1 50. 50. 50. /
 BEAM M5 1085 1087 0.5 0.1 0.1 50. 50. 50. /
 BEAM M5 87 1087 0.5 0.1 0.1 50. 50. 50. /
 */ BODY /
 */ STRINGERS /
 ROD M5 1 3 2.37 TO 23 25 BY 2 2 /
 **2 0 0 100 100 0. 0 100 100 0 0 /
 **1 0 **3 0. 0 **5 /
 ROD M5 25 27 4. TO 43 45 BY 2 2 /
 **2 0 0 100 100 0. 0 100 100 0 0 /
 **1 0 **3 0. 0 **5 /
 ROD M5 45 47 5.35 TO 67 69 BY 2 2 /
 **2 0 0 100 100 0. 0 100 100 0 0 /
 **1 0 **3 0. 0 **5 /
 ROD M5 69 71 4. TO 75 77 BY 2 2 /
 **2 0 0 100 100 0. 0 100 100 0 0 /
 **1 0 **3 0. 0 **5 /
 ROD M5 77 79 2.37 TO 87 89 BY 2 2 /
 **2 0 0 100 100 0. 0 100 100 0 0 /
 **1 0 **3 0. 0 **5 /
 SPLATE M5 1 3 203 201 .04 TO 25 27 227 225 BY 2 **3 /
 SPLATE M5 201 203 103 101 .04 TO 225 227 127 125 ** /
 SPLATE M5 27 29 229 227 .06 TO 43 45 245 243 ** /
 SPLATE M5 227 229 129 127 .06 TO 243 245 145 143 ** /
 SPLATE M5 45 47 247 245 .08 TO 67 69 269 267 ** /
 SPLATE M5 245 247 147 145 .08 TO 267 269 169 167 ** /
 SPLATE M5 69 71 271 269 .06 TO 75 77 277 275 ** /
 SPLATE M5 269 271 171 169 .06 TO 275 277 177 175 ** /
 SPLATE M5 77 79 279 277 .04 TO 87 89 289 287 ** /
 SPLATE M5 277 279 179 177 .04 TO 287 289 189 187 ** /
 */ BODY FRAMES /
 BEAM M5 1 201 3. 0. 0. 50. 50. 50. TO 27 227 BY 2 2 /
 **1 0 0 100 0 0. **5 0 100 0 **3 /
 BEAM M5 29 229 4.5 0. 0. 50. 50. 50. TO 45 245 BY 2 2 /
 **1 0 0 100 0 0. **5 0 100 0 **3 /
 BEAM M5 47 247 6. 0. 0. 50. 50. 50. TO 69 269 BY 2 2 /
 **1 0 0 100 0 0. **5 0 100 0 **3 /
 BEAM M5 71 271 4.5 0. 0. 50. 50. 50. TO 77 277 BY 2 2 /
 **1 0 0 100 0 0. **5 0 100 0 **3 /
 BEAM M5 79 279 3. 0. 0. 50. 50. 50. TO 89 289 BY 2 2 /
 **1 0 0 100 0 0. **5 0 100 0 **3 /
 BEAM 9 209 14.0 0. 0. 75. 75. 75. /
 **1 0 100 0 0. **5 /
 BEAM 27 227 14.0 0. 0. 75. 75. 75. /
 **1 0 100 0 0. **5 /
 BEAM 45 245 62. 0. 0. 450. 450. 450. /
 **1 0 100 0 0. **5 /
 BEAM 55 255 62. 0. 0. 450. 450. 450. /
 **1 0 100 0 0. **5 /
 BEAM 63 263 62. 0. 0. 450. 450. 450. /
 **1 0 100 0 0. **5 /
 BEAM 79 279 14. 0. 0. 75. 75. 75. /
 **1 0 100 0 0. **5 /
 BEAM 85 285 14. 0. 0. 75. 75. 75. /
 **1 0 100 0 0. **5 /

```

*/ ATTACHMENT OF WING FIN /
BEAM 25 656 1156 663 1. 0. 0. .1 .1 .1 /
BEAM 25 658 1158 663 1. 0. 0. .1 .1 .1 /
BEAM 25 661 1161 663 1. 0. 0. .1 .1 .1 /
BEAM 25 663 1163 661 1. 0. 0. .1 .1 .1 /
BEAM 25 656 658 10. 0. 0. 100. 100. 100. /
BEAM 25 658 661 10. 0. 0. 100. 100. 100. /
BEAM 25 661 663 10. 0. 0. 100. 100. 100. /
BEAM 25 89 289 0. 0. 0. 10000. **2 /
BEAM 25 189 289 ** /
END ELEMENT DATA /
END STIFFNESS DATA /
BEGIN BC DATA /
*/ORDER BODY,FIN,WING-FIN,WING HORIZONTAL TAIL /
STAGE 1 /
RETAIN TZ FOR 3 9 15 23 31 39 45 53 61 67 75 83 87 85 103 1087 /
RETAIN TZ TY FOR 1156 1356 1358 1158 1161 1361 1363 1163 /
RETAIN TZ FOR 223 331 231 337 237 245 355 255 363 263 /
267 543 345 551 349 555 563 656 659 663 /
760 761 763 359 559 661 762 279 979 981 /
281 283 983 985 285 /
SUPPORT TX TZ RY FOR 89 /
SUPPORT ASYM IN SURFACE 2 THROUGH 1 /
STAGE 2 /
RETAIN TY TZ FOR 3 9 15 23 31 39 45 53 61 67 75 83 87 /
RETAIN TZ TY FOR 85 1085 1087 /
RETAIN TZ TY FOR 1156 1356 1358 1158 1161 1361 1363 1163 /
RETAIN TZ FOR 223 331 231 337 237 245 355 255 363 263 /
267 543 345 551 349 555 563 656 659 663 /
760 761 763 359 559 661 762 279 979 981 /
281 283 983 985 285 /
SUPPORT TX TY TZ RX RY RZ FOR 89 /
SUPPORT SYMM IN SURFACE 2 THROUGH 1 /
END BC DATA /
BEGIN MASS DATA /
BEGIN CONDITION DATA /
STAGE 1 CONDITION 1 0 0 1 /
END CONDITION DATA /
BEGIN MASS ELEMENT DATA /
PLATE F2 B-1 6001 6002 6022 3495. /
PLATE F2 B-2 6002 6003 6023 6022 5955. /
PLATE F2 B-3 6003 6004 6024 6023 2589. /
PLATE F2 B-4 6004 6005 6025 6024 3440. /
PLATE F2 B-5 6005 6006 6026 6025 5420. /
PLATE F2 B-6 6006 6007 6027 6026 3280. /
PLATE F2 B-7 6007 6008 6028 6027 3306. /
PLATE F2 B-8 6008 6009 6029 6028 4346. /
PLATE F2 B-9 6009 6010 6030 6029 4507. /
PLATE F2 B-10 6010 6011 6031 6030 4486. /
PLATE F2 B-11 6011 6012 6032 6031 3619. /
PLATE F2 B-12 6012 6013 6033 6032 4730. /
PLATE F2 B-13 6013 6014 6034 6033 3982. /
PLATE F2 B-14 6014 6015 6035 6034 947. /
PLATE F2 B-15 6015 6016 6036 6035 1788. /
PLATE F2 W-1 6100 6101 6121 6120 768. /
PLATE F2 W-2 6101 6102 6122 6121 1151. /
PLATE F2 W-3 6102 6103 6123 6122 1667. /
PLATE F2 W-4 6103 6104 6124 6123 1112. /
PLATE F2 W-5 6104 6105 6125 6124 1190. /
PLATE F2 W-6 6105 6106 6126 6125 1659. /
PLATE F2 W-7 6106 6107 6127 6126 1988. /
PLATE F2 W-8 6107 6108 6128 6127 2467. /
PLATE F2 W-9 6108 6109 6129 6128 1335. /
PLATE F2 W-10 6109 6110 6130 6129 338. /
PLATE F2 W-11 6120 6121 6141 6140 795. /
PLATE F2 W-12 6121 6122 6142 6141 1415. /
PLATE F2 W-13 6122 6123 6143 6142 813. /
PLATE F2 W-14 6123 6124 6144 6143 1259. /
PLATE F2 W-15 6124 6125 6145 6144 1248. /
PLATE F2 W-16 6125 6126 6146 6145 1720. /
PLATE F2 W-17 6126 6127 6147 6146 1494. /
PLATE F2 W-18 6127 6128 6148 6147 1888. /
PLATE F2 W-19 6128 6129 6149 6148 498. /

```

PLATE F2 W-20	6129	6130	6150	6149	126.	/
PLATE F2 W-21	6140	6141	6161	6160	508.	/
PLATE F2 W-22	6141	6142	6162	6161	1279.	/
PLATE F2 W-23	6142	6143	6163	6162	536.	/
PLATE F2 W-24	6143	6144	6164	6163	532.	/
PLATE F2 W-25	6144	6145	6165	6164	550.	/
PLATE F2 W-26	6145	6146	6166	6165	1055.	/
PLATE F2 W-27	6146	6147	6167	6166	1405.	/
PLATE F2 W-28	6147	6148	6168	6167	1953.	/
PLATE F2 W-29	6148	6149	6169	6168	274.	/
PLATE F2 W-30	6149	6150	6170	6169	172.	/
PLATE F2 W-31	6180	6181	6201	6200	614.	/
PLATE F2 W-32	6181	6182	6202	6201	1286.	/
PLATE F2 W-33	6182	6183	6203	6202	562.	/
PLATE F2 W-34	6183	6184	6204	6203	786.	/
PLATE F2 W-35	6184	6185	6205	6204	1386.	/
PLATE F2 W-36	6185	6186	6206	6205	1849.	/
PLATE F2 W-37	6186	6187	6207	6206	1649.	/
PLATE F2 W-38	6187	6188	6208	6207	421.	/
PLATE F2 W-39	6188	6189	6209	6208	255.	/
PLATE F2 W-40	6200	6201	6221	6220	207.	/
PLATE F2 W-41	6201	6202	6222	6221	497.	/
PLATE F2 W-42	6202	6203	6223	6222	692.	/
PLATE F2 W-43	6203	6204	6224	6223	765.	/
PLATE F2 W-44	6204	6205	6225	6224	816.	/
PLATE F2 W-45	6205	6206	6226	6225	843.	/
PLATE F2 W-46	6206	6207	6227	6226	687.	/
PLATE F2 W-47	6207	6208	6228	6227	136.	/
PLATE F2 W-48	6208	6209	6229	6228	94.	/
PLATE F2 W-49	6220	6221	6241	6240	136.	/
PLATE F2 W-50	6221	6222	6242	6241	522.	/
PLATE F2 W-51	6222	6223	6243	6242	516.	/
PLATE F2 W-52	6223	6224	6244	6243	536.	/
PLATE F2 W-53	6224	6225	6245	6244	555.	/
PLATE F2 W-54	6225	6226	6246	6245	580.	/
PLATE F2 W-55	6226	6227	6247	6246	704.	/
PLATE F2 W-56	6227	6228	6248	6247	119.	/
PLATE F2 W-57	6228	6229	6249	6248	91.	/
PLATE F2 W-58	6260	6261	6281	6280	289.	/
PLATE F2 W-59	6261	6262	6282	6281	306.	/
PLATE F2 W-60	6262	6263	6283	6282	244.	/
PLATE F2 W-61	6263	6264	6284	6283	507.	/
PLATE F2 W-62	6264	6265	6285	6284	116.	/
PLATE F2 W-63	626	6266	6286	6285	76.	/
PLATE F2 W-64	6280	6281	6301	6300	216.	/
PLATE F2 W-65	6281	6282	6302	6301	144.	/
PLATE F2 W-66	6282	6283	6303	6302	245.	/
PLATE F2 W-67	6283	6284	6304	6303	365.	/
PLATE F2 W-68	6284	6285	6305	6304	86.	/
PLATE F2 W-69	6285	6286	6306	6305	71.	/
PLATE F2 W-70	6300	6301	6321	6320	184.	/
PLATE F2 W-71	6301	6302	6322	6321	160.	/
PLATE F2 W-72	6302	6303	6323	6322	126.	/
PLATE F2 W-73	6303	6304	6324	6323	273.	/
PLATE F2 W-74	6304	6305	6325	6324	66.	/
PLATE F2 W-75	6305	6306	6326	6325	66.	/
PLATE F2 HT-1	6400	6401	6411	6410	283.	/
PLATE F2 HT-2	6401	6402	6412	6411	212.	/
PLATE F2 HT-3	6402	6403	6413	6412	522.	/

*/ PLATES REPRESENTING FUEL

PLATE F2 F-1	6102	6103	6123	6122	129.6	/
PLATE F2 F-2	6103	6104	6124	6123	8637.2	/
PLATE F2 F-3	6104	6105	6125	6124	12852.9	/
PLATE F2 F-4	6106	6107	6127	6126	5531.1	/
PLATE F2 F-5	6107	6108	6128	6127	6919.3	/
PLATE F2 F-6	6108	6109	6129	6128	107.1	/
PLATE F2 F-7	6124	6125	6145	6144	442.8	/
PLATE F2 F-8	6125	6126	6146	6145	5450.7	/
PLATE F2 F-9	6126	6127	6147	6146	6537.8	/
PLATE F2 F-10	6128	6129	6149	6148	2604.5	/
PLATE F2 F-11	6129	6130	6150	6149	4011.2	/
PLATE F2 F-12	6140	6141	6161	6160	762.0	/
PLATE F2 F-13	6144	6145	6165	6164	128.9	/

PLATE F2 F-14	6145	6146	6166	6165	2470.2	/
PLATE F2 F-15	6147	6148	6168	6167	1825.8	/
PLATE F2 F-16	6148	6149	6169	6168	4994.1	/
PLATE F2 F-17	6149	6150	6170	6169	2341.4	/
PLATE F2 F-18	6180	6181	6201	6200	3598.6	/
PLATE F2 F-19	6184	6185	6205	6204	268.5	/
PLATE F2 F-20	6185	6186	6206	6205	1691.6	/
PLATE F2 F-21	6186	6187	6207	6206	3248.9	/
PLATE F2 F-22	6187	6188	6208	6207	2531.0	/
PLATE F2 F-23	6188	6189	6209	6208	4235.0	/
PLATE F2 F-24	6200	6201	6221	6220	775.4	/
PLATE F2 F-25	6204	6205	6225	6224	457.0	/
PLATE F2 F-26	6205	6206	6226	6225	1190.8	/
PLATE F2 F-27	6206	6207	6227	6226	1393.2	/
PLATE F2 F-28	6207	6208	6228	6227	1501.2	/
PLATE F2 F-29	6208	6209	6229	6228	1555.2	/
PLATE F2 F-30	6220	6221	6241	6240	140.4	/
PLATE F2 F-31	6224	6225	6245	6244	54.0	/
PLATE F2 F-32	6225	6226	6246	6245	442.8	/
PLATE F2 F-33	6226	6227	6247	6246	658.8	/
PLATE F2 F-34	6227	6228	6248	6247	648.0	/
PLATE F2 F-35	6228	6229	6249	6248	503.2	/
*/ PLATES REPRESENTING PAYLOAD						
PLATE F2 P-1	6002	6003	6023	6022	680.	/
PLATE F2 P-2	6003	6004	6024	6023	2295.	/
PLATE F2 P-3	6004	6005	6025	6024	3585.	/
PLATE F2 P-4	6005	6006	6026	6025	2200.	/
PLATE F2 P-5	6006	6007	6027	6026	3390.	/
PLATE F2 P-6	6007	6008	6028	6027	3475.	/
PLATE F2 P-7	6008	6009	6029	6028	2965.	/
PLATE F2 P-8	6009	6010	6030	6029	2040.	/
PLATE F2 P-9	6010	6011	6031	6030	2125.	/
PLATE F2 P-10	6011	6012	6032	6031	2125.	/
PLATE F2 P-11	6012	6013	6033	6032	1190.	/
END MASS ELEMENT DATA						
BEGIN CONCENTRATED MASS DATA 1						
1156	125.					/
1356	100.					/
1358	100.					/
1158	125.					/
1161	125.					/
1361	100.					/
1363	100.					/
1163	125.					/
85	150.					/
87	150.					/
1085	150.					/
1087	150.					/
END CONCENTRATED MASS DATA 1						
BEGIN LUMPING DATA						
LUMP MASS SUBSETS 1 AT NODE SUBSET 1						
**2 0	0	0 1	0	0	0 1	/
END LUMPING DATA						
BEGIN FACTOR DATA						
MASS FACTOR 32.17						
EXCLUDE STIFFNESS ELEMENTS						
END FACTOR DATA						
END MASS DATA						
BEGIN SUBSET DEFINITION						
SUBSETS OF NODAL SET 1						
N1 = 3 TO 87						
N2 = 223 TO 267 331 TO 763						
N3 = 279 281 283 285 979 981 983 935						
N5 = ALL						
N6 = 6000 TO 6499						
EXCLUDE N6 FROM N5						
N10 = 6000 TO 6099						
N11 = 6100 TO 6399						
N12 = 6400 TO 6499						
SUBSETS OF STIFFNESS SET 1						
E1 = ALL						

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SUBSETS OF MASS SET 1 /
E1 = IN N10 /
E2 = IN N11 /
E3 = IN N12 /
E4 = ALL /
END SUBSET DEFINITION /
END PROBLEM DATA /
BEGIN SLENDER BODY DATA /
0. 0. 1 1 1 13 1 2 Y 2 /
END DATA /
BEGIN VERTICAL THIN BODY DATA /
0. 0. 0. 1.570796 14 14 1 3 1 14 2 Y 2 /
BEGIN PANEL DEFINITION DATA /
1 2 2 2 3 2 0 0 /
END DATA /
BEGIN VERTICAL THIN BODY DATA /
0. 594. 0. 1.570796 17 17 0 8 3 17 2 Y 2 /
BEGIN PANEL DEFINITION DATA /
5 3 6 3 7 3 8 3 /
4 3 3 3 6 3 5 3 /
1 3 2 3 3 3 4 3 /
END DATA /
BEGIN HORIZONTAL THIN BODY DATA /
0. 0. 0. 0. 33 33 0 27 19 33 1 2 /
BEGIN PANEL DEFINITION DATA /
1 4 2 4 3 4 0 0 /
3 4 2 4 4 4 5 4 /
5 4 4 4 13 4 6 4 /
6 4 13 4 15 4 3 4 /
8 4 15 4 7 4 0 0 /
8 4 7 4 24 4 0 0 /
8 4 24 4 9 4 10 4 /
10 4 9 4 11 4 0 0 /
4 4 12 4 13 4 0 0 /
13 4 12 4 14 4 15 4 /
15 4 14 4 16 4 7 4 /
7 4 16 4 25 4 24 4 /
24 4 25 4 17 4 9 4 /
14 4 18 4 19 4 16 4 /
16 4 19 4 26 4 25 4 /
25 4 26 4 20 4 17 4 /
19 4 21 4 22 4 19 4 /
19 4 22 4 27 4 26 4 /
26 4 27 4 23 4 20 4 /
END DATA /
BEGIN HORIZONTAL THIN BODY DATA /
0. 0. 0. 0. 60 60 0 8 3 60 1 2 /
BEGIN PANEL DEFINITION DATA /
1 5 2 5 3 5 4 5 /
4 5 3 5 6 5 5 5 /
5 5 6 5 7 5 8 5 /
END DATA /
END FLEXSTAB DATA /

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*/ MOCE2 /
BEGIN NODAL DATA
1 20. 0. 1. TO 9 340. 0. 65. 8Y 2
101 20. 0. -1. TO 109 340. 0. -65. 8Y 2
201 20. 1. 0. TO 209 340. 65. 0. 8Y 2
11 420. 0. 65. TO 83 3300. 0. 65. 8Y 2
111 420. 0. -65. TO 189 3540. 0. -65. 8Y 2
211 420. 65. 0. TO 225 980. 65. 0. 8Y 2
265 2580. 65. 0. TO 277 3060. 65. 0. 8Y 2
287 3460. 65. 0. TO 289 3540. 65. 0. 8Y 2
*/ WING COORDINATES
227 1060. 65. 0. 26.25 TO 245 1780. 65. 0. 36.35 8Y 2
245 TO 255 2180. 65. 0. 28.8 8Y 2
255 TO 263 2500. 65. 0. 12.0 3Y 2
327 1060. 65. 0. 26.25 TO 341 1620. 265. 0. 8.85 8Y 2
445 1780. 195. 0. 22.65 TO 455 2180. 195. 0. 20.15 8Y 2
541 1620. 265. 0. 8.85 TO 551 2205. 455. 0. 5.75 8Y 2
651 2205. 455. 0. 5.75 TO 656 2545. 594. 0. 3.2
756 2545. 594. 0. 3.2 TO 760 2875. 765. 0. .95
760 TO 763 2995. 765. 0. 1.85
341 TO 355 2180. 255. 0. 20.15 8Y 2
355 TO 363 25 0. 265. 0. 11.25 8Y 2
551 TO 559 2525. 455. 0. 10.0
559 TO 563 2685. 455. 0. 5.0
656 TO 659 2665. 594. 0. 4.85
659 TO 663 2825. 594. 0. 2.45
*/ HORIZONTAL TAIL
279 3140. 65. 0. 1.80
779 3140. 65. 0. 1.80 TO 979 3365. 200. 0. 1.25 8Y 100
281 3220. 65. 0. 4.25
731 3220. 65. 0. 4.25 TO 981 3388. 200. 0. 1.75 8Y 100
283 3300. 65. 0. 4.55
783 3300. 65. 0. 4.55 TO 983 3412. 200. 0. 1.80 8Y 100
285 3380. 65. 0. 1.40
785 3380. 65. 0. 1.40 TO 985 3435. 200. 0. .80 8Y 100
*/ VERTICAL TAIL
REC REC1 0. 0. 0. 1. 0. 0. -1. 0.
95 3380. 65. 0. 3.25
37 3460. 65. 0. 2.47
1085 3460. 140. 0. 1.50
1087 3500. 140. 0. 1.80
*/ WING FIN
1150 2545. .1 -594. 2.40 TO 1356 2830. 100. -594. 1.80 8Y 100
1153 2625. .1 -594. 2.40 TO 1358 2942. 100. -594. 1.90 8Y 100
1161 2745. .1 -594. 2.80 TO 1361 2859. 100. -594. 1.95 8Y 100
1163 2825. .1 -594. 2.80 TO 1363 2970. 100. -594. 2.05 8Y 100
RESUME GLOBAL
89 3540. 0. 65.
*/ AIRLOAD PANEL NODES
*/ BODY
5100 0. 0. 0. TO 5112 3564. 0. 0.
5251 0. 26.1279 C.
5252 297. 26.1279 C.
5253 297. 63.5215 C.
5254 594. 63.5215 C.
5202 594. 65.1 C. TO 5212 3564. 65.1 0.
*/ WING
5400 741. 65.1 0. TO 5405 2715. 65.1 0.
5410 1017.7530 146.6 0. TO 5415 2705.9945 146.6 0.
5420 1294.1665 228. 0. TO 5425 2697. 228. 0.
5430 1677.8854 341. 0. TO 5435 2722.8855 341. 0.
5440 2065. 455. 0. TO 5445 2749. 455. 0.
5450 2487. 594. 0. TO 5455 2874.059 594. 0.
5460 2689.47 696. 0. TO 5465 2965.8239 696. 0.
5470 2884. 794. 0. TO 5475 3054. 794. 0.
*/ HOR TAIL
5500 3124. 65.1 0. TO 5502 3417. 65.1 0.
5510 3255.0804 146.6 0. TO 5512 3440.5144 146.6 0.
5520 3386. 228. 0. TO 5522 3464. 228. 0.
*/ VERT WING FIN
5313 2487. 594. 0. TO 5315 2880. 594. 134.
5316 2680.5 594. 0. TO 5318 2910. 594. 134.
5319 2874.059 594. 0. TO 5321 2940. 594. 134.

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*/ WEIGHT PANELS - BODY
6001 0. 0. 0. TO 6016 3564. C. 0.
6021 0. 65. 0. TO 6036 3564. 65. 0.
*/ WEIGHT PANELS - WING
6100 741.0 65.0 C. TO 6220 2487.0 594.0 0. BY 20
6100 TO 6260 2487.0 594.0 0. BY 20
6180 TO 6240 2487.0 594.0 0. BY 20
6260 TO 6320 2884.0 794.0 0. BY 20
6110 2715.0 65.0 0. TO 6170 2715.0 329.5 0. BY 20
6189 2715.0 329.5 0. TO 6249 2874.0 594.0 0. BY 20
6266 2874.0 594.0 C. TO 6326 3054.0 794.0 0. BY 20
6100 TO 6110
*+3 20 0 20
6180 TO 6189
*+3 20 0 20
6260 TO 6266
*+3 20 0 20
*/ WEIGHT PANELS - HOR TAIL
6400 3124. 65.1 0. TO 6403 3417. 65.1 0.
6410 3386. 228.0 0. TO 6413 3464. 228.0 0.
*/ WEIGHT PANELS - VERT FIN
6501 3374.6 C. 92.8
6502 3472. C. 92.8
6503 3458.7 0. 149.8
6504 3514.6 0. 149.8
*/ WEIGHT PANELS - WING VERT FIN
6601 2487. 594. 0. TO 6603 2880. 594. 134.
6604 2874.050 594. 0. TO 6606 2940. 594. 134.
END NODAL DATA
BEGIN STIFFNESS DATA
BEGIN ELEMENT DATA
*/ WING SPARS
SPAR M5 227 329 .06 1.
SPAR M5 247 447 .10 2.0 TO 253 453 BY 2 2
SPAR M5 329 331 .06 1. TO 339 341 BY 2 2
SPAR M5 341 543 .06 1.
SPAR M5 543 545 .06 1. TO 549 551 BY 2 2
SPAR M5 551 653 .06 1.
SPAR M5 653 655 .06 1.
SPAR M5 655 656 .06 1.
SPAR M5 656 757 .06 1.
SPAR M5 757 758 .06 1. TO 759 760
SPAR M5 762 363 .20 6.
SPAR M5 362 563 .17 0.
SPAR M5 563 663 .15 4.
SPAR M5 662 763 .15 2.
SPAR M5 229 329 .1 1. TO 243 343 BY 2 2
SPAR M5 245 445 .18 1.
SPAR M5 445 345 .18 1.
SPAR M5 447 347 .1 2. TO 453 353 BY 2 2
SPAR M5 255 455 .3 6.
SPAR M5 455 353 .3 6.
SPAR M5 257 357 .12 6. TO 261 361 BY 2 2
SPAR M5 343 543 .1 1. TO 345 545 BY 2 2
SPAR M5 347 547 .1 2. TO 353 553 BY 2 2
SPAR M5 355 555 .1 4.
SPAR M5 357 557 .1 5. TO 361 561 BY 2 2
SPAR M5 553 653 .06 2. TO 555 655 BY 2 2
SPAR M5 556 656 .03 2. TO 562 662
SPAR M5 657 757 .03 1. TO 662 762
*/ WING RIBS
SPAR M5 445 447 .17 2. TO 453 455 BY 2 2
SPAR M5 341 343 .10 1.5 TO 361 363 BY 2 2
SPAR M5 551 553 .10 2. TO 553 555 BY 2 2
SPAR M5 555 556 .10 2. TO 562 563
SPAR M5 656 657 .06 1. TO 662 663
SPAR M5 760 761 .15 .7 TO 762 763
*/ WING COVERS
COVER M5 229 329 227 .03
COVER M5 229 329 331 231 .03 TO 241 341 343 243 BY 2 *+3
COVER M5 243 343 445 245 .03
COVER M5 445 345 343 .03
COVER M5 245 247 447 445 .06 .0 TO 253 255 455 453 BY 2 *+3

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COVER M5 445 345 347 447 .03 TO 453 353 355 455 BY 2 **3
COVER M5 255 455 357 257 .05 .07
COVER M5 455 355 357 .05 .07
COVER M5 257 357 359 259 .05 .07
COVER M5 259 359 361 261 .13 .07 .11 .0 TO 261 361 363 263 BY 2 **3
COVER M5 343 543 341 .03
COVER M5 343 543 545 345 .03 TO 353 553 555 355 BY 2 **3
COVER M5 355 555 557 357 .05 .04 TO 357 557 559 359 BY 2 **3
COVER M5 359 559 561 361 .15 .07 .10 .0 TO 361 561 563 363 BY 2 **3
COVER M5 553 653 551 .15 .07 .11 .06
COVER M5 553 653 655 555 .15 .07 .11 .06
COVER M5 555 655 656 556 .15 .07 .11 .06 TO 562 662 663 563
COVER M5 657 757 656 .04
COVER M5 657 757 758 658 .04 TO 662 762 763 663
*/ HORIZONTAL TAIL
SPAR M5 279 879 .05 .6
SPAR M5 879 979 .05 .6
SPAR M5 281 881 .025 .9
SPAR M5 881 981 .025 .9
SPAR M5 283 883 .025 .8
SPAR M5 883 983 .025 .8
SPAR M5 285 885 .10 1.3
SPAR M5 885 985 .10 1.3
SPAR M5 879 881 .05 .6 TO 883 885 BY 2 2
SPAR M5 979 981 .05 .6 TO 983 985 BY 2 2
COVER M5 279 879 881 281 .08
**2 0 0 2 **3 0.
COVER M5 879 979 981 881 .035
**2 0 0 2 **3 0.
*/ WING FIN
SPAR M5 1156 1256 .025 .5 TO 1256 1356 BY 100 100
SPAR M5 1158 1258 .025 .5 TO 1258 1358 BY 100 100
SPAR M5 1161 1261 .025 .5 TO 1261 1361 BY 100 100
SPAR M5 1163 1263 .025 .5 TO 1263 1363 BY 100 100
SPAR M5 1256 1258 .025 .5 TO 1356 1358 BY 100 100
SPAR M5 1259 1261 .025 .5 TO 1356 1361 BY 100 100
SPAR M5 1261 1263 .025 .5 TO 1361 1363 BY 100 100
COVER M5 1156 1256 1258 1158 .025 TO 1256 1356 1358 1258 +
BY 100 100 100 100
COVER M5 1158 1258 1261 1161 .025 TO 1258 1358 1361 1261 +
BY 100 100 100 100
COVER M5 1161 1261 1263 1163 .025 TO 1261 1361 1363 1263 +
BY 100 100 100 100
*/ VERTICAL TAIL
COVER M5 85 1085 1087 87 .0 0.035
SPAR M5 85 1085 0. 0. .5 .0 .0
SPAR M5 87 1087 0. 0. .5 .0 .0
SPAR M5 1085 1087 0. 0. .5 .0 .0
*/ BODY
*/ STRINGERS
ROD M5 1 3 2.37 TO 23 25 BY 2 2
**2 0 0 100 100 0. 0 100 100 0 0 0
**1 0 **3 0. 0 **5
ROD M5 25 27 4. TO 43 45 BY 2 2
**2 0 0 100 100 0. 0 100 100 0 0 0
**1 0 **3 0. 0 **5
ROD M5 45 47 5.35 TO 67 69 BY 2 2
**2 0 0 100 100 0. 0 100 100 0 0 0
**1 0 **3 0. 0 **5
ROD M5 69 71 4. TO 75 77 BY 2 2
**2 0 0 100 100 0. 0 100 100 0 0 0
**1 0 **3 0. 0 **5
ROD M5 77 79 2.37 TO 87 89 BY 2 2
**2 0 0 100 100 0. 0 100 100 0 0 0
**1 0 **3 0. 0 **5
SPLATE M5 1 3 203 201 .04 TO 25 27 227 225 BY 2 **3
SPLATE M5 201 203 103 101 .04 TO 225 227 127 125 **
SPLATE M5 27 29 229 227 .06 TO 43 45 245 243 **
SPLATE M5 227 229 129 127 .06 TO 243 245 145 143 **
SPLATE M5 45 47 247 245 .08 TO 67 69 269 267 **
SPLATE M5 245 247 147 145 .08 TO 267 269 169 167 **
SPLATE M5 69 71 271 269 .06 TO 75 77 277 275 **

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SPLATE M5 269 271 171 169 .06 TO 275 277 177 175 **
SPLATE M5 77 79 279 277 .04 TO 87 89 289 287 **
SPLATE M5 277 279 179 177 .04 TO 287 289 189 187 **
*/ BODY FRAMES
BEAM M5 1 201 3. 0. 0. 50. 50. 50. TO 27 227 BY 2 2
**1 0 0 100 0 0. **5 0 100 0 **3
BEAM M5 29 229 4.5 0. 0. 50. 50. 50. TO 45 245 BY 2 2
**1 0 0 100 0 0. **5 0 100 0 **3
BEAM M5 47 247 6. 0. 0. 50. 50. 50. TO 69 269 BY 2 2
**1 0 0 100 0 0. **5 0 100 0 **3
BEAM M5 71 271 4.5 0. 0. 50. 50. 50. TO 77 277 BY 2 2
**1 0 0 100 0 0. **5 0 100 0 **3
BEAM M5 79 279 3. 0. 0. 50. 50. 50. TO 89 289 BY 2 2
**1 0 0 100 0 0. **5 0 100 0 **3
BEAM 9 209 14. 0. 0. 75. 75. 75.
**1 0 100 0 0. **5
BEAM 27 227 14. 0. 0. 75. 75. 75.
**1 0 100 0 0. **5
BEAM 45 245 62. 0. 0. 450. 450. 450.
**1 0 100 0 0. **5
BEAM 55 255 62. 0. 0. 450. 450. 450.
**1 0 100 0 0. **5
BEAM 63 263 62. 0. 0. 450. 450. 450.
**1 0 100 0 0. **5
BEAM 79 279 14. 0. 0. 75. 75. 75.
**1 0 100 0 0. **5
BEAM 85 285 14. 0. 0. 75. 75. 75.
**1 0 100 0 0. **5
*/ ATTACHMENT OF WING FIN
BEAM Z5 656 1156 663 1. 0. 0. .1 .1 .1
BEAM Z5 658 1158 663 1. 0. 0. .1 .1 .1
BEAM Z5 661 1161 663 1. 0. 0. .1 .1 .1
BEAM Z5 663 1163 661 1. 0. 0. .1 .1 .1
BEAM Z5 656 658 10. 0. 0. 100. 100. 100.
BEAM Z5 658 661 10. 0. 0. 100. 100. 100.
BEAM Z5 661 663 10. 0. 0. 100. 100. 100.
BEAM Z5 89 289 0. 0. 0. 10000. **2
BEAM Z5 189 289 **
END ELEMENT DATA
END STIFFNESS DATA
BEGIN BC DATA
*/ORDER BODY,FIN,WING-FIN,WING HORIZONTAL TAIL
STAGE 1
RETAIN TZ FOR 3 9 15 23 31 39 45 53 61 67 75 83 87 95 105 1087
RETAIN TZ TY FOR 1156 1356 1358 1158 1161 1361 1363 1163
RETAIN TZ FOR 223 331 231 337 237 245 355 255 363 263 +
267 543 345 551 349 555 563 656 659 663 +
760 761 763 359 559 661 762 279 979 981 +
281 283 983 985 285
SUPPORT TX TZ RY FOR 39
SUPPORT ASYM IN SURFACE 2 THROUGH 1
END BC DATA
BEGIN LOAD DATA
STAGE 1
READ NODAL LOADS FROM DATARF WITH INDEX QSYMM**
END LOAD DATA
BEGIN MASS DATA
BEGIN CONDITION DATA
PANEL DATA 1 CONDITION 1
END CONDITION DATA
BEGIN MASS ELEMENT DATA
PLATE F2 8-1 6001 6002 6022 3495.
PLATE F2 8-2 6002 6003 6023 6022 5955.
PLATE F2 8-3 6003 6004 6024 6023 2589.
PLATE F2 8-4 6004 6005 6025 6024 3440.
PLATE F2 8-5 6005 6006 6026 6025 5420.
PLATE F2 8-6 6006 6007 6027 6026 3280.
PLATE F2 8-7 6007 6008 6028 6027 3306.
PLATE F2 8-8 6008 6009 6029 6028 4346.
PLATE F2 8-9 6009 6010 6030 6029 4507.
PLATE F2 8-10 6010 6011 6031 6030 4486.
PLATE F2 8-11 6011 6012 6032 6031 3619.
PLATE F2 8-12 6012 6013 6033 6032 4730.

```

PLATE F2	B-13	6013	6014	6034	6033	3982.
PLATE F2	B-14	6014	6015	6035	6034	947.
PLATE F2	B-15	6015	6016	6036	6035	1788.
PLATE F2	VT-1	6501	6502	6504	6503	600.
PLATE F2	W-1	6100	6101	6121	6120	768.
PLATE F2	W-2	6101	6102	6122	6121	1151.
PLATE F2	W-3	6102	6103	6123	6122	1667.
PLATE F2	W-4	6103	6104	6124	6123	1112.
PLATE F2	W-5	6104	6105	6125	6124	1190.
PLATE F2	W-6	6105	6106	6126	6125	1659.
PLATE F2	W-7	6106	6107	6127	6126	1988.
PLATE F2	W-8	6107	6108	6128	6127	2467.
PLATE F2	W-9	6108	6109	6129	6128	1335.
PLATE F2	W-10	6109	6110	6130	6129	338.
PLATE F2	W-11	6120	6121	6141	6140	795.
PLATE F2	W-12	6121	6122	6142	6141	1415.
PLATE F2	W-13	6122	6123	6143	6142	813.
PLATE F2	W-14	6123	6124	6144	6143	1259.
PLATE F2	W-15	6124	6125	6145	6144	1248.
PLATE F2	W-16	6125	6126	6146	6145	1720.
PLATE F2	W-17	6126	6127	6147	6146	1494.
PLATE F2	W-18	6127	6128	6148	6147	1888.
PLATE F2	W-19	6128	6129	6149	6148	498.
PLATE F2	W-20	6129	6130	6150	6149	126.
PLATE F2	W-21	6140	6141	6161	6160	508.
PLATE F2	W-22	6141	6142	6162	6161	1279.
PLATE F2	W-23	6142	6143	6163	6162	536.
PLATE F2	W-24	6143	6144	6164	6163	532.
PLATE F2	W-25	6144	6145	6165	6164	559.
PLATE F2	W-26	6145	6146	6166	6165	1055.
PLATE F2	W-27	6146	6147	6167	6166	1405.
PLATE F2	W-28	6147	6148	6168	6167	1953.
PLATE F2	W-29	6148	6149	6169	6168	274.
PLATE F2	W-30	6149	6150	6170	6169	172.
PLATE F2	W-31	6180	6181	6201	6200	614.
PLATE F2	W-32	6181	6182	6202	6201	1286.
PLATE F2	W-33	6182	6183	6203	6202	562.
PLATE F2	W-34	6183	6184	6204	6203	786.
PLATE F2	W-35	6184	6185	6205	6204	1386.
PLATE F2	W-36	6185	6186	6206	6205	1849.
PLATE F2	W-37	6186	6187	6207	6206	1649.
PLATE F2	W-38	6187	6188	6208	6207	421.
PLATE F2	W-39	6188	6189	6209	6208	255.
PLATE F2	W-40	6200	6201	6221	6220	207.
PLATE F2	W-41	6201	6202	6222	6221	497.
PLATE F2	W-42	6202	6203	6223	6222	692.
PLATE F2	W-43	6203	6204	6224	6223	765.
PLATE F2	W-44	6204	6205	6225	6224	816.
PLATE F2	W-45	6205	6206	6226	6225	843.
PLATE F2	W-46	6206	6207	6227	6226	687.
PLATE F2	W-47	6207	6208	6228	6227	136.
PLATE F2	W-48	6208	6209	6229	6228	94.
PLATE F2	W-49	6220	6221	6241	6240	136.
PLATE F2	W-50	6221	6222	6242	6241	522.
PLATE F2	W-51	6222	6223	6243	6242	516.
PLATE F2	W-52	6223	6224	6244	6243	536.
PLATE F2	W-53	6224	6225	6245	6244	555.
PLATE F2	W-54	6225	6226	6246	6245	580.
PLATE F2	W-55	6226	6227	6247	6246	704.
PLATE F2	W-56	6227	6228	6248	6247	119.
PLATE F2	W-57	6228	6229	6249	6248	91.
PLATE F2	W-58	6260	6261	6281	6280	289.
PLATE F2	W-59	6261	6262	6282	6281	306.
PLATE F2	W-60	6262	6263	6283	6282	244.
PLATE F2	W-61	6263	6264	6284	6283	507.
PLATE F2	W-62	6264	6265	6285	6284	116.
PLATE F2	W-63	6265	6266	6286	6285	76.
PLATE F2	W-64	6280	6281	6301	6300	216.
PLATE F2	W-65	6281	6282	6302	6301	144.
PLATE F2	W-66	6282	6283	6303	6302	245.
PLATE F2	W-67	6283	6284	6304	6303	365.
PLATE F2	W-68	6284	6285	6305	6304	86.
PLATE F2	W-69	6285	6286	6306	6305	71.

PLATE F2	W-70	6300	6301	6321	6320	184.
PLATE F2	W-71	6301	6302	6322	6321	160.
PLATE F2	W-72	6302	6303	6323	6322	126.
PLATE F2	W-73	6303	6304	6324	6323	273.
PLATE F2	W-74	6304	6305	6325	6324	66.
PLATE F2	W-75	6305	6306	6326	6325	66.
PLATE F2	HT-1	6400	6401	6411	6410	283.
PLATE F2	HT-2	6401	6402	6412	6411	212.
PLATE F2	HT-3	6402	6403	6413	6412	522.
PLATE F2	WF-1	6601	6602	6605	6604	500.
PLATE F2	WF-2	6602	6603	6606	6605	400.

*/ PLATES REPRESENTING FUEL

PLATE F2	F-1	6102	6103	6123	6122	129.6
PLATE F2	F-2	6103	6104	6124	6123	8637.2
PLATE F2	F-3	6104	6105	6125	6124	12852.9
PLATE F2	F-4	6106	6107	6127	6126	5531.1
PLATE F2	F-5	6107	6108	6128	6127	6919.3
PLATE F2	F-6	6108	6109	6129	6128	107.1
PLATE F2	F-7	6124	6125	6145	6144	442.8
PLATE F2	F-8	6125	6126	6146	6145	5450.7
PLATE F2	F-9	6126	6127	6147	6146	6537.8
PLATE F2	F-10	6128	6129	6149	6148	2604.5
PLATE F2	F-11	6129	6130	6150	6149	4011.2
PLATE F2	F-12	6140	6141	6161	6160	5762.0
PLATE F2	F-13	6144	6145	6165	6164	1128.9
PLATE F2	F-14	6145	6146	6166	6165	2470.2
PLATE F2	F-15	6147	6148	6168	6167	1825.8
PLATE F2	F-16	6148	6149	6169	6168	4994.1
PLATE F2	F-17	6149	6150	6170	6169	2341.4
PLATE F2	F-18	6180	6181	6201	6200	3598.6
PLATE F2	F-19	6184	6185	6205	6204	258.5
PLATE F2	F-20	6185	6186	6206	6205	1691.6
PLATE F2	F-21	6186	6187	6207	6206	3248.9
PLATE F2	F-22	6187	6188	6208	6207	2531.0
PLATE F2	F-23	6188	6189	6209	6208	4235.0
PLATE F2	F-24	6200	6201	6221	6220	775.4
PLATE F2	F-25	6204	6205	6225	6224	457.0
PLATE F2	F-26	6205	6206	6226	6225	1190.8
PLATE F2	F-27	6206	6207	6227	6226	1393.2
PLATE F2	F-28	6207	6208	6228	6227	1501.2
PLATE F2	F-29	6208	6209	6229	6228	1555.2
PLATE F2	F-30	6220	6221	6241	6240	140.4
PLATE F2	F-31	6224	6225	6245	6244	54.0
PLATE F2	F-32	6225	6226	6246	6245	442.8
PLATE F2	F-33	6226	6227	6247	6246	658.3
PLATE F2	F-34	6227	6228	6248	6247	648.0
PLATE F2	F-35	6228	6229	6249	6248	583.2

*/ PLATES REPRESENTING PAYLOAD

PLATE F2	P-1	6002	6003	6023	6022	680.
PLATE F2	P-2	6003	6004	6024	6023	2295.
PLATE F2	P-3	6004	6005	6025	6024	3585.
PLATE F2	P-4	6005	6006	6026	6025	2200.
PLATE F2	P-5	6006	6007	6027	6026	3390.
PLATE F2	P-6	6007	6008	6028	6027	3475.
PLATE F2	P-7	6008	6009	6029	6028	2965.
PLATE F2	P-8	6009	6010	6030	6029	2040.
PLATE F2	P-9	6010	6011	6031	6030	2125.
PLATE F2	P-10	6011	6012	6032	6031	2125.
PLATE F2	P-11	6012	6013	6033	6032	1190.

END MASS ELEMENT DATA

BEGIN PANEL DATA 1

*/ BODY

MASS SUBSETS 1

DIRECTION Z

1	5100	5251	5252	5101	
2	5101	5253	5254	5102	
3	5202	5203	5103	5102	TO 12

*/ WING FIN

MASS SUBSETS 2

DIRECTION Y

13	5313	5316	5317	5314	
14	5316	5319	5320	5317	
15	5314	5317	5318	5315	
16	5317	5320	5321	5318	

```

*/ WING
  MASS SUBSETS 3
  DIRECTION 2
    17 5400 5401 5411 5410 TO 21
**6   5   10 **3           0   5
*/ HOR TAIL
  MASS SUBSETS 4
  DIRECTION 2
    52 5500 5501 5511 5510 TO 53
**1   2   10 **3           0   2

```

```

END PANEL DATA 1
BEGIN FACTOR DATA
  EXCLUDE STIFFNESS ELEMENTS
  MASS FACTOR 32.17
END FACTOR DATA
END MASS DATA
BEGIN SUBSET DEFINITION
SUBSETS OF MASS SET 1
  N1 = 6001 TO 6036 6501 TO 6504
  E1 = ALL IN N1
  N2 = 6601 TO 6606
  E2 = ALL IN N2
  N3 = 6100 TO 6326
  E3 = ALL IN N3
  N4 = 6400 TO 6413
  E4 = ALL IN N4

```

END SUBSET DEFINITION

END PROBLEM DATA

*/ MODE2 /

BEGIN VAMAT DATA

BODY	12	2	2		
FIN	0	2	8		
WING-FIN	4	3	2		
WING	35	3	3		
HOR-TAIL	4	3	3		
	55	33	1		
	6	1.	20	24	1
	13	16	25	33	1
1.	0.	.00001			
200.	0.	.00001			
400.	0.	.00001			
600.	0.	.00001			
800.	0.	.00001			
1000.	0.	.00001			
1200.	0.	.00001			
1400.	0.	.00001			
1600.	0.	.00001			
1800.	0.	.00001			
2000.	0.	.00001			
3599.	0.	0.			
3400.	0.	0.			
3200.	0.	0.			
3000.	0.	0.			
2800.	0.	0.			
2600.	0.	0.			
2400.	0.	0.			
2200.	0.	0.			
2000.	0.	0.			
2985.	793.	-9999.			
2855.3	696.	-9999.			
2720.	595.	-9999.			
2641.8236	594.	-9999.			
2718.	593.	-9999.			
2600.	525.	-9999.			
2475.4	455.	-9999.			
2390.	398.	-9999.			
2304.9	341.	-9999.			
2220.	285.	-9999.			
2136.	228.	-9999.			
2030.7	146.6	-9999.			
1925.4	65.1	-9999.			

** FORE BODY #
 ** AFT BODY #
 ** OUTBOARD WING #
 ** WING FIN #
 ** INBOARD WING #
 ** HORIZONTAL STABILIZER #

11 20 23 24 33 0
 0 0 0 0 3 0 0 0 0 0 1 2 2 2 2 2 2 2 1 2 2 2 2 2 2 2 2 2 2 2

14
 17 0. 18 0. 19 0. 20 0.
 22 0. 23 0. 24 0. 25 0.
 27 0. 28 0. 29 0. 32 0.
 33 0. 37 0.
 17 51 0.
 52 55 0.

MDC001A
 END VAMAT DATA
 BEGIN VAMSCN DATA

2 2 1
 1
 2 1
 **GROUP 1 - PASS 1#
 1 2
 **GROUP 2 - PASS 1#
 1
 2
 **GROUP 1 - PASS 2#
 1 2
 END VAMSCN DATA

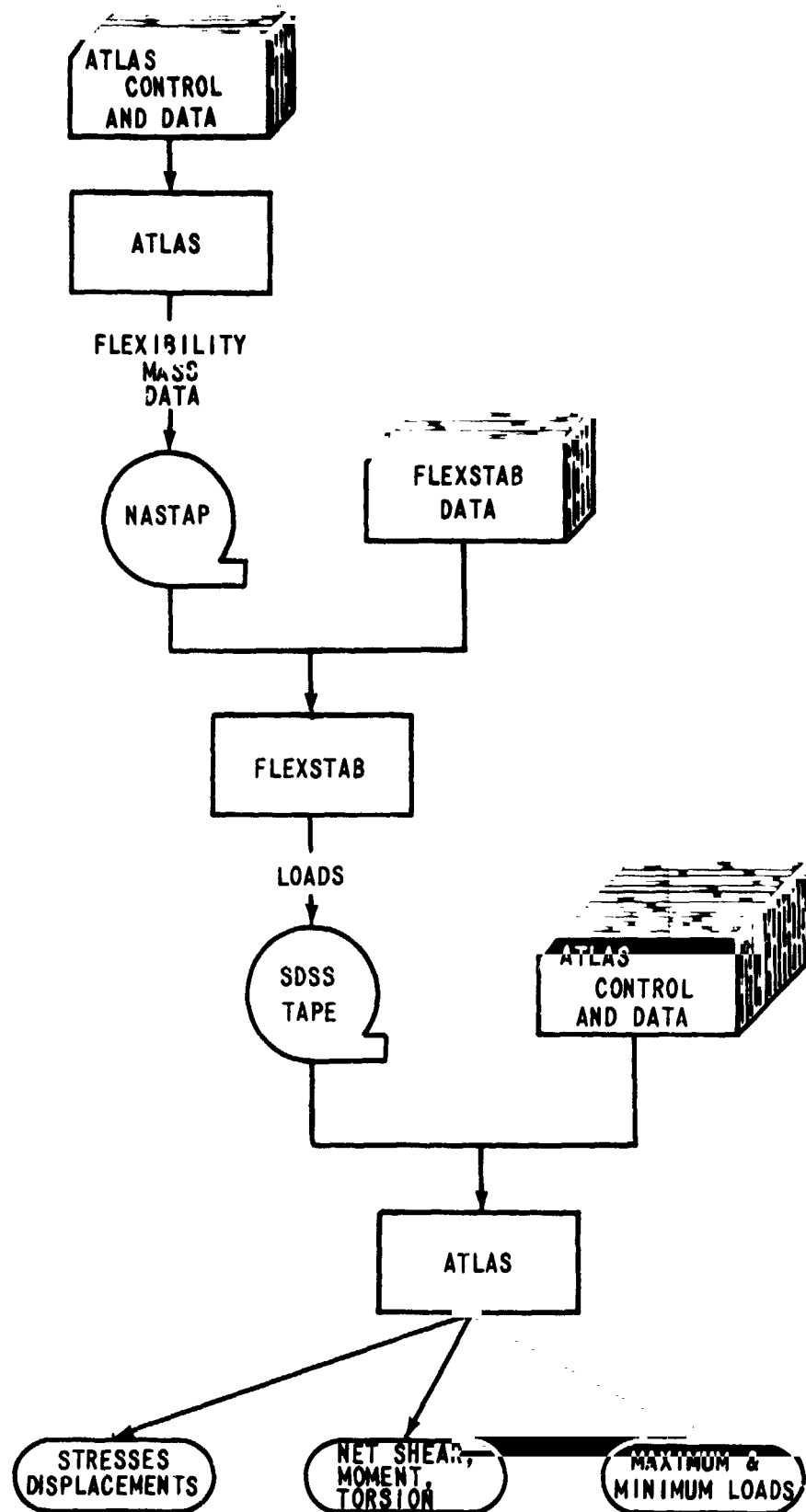


Figure 301-1. Schematic of ATLAS/FLEXSTAB Interface Demonstration

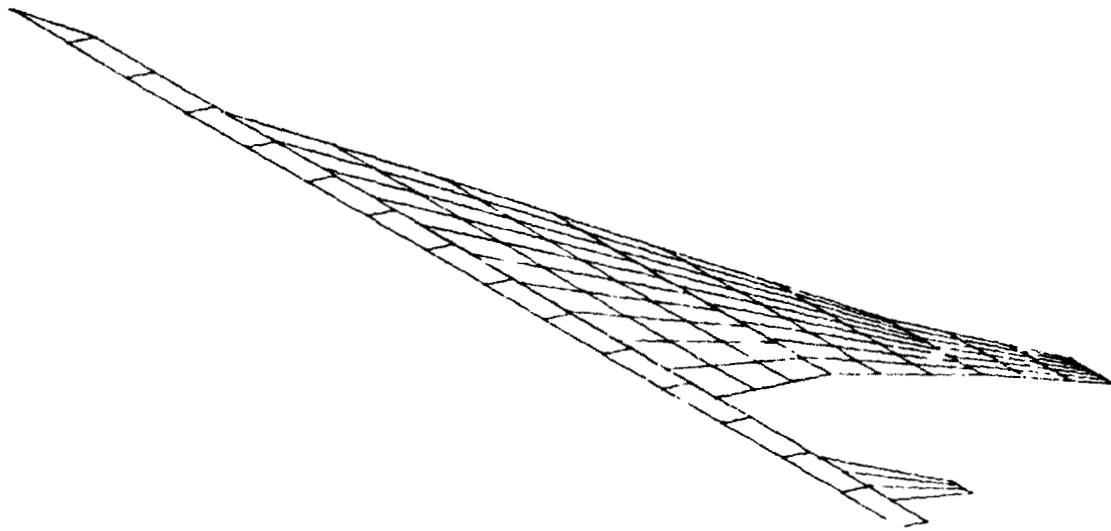


Figure 301-2. Structural Model

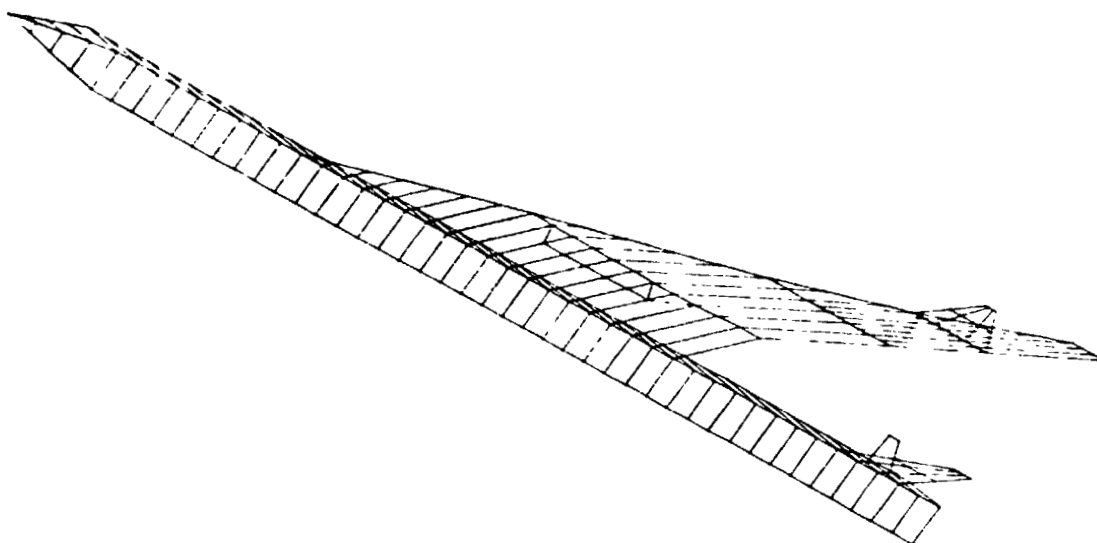


Figure 301-3. Mass Model

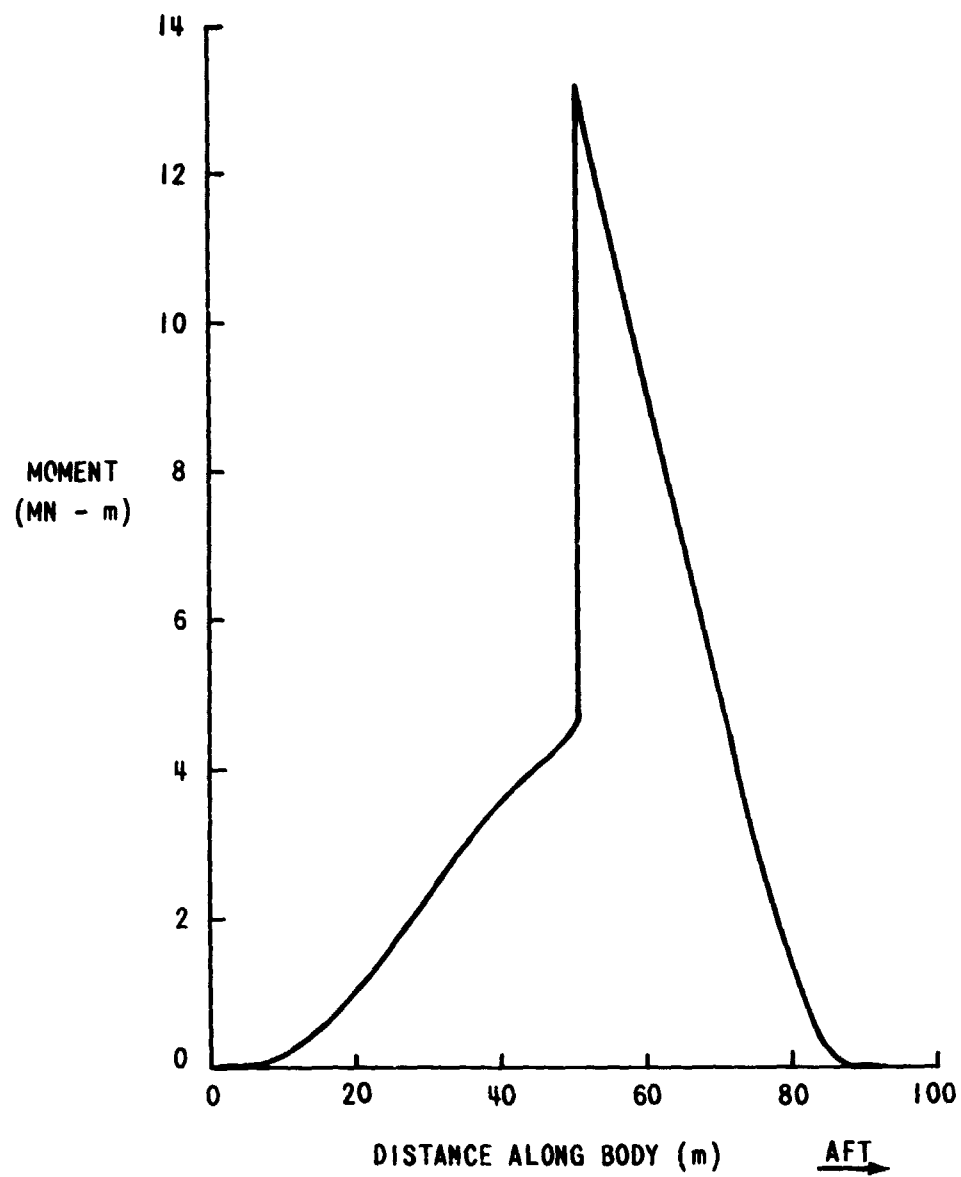


Figure 301-4. Body Bending Moment

302. ATLAS/NASTRAN INTERFACES (DECK 9)

302.1 DESCRIPTION OF DEMONSTRATION

The method used to demonstrate the ATLAS-NASTRAN interfaces is shown schematically in figure 302-1. An ATLAS model consisting of ROD, BEAM, PLATE, SPLATE and GPLATE elements was prepared. Only nodal loads are applied. An ATLAS stress analysis is performed and the data are converted to NASTRAN (ref. 201-1) bulk data. Nonconvertible NASTRAN bulk data cards and the Executive and Case Control decks are added. This complete NASTRAN problem deck is then used to perform a NASTRAN stress analysis.

The complete NASTRAN bulk data deck is then processed through the NASTRAN-to-ATLAS interface. The resulting ATLAS data deck is then used to perform a stress analysis.

302.2 RESULTS

NASTRAN detected no data errors while reading and checking the bulk data produced by the ATLAS-to-NASTRAN interface. The stress analysis results of the two ATLAS executions are equal within the accuracy of the data being converted. The NASTRAN stress analysis results agree with the ATLAS results as closely as expected considering the somewhat different behavior of the NASTRAN and ATLAS plate elements.

302.3 LISTING OF CONTROL PROGRAM AND DATA

BEGIN CONTROL MATRIX PROGRAM DEMO09
PROBLEM ICICEM009 - PART 1. ATLAS-TO-NASTRAN DATA CONVERSION

C
C PURPOSE THE PRINCIPAL CAPABILITIES DEMONSTRATED BY THIS
C DECK ARE
C 1. ATLAS-TO-NASTRAN DATA CONVERSION
C 2. NASTRAN-TO-ATLAS DATA CONVERSION

C AUTHOR M. TANAKUNI

C CORE 140K (OCTAL)

```

DIMENSION FET(100,5)
DIMENSION A1(200),A3(200),A4(200),A5(200),A6(200)
INTEGER D31,STAGE,SET
READ INPUT
PRINT INPUT(NODAL,SET=3)
PRINT INPUT(STIFFNESS,SET=3)
PRINT INPUT(BC,SET=3)
PERFORM STRESS (SET=3)
PRINT OUTPUT (DISPLACE,SET=3)
PRINT OUTPUT (STRESSES,SET=3)
PRINT OUTPUT (REACTIONS,SET=3)

```

```
C CALL FILEADD(FET,CATARNF,MERGRNF,MASSRNF,STIFRNF,SCOOARNF)
CALL FETADD (SAVESS1,A1,200,1.0,IRR)
CALL FETADD (SC00SSF,A3,200,1.0,IRR)
CALL FETADD (SC01SSF,A4,200,1.0,IRR)
CALL FETADD (SC02SSF,A5,200,1.0,IRR)
CALL FETADD (SC03SSF,A6,200,1.0,IRR)
```

```

C
      LOUT1 = SAVESS1
      L11 = 3LL11
      L21 = 3LL21
      L31 = 3LL31
      D31 = 3LD31
      STAGE = 1
      SET = 3
      NCOND = 0
      NELEM = 1
      NNODE = 1
      NBCLD = 1
      NMASS = 0

```

```

CALL ATNAISET,NCOND,NELEM,NNCDE,NMASS,LOUT,STAGE,L11,L21,L31,D31
X,NBCLD)
END CONTROL PROGRAM

```

```

*/ MODE2 /
BEGIN NODAL DATA
SET 3
1 0. 0. 0. TO 21 20. 0. 0. BY 10
2 0. 10. 0. TO 22 20. 10. 0. BY 10
3 0. 10. 10. TO 23 20. 10. 10. BY 10
4 0. 0. 10. TO 24 20. 0. 10. BY 10
END NODAL DATA
BEGIN STIFFNESS DATA
SET 3
BEGIN ELEMENT DATA
ROD 1 11 3.
**3 0 1 1 0.
ROD 11 21 2.
**3 0 1 1 0.
BEAM N100 11 12 13 1. .2 .3 .4 .5 .6
* N101 12 13 14 **
* N102 13 14 11 **
* N103 14 11 12 **
BEAM N104 1 11 22 **
* N105 2 12 1 **
* N106 3 13 1 **
* N107 4 14 1 **
* N201 11 21 2 **
* N202 12 22 1 **
* N203 13 23 2 **
* N204 14 24 1 **
PLATE N110 1 11 12 2 .1
* N111 4 14 13 3 **
* N112 11 21 22 12 .15
* N113 14 24 23 13 .20
* N114 3 4 14 .05
SPLATE N120 1 11 14 4 .05
* N121 2 12 13 3 .05
* N122 11 21 24 14 .07
* N123 12 22 23 13 .07
GPLATE N130 21 22 23 24 .06 .08 30.
* M4 T150 N131 11 12 14 .07
* * N132 12 13 14 .07
END ELEMENT DATA
END STIFFNESS DATA
BEGIN BC DATA
SET 3 STAGE 1
SUPPORT ALL FOR 1 TO 4
END BC DATA
BEGIN LOADS DATA
SET 3 STAGE 1
BEGIN NODAL LOAD DATA
CASE C8
21 TO 24 FX 1000.
END NODAL LOAD DATA
END LOADS DATA
END PROBLEM DATA

```



```

BEGIN CONTROL MATRIX PROGRAM DEM009
PROBLEM 10(CEM009 - PART II . NASTRAN-TO-ATLAS DATA CONVERSION)
DIMENSION A1(1000),A2(1000),A3(1000)
CALL FETACC(SCO0SSF,A1,1000,1,0,IRR)
CALL FETACC(SCO1SSF,A2,1000,1,0,IRR)
CALL FETADD(SAVESS2,A3,1000,1,0,IRR)
LOUT2 = SAVESS2
CALL NASTATL (LOUT2)
END CONTROL PROGRAM

```

```

BEGIN CONTROL PROGRAM DEM009
PROBLEM 10(CEM009 - PART III. ATLAS STRESS ANALYSIS)
READ INPUT
PRINT INPUT(NODAL)
PRINT INPUT(STIFFNESS)
PRINT INPUT(BC)
PERFORM STRESS (SET=1)
PRINT OUTPUT (DISPLACE,SET=1)
PRINT OUTPUT (STRESSES,SET=1)
PRINT OUTPUT (REACTIONS,SET=1)
END CONTROL PROGRAM

```

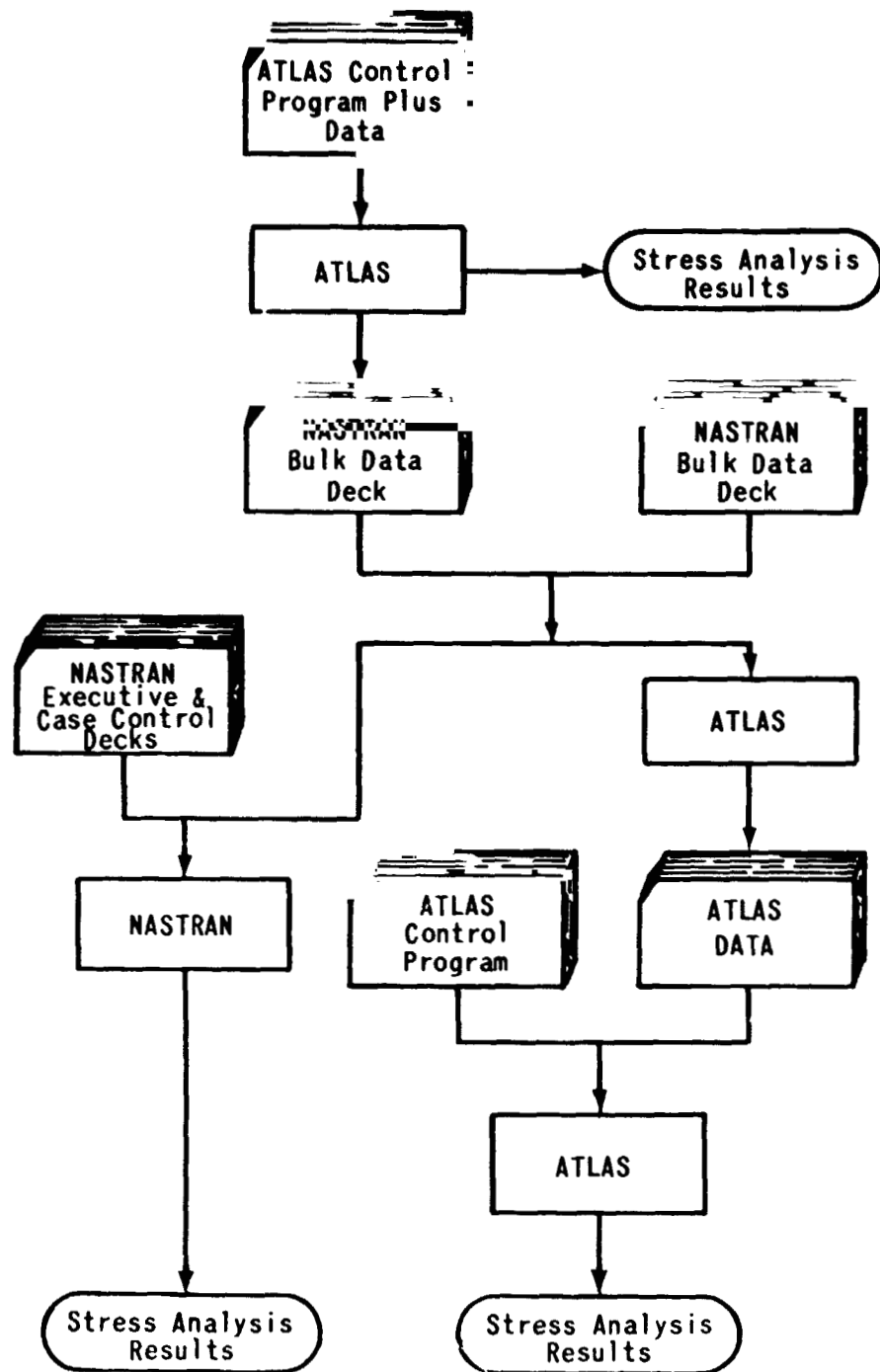


Figure 302-1. Schematic of ATLAS/NASTRAN Interface Demonstration

303. ATLAS/NASA-LaRC AIRPLANE CONFIGURATION PROGRAM INTERFACE (DECK 7)

303.1 DESCRIPTION OF DEMONSTRATION

This deck demonstrates the data interface between ATLAS and the NASA-LaRC airplane configuration plot program (ref. 303-1) and the NASA Aerodynamic Design and Analysis System for Supersonic Aircraft (ref. 303-2). The demonstration makes use of two airplane configurations documented in reference 303-1, viz.,

- A cambered circular body SST configuration (fig. 303-1)
- A blended wing-body fighter aircraft (fig. 303-3)

These examples illustrate each type of airplane component that can be defined by the LaRC configuration program.

The demonstration proceeds as shown schematically in figure 303-5. The LaRC configuration program data for the SST aircraft are processed by the ATLAS library subroutine LRCGEOM to produce geometry data in the format expected by the Geometry Preprocessor. Since the SST is symmetrical about the X-Z plane, each LaRC configuration component produces two ATLAS geometry components (right and left sides). The generated data are read by the Geometry Preprocessor and stored on DATARNF. ATLAS nodal data defining the model are read by the Nodal Preprocessor which interrogates the geometry data to obtain nodal coordinates. Surface nodes are defined for the body and pod components, and mid-surface nodes are defined for the wing, fin and canard components. The same process is then repeated for the fighter aircraft.

303.2 RESULTS

Nodal coordinates for both aircraft were printed by the Nodal Postprocessor and compared with the original airplane configuration data to confirm the correct operation of the interface. The ATLAS nodal data for the SST aircraft were plotted and are displayed in figure 303-2. The ATLAS nodal data for the fighter aircraft are displayed in figure 303-4.

303.3 LISTING OF CONTROL PROGRAM AND DATA

```
C
C BEGIN CONTROL MATRIX PROGRAM DEMO07
C PROBLEM ID(=DEMO07 - NASA/LARC CONFIGURATION PROGRAM INTERFACE)
C
C PURPOSE      THE PRINCIPAL CAPABILITIES DEMONSTRATED BY THIS
C               DECK ARE
C               1. NASA/LARC CONFIGURATION PROGRAM-TO-ATLAS
C                 INTERFACE
C               2. GEOMETRY PREPROCESSOR
C
C AUTHOR       R. L. DREISBACH
C
C CURE         ZOCC (OCTAL)
C
C DIMENSION A1(100)
C
C CALL FILEADD(A1,SAVESS1)
C
C S S T   C O N F I G U R A T I O N
C
C CALL LRCGEOM(SLINPUT,SAVESS1)
C REWIND SAVESS1
C READ INPUT(I=SAVESS1)
C PRINT INPUT
C PRINT INPUT(NODAL,SET=5)
C EXECUTE EXTRACT(EXNAME=SET5,LSUB=NODES,KSET=5,NSUB=N5)
C EXECUTE GRAPHICS(GNAME=NODEPLOT,TYPE=(ORTH,POINT),OFFLINE=CALCOMP,
X  RZ=60,RX=45,PX=0,SIZE=(30,20),EXNAME=SET5)
C PURGE FILES(DATARNF)
C
C F I G H T E R   C O N F I G U R A T I O N
C
C CALL FILEADD(A1,SAVESS1)
C REWIND SAVESS1
C CALL LRCGEOM(SLINPUT,SAVESS1)
C REWIND SAVESS1
C READ INPUT(I=SAVESS1)
C PRINT INPUT
C PRINT INPUT(NODAL,SET=10)
C EXECUTE EXTRACT(EXNAME=SET10,LSUB=NODES,KSET=10,NSUB=N10)
C EXECUTE GRAPHICS(GNAME=NODEPLOT,TYPE=(ORTH,POINT),SIZE=(30,20),
X  RZ=-150,RY=35,PX=0,EXNAME=SET10)
C END CONTROL PROGRAM
```

SST CONFIGURATION WITH CAMBERED CIRCULAR BODY

1	1	-1	1	1	2	0	12	13	1	17	26	2	10	3	10	
9494.																RFFA
0.	.1	.6	10.	20.	30.	40.	50.	60.	70.			XAF	10			XAF 10
80.	90.	100.										XAF	13			XAF 13
82.30	5.05	0.	180.10									WAFORG	1			WAFORG 1
93.80	6.60	0.	166.201									WAFORG	2			WAFORG 2
114.199	9.90	-45	142.351									WAFORG	3			WAFORG 3
130.629	13.20	-1.40	124.670									WAFORG	4			WAFORG 4
157.98	19.80	-1.85	56.570									WAFORG	5			WAFORG 5
181.29	26.40	-1.15	78.510									WAFORG	6			WAFORG 6
202.41	33.00	-35	61.241									WAFORG	7			WAFORG 7
221.63	39.60	-1.60	47.319									WAFORG	8			WAFORG 8
239.18	46.20	-2.80	36.719									WAFORG	9			WAFORG 9
255.00	52.80	-3.75	25.35									WAFORG	10			WAFORG 10
269.23	59.40	-4.30	15.670									WAFORG	11			WAFORG 11
282.00	66.00	-4.40	7.400									WAFORG	12			WAFORG 12
3.60	3.70	3.90	3.75	2.75	.95	-1.35	-3.45	-5.30	-6.80			TZORD	1			TZORD 1
-8.20	-9.10	-9.40										TZORD	1			TZORD 1
.10	.50	1.75	2.00	2.10	1.20	-1.05	-1.85	-3.25	-4.70			TZORD	2			TZORD 2
-6.30	-7.70	-8.80										TZORD	2			TZORD 2
0.	.35	.90	1.20	1.35	.70	-1.20	-1.20	-2.35	-3.45			TZORD	3			TZORD 3
-4.55	-5.75	-6.80										TZORD	3			TZORD 3
0.	.165	.72	.93	1.0	.6875	.15	-.56	-1.35	-2.205			TZORD	4			TZORD 4
-3.07	-3.9375	-4.801										TZORD	4			TZORD 4
0.	.10	.45	.60	.72	.695	.40	.0875	-.295	-.7825			TZORD	5			TZORD 5
-1.15	-1.685	-2.173										TZORD	5			TZORD 5
0.	.05	.285	.42	.5925	.625	.47	.0125	.12	-.10			TZORD	6			TZORD 6
-.345	-.6175	-.8589										TZORD	6			TZORD 6
0.	.04	.1935	.2765	.3950	.4395	.4330	.3860	.3085	.2075			TZORD	7			TZORD 7
.0915	-.0390	-.1820										TZORD	7			TZORD 7
0.	.0225	.1085	.160	.249	.2980	.3135	.3040	.2780	.2380			TZORD	8			TZORD 8
.185	.1235	.0563										TZORD	8			TZORD 8
0.	.02	.1055	.1500	.248	.2858	.305	.311	.308	.2995			TZORD	9			TZORD 9
.2845	.2635	.2385										TZORD	9			TZORD 9
0.	.0085	.049	.0695	.1175	.144	.155	.158	.1595	.1585			TZORD	10			TZORD 10
.1545	.148	.1398										TZORD	10			TZORD 10
0.	-.003	-.014	-.023	-.043	-.061	-.077	-.090	-.1005	-.110			TZORD	11			TZORD 11
-.1155	-.1190	-.1224										TZORD	11			TZORD 11
0.	-.0025	-.010	-.017	-.0325	-.047	-.062	-.075	-.088	-.100			TZORD	12			TZORD 12
-.1115	-.1220	-.1324										TZORD	12			TZORD 12
0.	.304	.491	.803	1.069	1.280	1.430	1.518	1.550	1.451			WAFORD	1			WAFORD 1
1.162	.678	0.0										WAFORD	1			WAFORD 1
0.0	.265	.423	.710	.962	1.156	1.296	1.373	1.396	1.294			WAFORD	2			WAFORD 2
1.028	.593	0.0										WAFORD	2			WAFORD 2
0.0	.226	.338	.635	.889	1.079	1.204	1.272	1.263	1.136			WAFORD	3			WAFORD 3
.886	.506	0.0										WAFORD	3			WAFORD 3
0.	.204	.274	.596	.870	1.074	1.20	1.250	1.234	1.083			WAFORD	4			WAFORD 4
.832	.472	0.										WAFORD	4			WAFORD 4
0.	.144	.175	.559	.886	1.111	1.246	1.294	1.242	1.087			WAFORD	5			WAFORD 5
.828	.466	0.0										WAFORD	5			WAFORD 5
0.0	.066	.09	.522	.886	1.145	1.289	1.341	1.285	1.125			WAFORD	6			WAFORD 6
.852	.48	0.										WAFORD	6			WAFORD 6
0.0	.006	.033	.495	.880	1.155	1.320	1.357	1.320	1.155			WAFORD	7			WAFORD 7
.880	.495	0.0										WAFORD	7			WAFORD 7
0.	.006	.033	.495	.880	1.155	1.320	1.357	1.320	1.155			WAFORD	8			WAFORD 8
.880	.495	0.0										WAFORD	8			WAFORD 8
0.0	.006	.033	.495	.880	1.155	1.320	1.357	1.320	1.155			WAFORD	9			WAFORD 9
.880	.495	0.										WAFORD	9			WAFORD 9
0.0	.006	.033	.495	.880	1.155	1.320	1.357	1.320	1.155			WAFORD	10			WAFORD 10
.880	.495	0.										WAFORD	10			WAFORD 10
0.0	.006	.033	.495	.880	1.155	1.320	1.357	1.320	1.155			WAFORD	11			WAFORD 11
.880	.495	0.										WAFORD	11			WAFORD 11
0.0	.006	.033	.495	.880	1.155	1.320	1.357	1.320	1.155			WAFORD	12			WAFORD 12
.880	.495	0.										WAFORD	12			WAFORD 12
0.	20.	40.	50.	60.	70.	80.	90.	100.	120.			XFUS	10			XFUS 10
130.	140.	150.	160.	180.	200.	220.	230.	240.	250.			XFUS	20			XFUS 20
260.	270.	280.	290.	300.	312.							XFUS	26			XFUS 26
7.4	7.4	7.4	7.4	7.4	7.4	7.	6.15	5.	2.5			ZFUS	10			ZFUS 10
1.25	0.	-1.3	-2.5	-5.	-7.45	-9.2	-9.75	-10.	-10.15			ZFUS	20			ZFUS 20
-10.2	-10.2	-10.2	-10.2	-10.2	-10.2							ZFUS	26			ZFUS 26

0.	18.5	48.	65.	83.	96.	95.5	92.2	95.5	96.	AFUS	10
98.	100.7	101.	98.	89.5	79.	70.	68.5	68.5	67.3	AFUS	20
62.	50.5	37.	24.	11.5	0.					AFUS	26
236.8	7.50	-11.55								PDDORG	1
0.	4.	8.	12.	16.	20.	24.	28.	32.	34.5	XPOD	1
2.292	2.477	2.644	2.791	2.915	3.012	3.076	3.097	3.100	3.100	PDDR	1
241.0	31.75	-3.60								PDDORG	2
0.	4.	8.	12.	16.	20.	24.	28.	32.	34.5	XPOD	2
2.292	2.477	2.644	2.791	2.915	3.012	3.076	3.097	3.100	3.100	PDDR	2
252.0	47.0	-2.95	35.3	285.36	47.0	6.31	4.77			FINORG	1
0.0	10.0	20.0	30.	40.	50.	60.	70.	90.	100.	XFIN	1
0.0	0.311	0.564	0.759	0.897	0.977	0.999	0.927	0.427	0.0	FINORD	1
277.9	0.	-6.77	35.3	311.3	0.	2.49	4.77			FINORG	2
0.0	10.	20.	30.	40.	50.	60.	70.	90.	100.	XFIN	2
0.	0.311	0.564	0.759	0.897	0.977	0.999	0.927	0.427	0.0	FINORD	2
312.	0.	-10.7	0.	277.9	0.	-6.77	35.3			FINORG	3
0.	10.	20.	30.	40.	50.	60.	70.	90.	100.	XFIN	3
0.	0.311	0.564	0.759	0.897	0.977	0.999	0.927	0.427	0.0	FINORD	3

*/ DEFINE NODES FOR SST CONFIGURATION -- EXAMPLE 1. /

BEGIN NODAL DATA /

SET 5 /

*/ DEFINE A LOCAL INPUT FRAME FOR EACH GEOMETRY COMPONENT. /

```

REC WINGR 0. 0. 0. 1. 0. 0. 0. 0. 1. /
REC WINGL 0. 0. 0. 1. 0. 0. 0. 0. 1. /
REC BODYA 0. 0. 0. 0. -1. 0. 0. 0. 1. /
REC PODAR 0. 0. 0. 0. -1. 0. 0. 0. 1. /
REC PODAL 0. 0. 0. 0. -1. 0. 0. 0. 1. /
REC PODRR 0. 0. 0. 0. -1. 0. 0. 0. 1. /
REC PODRL 0. 0. 0. 0. -1. 0. 0. 0. 1. /
REC FINAR 0. 0. 0. 1. 0. 0. 0. -1. 0. /
REC FINAL 0. 0. 0. 1. 0. 0. 0. -1. 0. /
REC FINB 0. 0. 0. 1. 0. 0. 0. -1. 0. /
REC FINC 0. 0. 0. 1. 0. 0. 0. -1. 0. /

```

BEGIN EXTRACT /

*/ DEFINE MID-SURFACE NODES FOR WING COMPONENTS -- 13 NODES PER SECTION AS DEFINED BY THE GEOMETRY DATA. THE NODES ARE LOCATED SUCH THAT THEY COINCIDE WITH THE LONGITUDINAL CONTROL CURVES DEFINED BY THE ENRICH DATA RECORD IN THE GEOMETRY DATA SET. /

COMPONENT WINGR /

MIDSURFACE NODES IN SECTION 70. 5.05 -10. 290. 5.05 -10. 70. 5.05 70. /
1 TO 13 OF .001 .005 .094 .1 * = 8 /

MIDSURFACE NODES IN SECTION 70. 6.60 -10. 290. 6.60 -10. 70. 6.60 70. /
14 TO 26 OF .001 .005 .094 .1 * = 8 /

MIDSURFACE NODES IN SECTION 70. 9.90 -10. 290. 9.90 -10. 70. 9.90 70. /
27 TO 39 OF .001 .005 .094 .1 * = 8 /

MIDSURFACE NODES IN SECTION 70. 13.2 -10. 290. 13.2 -10. 70. 13.2 70. /
40 TO 52 OF .001 .005 .094 .1 * = 8 /

MIDSURFACE NODES IN SECTION 70. 19.8 -10. 290. 19.8 -10. 70. 19.8 70. /
53 TO 65 OF .001 .005 .094 .1 * = 8 /

MIDSURFACE NODES IN SECTION 70. 26.4 -10. 290. 26.4 -10. 70. 26.4 70. /
66 TO 78 OF .001 .005 .094 .1 * = 8 /

MIDSURFACE NODES IN SECTION 70. 33.0 -10. 290. 33.0 -10. 70. 33.0 70. /
79 TO 91 OF .001 .005 .094 .1 * = 8 /

MIDSURFACE NODES IN SECTION 70. 39.6 -10. 290. 39.6 -10. 70. 39.6 70. /
92 TO 104 OF .001 .005 .094 .1 * = 8 /

MIDSURFACE NODES IN SECTION 70. 46.2 -10. 290. 46.2 -10. 70. 46.2 70. /
105 TO 117 OF .001 .005 .094 .1 * = 8 /

MIDSURFACE NODES IN SECTION 70. 52.8 -10. 290. 52.8 -10. 70. 52.8 70. /
118 TO 130 OF .001 .005 .094 .1 * = 8 /

MIDSURFACE NODES IN SECTION 70. 59.4 -10. 290. 59.4 -10. 70. 59.4 70. /
131 TO 143 OF .001 .005 .094 .1 * = 8 /

MIDSURFACE NODES IN SECTION 70. 66.0 -10. 290. 66.0 -10. 70. 66.0 70. /
144 TO 156 OF .001 .005 .094 .1 * = 8 /

*/ COMPONENT WINGL /

MIDSURFACE NODES IN SECTION 70. -5.05 -10. 290. -5.05 -10. 70. -5.05 70. /
201 TO 213 OF .001 .005 .094 .1 * = 8 /

MIDSURFACE NODES IN SECTION 70. -6.60 -10. 290. -6.60 -10. 70. -6.60 70. /
214 TO 226 OF .001 .005 .094 .1 * = 8 /

MIDSURFACE NODES IN SECTION 70. -9.90 -10. 290. -9.90 -10. 70. -9.90 70. /
227 TO 239 OF .001 .005 .094 .1 * = 8 /

MIDSURFACE NODES IN SECTION 70. -13.2 -10. 290. -13.2 -10. 70. -13.2 70. /
240 TO 252 OF .001 .005 .094 .1 *=8 /
MIDSURFACE NODES IN SECTION 70. -19.8 -10. 290. -19.8 -10. 70. -19.8 70. /
253 TO 265 OF .001 .005 .094 .1 *=8 /
MIDSURFACE NODES IN SECTION 70. -26.4 -10. 290. -26.4 -10. 70. -26.4 70. /
266 TO 278 OF .001 .005 .094 .1 *=8 /
MIDSURFACE NODES IN SECTION 70. -33.0 -10. 290. -33.0 -10. 70. -33.0 70. /
279 TO 291 OF .001 .005 .094 .1 *=8 /
MIDSURFACE NODES IN SECTION 70. -39.6 -10. 290. -39.6 -10. 70. -39.6 70. /
292 TO 304 OF .001 .005 .094 .1 *=8 /
MIDSURFACE NODES IN SECTION 70. -46.2 -10. 290. -46.2 -10. 70. -46.2 70. /
305 TO 317 OF .001 .005 .094 .1 *=8 /
MIDSURFACE NODES IN SECTION 70. -52.8 -10. 290. -52.8 -10. 70. -52.8 70. /
318 TO 330 OF .001 .005 .094 .1 *=8 /
MIDSURFACE NODES IN SECTION 70. -59.4 -10. 290. -59.4 -10. 70. -59.4 70. /
331 TO 343 OF .001 .005 .094 .1 *=8 /
MIDSURFACE NODES IN SECTION 70. -66.0 -10. 290. -66.0 -10. 70. -66.0 70. /
344 TO 356 OF .001 .005 .094 .1 *=8 /

*/
*/ DEFINE 30 EQUALLY-SPACED NODES PER SECTION OF THE BODY. /

COMPONENT PODS A /

SURFACE NODES IN SECTION -6. 1. -20. 6. 1. -20. -6. 1. 15. /
1001 TO 1030 /
SURFACE NODES IN SECTION -6. 20. -20. 6. 20. -20. -6. 20. 15. /
1031 TO 1060 /
SURFACE NODES IN SECTION -6. 40. -20. 6. 40. -20. -6. 40. 15. /
1061 TO 1090 /
SURFACE NODES IN SECTION -6. 50. -20. 6. 50. -20. -6. 50. 15. /
1091 TO 1120 /
SURFACE NODES IN SECTION -6. 60. -20. 6. 60. -20. -6. 60. 15. /
1121 TO 1150 /
SURFACE NODES IN SECTION -6. 70. -20. 6. 70. -20. -6. 70. 15. /
1151 TO 1180 /
SURFACE NODES IN SECTION -6. 80. -20. 6. 80. -20. -6. 80. 15. /
1181 TO 1210 /
SURFACE NODES IN SECTION -6. 90. -20. 6. 90. -20. -6. 90. 15. /
1211 TO 1240 /
SURFACE NODES IN SECTION -6. 100. -20. 6. 100. -20. -6. 100. 15. /
1241 TO 1270 /
SURFACE NODES IN SECTION -6. 120. -20. 6. 120. -20. -6. 120. 15. /
1271 TO 1300 /
SURFACE NODES IN SECTION -6. 130. -20. 6. 130. -20. -6. 130. 15. /
1301 TO 1330 /
SURFACE NODES IN SECTION -6. 140. -20. 6. 140. -20. -6. 140. 15. /
1331 TO 1360 /
SURFACE NODES IN SECTION -6. 150. -20. 6. 150. -20. -6. 150. 15. /
1361 TO 1390 /
SURFACE NODES IN SECTION -6. 160. -20. 6. 160. -20. -6. 160. 15. /
1391 TO 1420 /
SURFACE NODES IN SECTION -6. 180. -20. 6. 180. -20. -6. 180. 15. /
1421 TO 1450 /
SURFACE NODES IN SECTION -6. 200. -20. 6. 200. -20. -6. 200. 15. /
1451 TO 1480 /
SURFACE NODES IN SECTION -6. 220. -20. 6. 220. -20. -6. 220. 15. /
1481 TO 1510 /
SURFACE NODES IN SECTION -6. 230. -20. 6. 230. -20. -6. 230. 15. /
1511 TO 1540 /
SURFACE NODES IN SECTION -6. 240. -20. 6. 240. -20. -6. 240. 15. /
1541 TO 1570 /
SURFACE NODES IN SECTION -6. 250. -20. 6. 250. -20. -6. 250. 15. /
1571 TO 1600 /
SURFACE NODES IN SECTION -6. 260. -20. 6. 260. -20. -6. 260. 15. /
1601 TO 1630 /
SURFACE NODES IN SECTION -6. 270. -20. 6. 270. -20. -6. 270. 15. /
1631 TO 1660 /
SURFACE NODES IN SECTION -6. 280. -20. 6. 280. -20. -6. 280. 15. /
1661 TO 1690 /
SURFACE NODES IN SECTION -6. 290. -20. 6. 290. -20. -6. 290. 15. /
1691 TO 1720 /
SURFACE NODES IN SECTION -6. 300. -20. 6. 300. -20. -6. 300. 15. /
1721 TO 1750 /

SURFACE NODES IN SECTION -6. 311. -20. 6. 311. -20. -6. 311. 15. /
1751 TO 1700 /

*/
*/

DEFINE 25 EQUALLY-SPACED NODES PER SECTION OF EACH NACELLE. /

COMPONENT PODAR /

SURFACE NODES IN SECTION -20. 236.8 -13. -4. 236.8 -13. -20. 236.8 -2. /

2001 TO 2025 /

SURFACE NODES IN SECTION -20. 240.8 -13. -4. 240.8 -13. -20. 240.8 -2. /

2026 TO 2050 /

SURFACE NODES IN SECTION -20. 244.8 -13. -4. 244.8 -13. -20. 244.8 -2. /

2051 TO 2075 /

SURFACE NODES IN SECTION -20. 248.8 -13. -4. 248.8 -13. -20. 248.8 -2. /

2076 TO 2100 /

SURFACE NODES IN SECTION -20. 252.8 -13. -4. 252.8 -13. -20. 252.8 -2. /

2101 TO 2125 /

SURFACE NODES IN SECTION -20. 256.8 -13. -4. 256.8 -13. -20. 256.8 -2. /

2126 TO 2150 /

SURFACE NODES IN SECTION -20. 260.8 -13. -4. 260.8 -13. -20. 260.8 -2. /

2151 TO 2175 /

SURFACE NODES IN SECTION -20. 264.8 -13. -4. 264.8 -13. -20. 264.8 -2. /

2176 TO 2200 /

SURFACE NODES IN SECTION -20. 268.8 -13. -4. 268.8 -13. -20. 268.8 -2. /

2201 TO 2225 /

SURFACE NODES IN SECTION -20. 271.3 -13. -4. 271.3 -13. -20. 271.3 -2. /

2226 TO 2250 /

COMPONENT PODAR /

SURFACE NODES IN SECTION 4. 236.8 -13. 20. 236.8 -13. 4. 236.8 -2. /

2251 TO 2275 /

SURFACE NODES IN SECTION 4. 240.8 -13. 20. 240.8 -13. 4. 240.8 -2. /

2276 TO 2300 /

SURFACE NODES IN SECTION 4. 244.8 -13. 20. 244.8 -13. 4. 244.8 -2. /

2301 TO 2325 /

SURFACE NODES IN SECTION 4. 248.8 -13. 20. 248.8 -13. 4. 248.8 -2. /

2326 TO 2350 /

SURFACE NODES IN SECTION 4. 252.8 -13. 20. 252.8 -13. 4. 252.8 -2. /

2351 TO 2375 /

SURFACE NODES IN SECTION 4. 256.8 -13. 20. 256.8 -13. 4. 256.8 -2. /

2376 TO 2400 /

SURFACE NODES IN SECTION 4. 260.8 -13. 20. 260.8 -13. 4. 260.8 -2. /

2401 TO 2425 /

SURFACE NODES IN SECTION 4. 264.8 -13. 20. 264.8 -13. 4. 264.8 -2. /

2426 TO 2450 /

SURFACE NODES IN SECTION 4. 268.8 -13. 20. 268.8 -13. 4. 268.8 -2. /

2451 TO 2475 /

SURFACE NODES IN SECTION 4. 271.3 -13. 20. 271.3 -13. 4. 271.3 -2. /

2476 TO 2500 /

COMPONENT PODAR /

SURFACE NODES IN SECTION -8.0 241.0 -36.0 0. 241.0 -36.0 -8. 241.0 -28. /

2501 TO 2525 /

SURFACE NODES IN SECTION -8.0 245.0 -36.0 0. 245.0 -36.0 -8. 245.0 -28. /

2526 TO 2550 /

SURFACE NODES IN SECTION -8.0 249.0 -36.0 0. 249.0 -36.0 -8. 249.0 -28. /

2551 TO 2575 /

SURFACE NODES IN SECTION -8.0 253.0 -36.0 0. 253.0 -36.0 -8. 253.0 -28. /

2576 TO 2600 /

SURFACE NODES IN SECTION -8.0 257.0 -36.0 0. 257.0 -36.0 -8. 257.0 -28. /

2601 TO 2625 /

SURFACE NODES IN SECTION -8.0 261.0 -36.0 0. 261.0 -36.0 -8. 261.0 -28. /

2626 TO 2650 /

SURFACE NODES IN SECTION -8.0 265.0 -36.0 0. 265.0 -36.0 -8. 265.0 -28. /

2651 TO 2675 /

SURFACE NODES IN SECTION -8.0 269.0 -36.0 0. 269.0 -36.0 -8. 269.0 -28. /

2676 TO 2700 /

SURFACE NODES IN SECTION -8.0 273.0 -36.0 0. 273.0 -36.0 -8. 273.0 -28. /

2701 TO 2725 /

SURFACE NODES IN SECTION -8.0 275.5 -36.0 0. 275.5 -36.0 -8. 275.5 -28. /

2726 TO 2750 /


```

COMPONENT PODDL /
  SURFACE NODES IN SECTION 0. 241.0 -36.0 8.0 241.0 -36.0 0. 241.0 -28. /
  2751 TO 2775 /
  SURFACE NODES IN SECTION 0. 245.0 -36.0 8.0 245.0 -36.0 0. 245.0 -28. /
  2776 TO 2800 /
  SURFACE NODES IN SECTION 0. 249.0 -36.0 8.0 249.0 -36.0 0. 249.0 -28. /
  2801 TO 2825 /
  SURFACE NODES IN SECTION 0. 253.0 -36.0 8.0 253.0 -36.0 0. 253.0 -28. /
  2826 TO 2850 /
  SURFACE NODES IN SECTION 0. 257.0 -36.0 8.0 257.0 -36.0 0. 257.0 -28. /
  2851 TO 2875 /
  SURFACE NODES IN SECTION 0. 261.0 -36.0 8.0 261.0 -36.0 0. 261.0 -28. /
  2876 TO 2900 /
  SURFACE NODES IN SECTION 0. 265.0 -36.0 8.0 265.0 -36.0 0. 265.0 -28. /
  2901 TO 2925 /
  SURFACE NODES IN SECTION 0. 269.0 -36.0 8.0 269.0 -36.0 0. 269.0 -28. /
  2926 TO 2950 /
  SURFACE NODES IN SECTION 0. 273.0 -36.0 8.0 273.0 -36.0 0. 273.0 -28. /
  2951 TO 2975 /
  SURFACE NODES IN SECTION 0. 275.5 -36.0 8.0 275.5 -36.0 0. 275.5 -28. /
  2976 TO 3000 /
*/ DEFINE MID-SURFACE NODES FOR FIN COMPONENTS -- 10 NODES PER SECTION AS
   DEFINED BY THE GEOMETRY DATA. THE NODES ARE LOCATED SUCH THAT THEY
   COINCIDE WITH THE LONGITUDINAL CONTROL CURVES DEFINED BY THE ENRICH DATA
   RECORD IN THE GEOMETRY DATA SET. /
*/
COMPONENT FINAK /
  MIDSURFACE NODES IN SECTION 250. -2.95 -48. 300. -2.95 -48. 250. -2.95 -45. /
  4001 TO 4010 OF .1 *#6 .2 .1 /
  MIDSURFACE NODES IN SECTION 250. .14 -48. 300. .14 -48. 250. .14 -45. /
  4011 TO 4020 OF .1 *#6 .2 .1 /
  MIDSURFACE NODES IN SECTION 250. 3.23 -48. 300. 3.23 -48. 250. 3.23 -45. /
  4021 TO 4030 OF .1 *#6 .2 .1 /
  MIDSURFACE NODES IN SECTION 250. 6.31 -48. 300. 6.31 -48. 250. 6.31 -45. /
  4031 TO 4040 OF .1 *#6 .2 .1 /
  COMPONENT FINAL /
  MIDSURFACE NODES IN SECTION 250. -2.95 45. 300. -2.95 45. 250. -2.95 48. /
  4041 TO 4050 OF .1 *#6 .2 .1 /
  MIDSURFACE NODES IN SECTION 250. .14 45. 300. .14 45. 250. .14 48. /
  4051 TO 4060 OF .1 *#6 .2 .1 /
  MIDSURFACE NODES IN SECTION 250. 3.23 45. 300. 3.23 45. 250. 3.23 48. /
  4061 TO 4070 OF .1 *#6 .2 .1 /
  MIDSURFACE NODES IN SECTION 250. 6.31 45. 300. 6.31 45. 250. 6.31 48. /
  4071 TO 4080 OF .1 *#6 .2 .1 /
*/
COMPONENT FINB /
  MIDSURFACE NODES IN SECTION 270. -6.77 -1. 318. -6.77 -1. 270. -6.77 1. /
  5001 TO 5010 OF .1 *#6 .2 .1 /
  MIDSURFACE NODES IN SECTION 270. -3.68 -1. 318. -3.68 -1. 270. -3.68 1. /
  5011 TO 5020 OF .1 *#6 .2 .1 /
  MIDSURFACE NODES IN SECTION 270. -.59 -1. 318. -.59 -1. 270. -.59 1. /
  5021 TO 5030 OF .1 *#6 .2 .1 /
  MIDSURFACE NODES IN SECTION 270. 2.49 -1. 318. 2.49 -1. 270. 2.49 1. /
  5031 TO 5040 OF .1 *#6 .2 .1 /
*/
COMPONENT FINC /
  MIDSURFACE NODES IN SECTION 270. -10.2 -1. 318. -10.2 -1. 270. -10.2 1. /
  5051 TO 5060 OF .1 *#6 .2 .1 /
  MIDSURFACE NODES IN SECTION 270. -9.06 -1. 318. -9.06 -1. 270. -9.06 1. /
  5061 TO 5070 OF .1 *#6 .2 .1 /
  MIDSURFACE NODES IN SECTION 270. -7.92 -1. 318. -7.92 -1. 270. -7.92 1. /
  5071 TO 5080 OF .1 *#6 .2 .1 /
  MIDSURFACE NODES IN SECTION 270. -6.77 -1. 318. -6.77 -1. 270. -6.77 1. /
  5081 TO 5090 OF .1 *#6 .2 .1 /
  END EXTRACT /
END NODAL DATA /
*/
*/ DEFINE NODE SUBSETS FOR PRINT AND PLOT DISPLAYS. /
BEGIN SUBSET DEFINITION /
  SUBSETS OF NODAL SET 5 /
  N5 = ALL /
END SUBSET DEFINITION /
END PROBLEM DATA /

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1	-1	1	1	1	11	13	1	19	15	5	10	2	10
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303.8

-2.0	-2.0	-2.0	-2.0	-1.95	-1.85	-1.5	-1.05	-0.5	0.	Y 8
.5	1.05	1.5	1.85	1.95	2.	2.	2.	2.	2.	Z 8
0.	.35	.725	1.15	1.65	2.15	3.0	3.0	3.0	3.0	Y 9
3.0	3.0	3.0	2.15	1.65	1.15	.725	.35	0.	0.	Y 9
-2.0	-2.0	-2.0	-2.0	-1.95	-1.8	-1.5	-1.05	-0.5	0.	Y 9
.5	1.05	1.5	1.8	1.95	2.	2.	2.	2.	2.	Z 9
0.	.35	.725	1.15	1.65	2.15	3.0	3.0	3.0	3.0	Y 10
3.0	3.0	3.0	2.15	1.65	1.15	.725	.35	0.	0.	Y 10
-2.0	-2.0	-2.0	-2.0	-1.95	-1.8	-1.5	-1.05	-0.5	0.	Y 10
.5	1.05	1.5	1.8	1.95	2.	2.	2.	2.	2.	Z 10
0.	.35	.725	1.15	1.65	2.15	3.0	3.0	3.0	3.0	Y 11
3.0	3.0	3.0	2.15	1.65	1.15	.725	.35	0.	0.	Y 11
-2.0	-2.0	-2.0	-2.0	-1.95	-1.8	-1.5	-1.05	-0.5	0.	Y 11
.5	1.05	1.5	1.8	1.95	2.	2.	2.	2.	2.	Z 11
0.	.35	.725	1.15	1.65	2.15	2.5	3.0	3.0	3.0	Y 12
3.0	3.0	2.5	2.15	1.65	1.15	.725	.35	0.	0.	Y 12
-2.0	-2.0	-2.0	-2.0	-1.95	-1.8	-1.4	-1.05	-0.5	0.	Y 12
.5	1.05	1.4	1.8	1.95	2.	2.	2.	2.	2.	Z 12
0.	.35	.725	1.15	1.65	2.15	2.5	2.875	2.95	3.0	Y 13
2.95	2.875	2.5	2.15	1.65	1.15	.725	.35	0.	0.	Y 13
-2.0	-2.0	-2.0	-2.0	-1.95	-1.8	-1.4	-.975	-0.5	0.	Y 13
.5	.975	1.4	1.8	1.95	2.	2.	2.	2.	2.	Z 13
0.	.35	.725	1.125	1.525	1.9	2.25	2.55	2.8	3.0	Y 14
2.8	2.55	2.25	1.9	1.525	1.125	.725	.35	0.	0.	Y 14
-2.0	-2.0	-2.0	-1.95	-1.8	-1.6	-1.275	-.9	-0.5	0.	Y 14
.5	.9	1.275	1.6	1.9	1.95	2.	2.	2.	2.	Z 14
0.	.35	.725	1.125	1.525	1.9	2.25	2.55	2.8	3.0	Y 15
2.8	2.55	2.25	1.9	1.525	1.125	.725	.35	0.	0.	Y 15
-2.0	-2.0	-2.0	-1.95	-1.8	-1.6	-1.275	-.9	-0.5	0.	Y 15
.5	.9	1.275	1.6	1.8	1.95	2.	2.	2.	2.	Z 15
53.091	0.	2.0	12.162	62.215	0.	8.483	6.129	0.	0.	VING 1
0.	10.	20.	30.	40.	50.	60.	70.	80.	100.	XFIN
0.	.72	1.28	1.68	1.92	2.0	1.92	1.68	1.28	0.	FINED
62.215	0.	8.483	6.129	64.662	0.	10.18	0.	0.	0.	VING 2
0.	10.	20.	30.	40.	50.	60.	70.	80.	100.	XFIN
0.	.72	1.28	1.68	1.92	2.0	1.92	1.68	1.28	0.	FINED
55.774	0.	-4.481	0.	55.026	0.	-3.948	1.495	0.	0.	VING 3
0.	13.727	20.	30.	40.	50.	60.	70.	86.278	100.	VERD
0.	1.49	1.49	1.49	1.49	1.49	1.49	1.49	1.49	0.	VERD
55.026	0.	-3.948	8.498	53.073	0.	-2.455	11.473	0.	0.	VING 4
0.	13.722	20.	30.	40.	50.	60.	70.	86.278	100.	VERD
0.	1.49	1.49	1.49	1.49	1.49	1.49	1.49	1.49	0.	VERD
53.073	0.	-2.455	11.473	52.481	0.	-2.0	12.066	0.	0.	VING 5
0.	13.722	20.	30.	40.	50.	60.	70.	86.278	100.	VERD
0.	1.49	1.49	1.49	1.49	1.49	1.49	1.49	1.49	0.	VERD
57.473	3.0	0.	8.987	66.868	11.315	0.	3.413	0.	0.	CANDG 1
0.	10.	20.	30.	40.	50.	60.	70.	80.	100.	XCAN
0.	.72	1.28	1.68	1.92	2.0	1.92	1.68	1.28	0.	CANDG 2
66.968	11.315	0.	3.413	63.115	12.419	0.	0.	0.	0.	XCAN
0.	10.	20.	30.	40.	50.	60.	70.	80.	100.	XCAN
0.	.72	1.28	1.68	1.92	2.0	1.92	1.68	1.28	0.	CANDG

*/ DEFINE NODES FOR BLENDED WING-BODY FIGHTER -- EXAMPLE 2. /

BEGIN NODAL DATA /

SET 10 /

*/ DEFINE A LOCAL INPUT FRAME FOR EACH GEOMETRY COMPONENT. /

REC WINGR	0.	0.	0.	1.	0.	0.	0.	0.	1.	/
REC WINGL	0.	0.	0.	1.	0.	0.	0.	0.	1.	/
REC BODYA	0.	0.	0.	1.	0.	0.	0.	0.	1.	/
REC FINA	0.	0.	0.	1.	0.	0.	0.	-1.	0.	/
REC FINB	0.	0.	0.	1.	0.	0.	0.	-1.	0.	/
REC FINL	0.	0.	0.	1.	0.	0.	0.	-1.	0.	/
REC FINR	0.	0.	0.	1.	0.	0.	0.	-1.	0.	/
REC CAN	0.	0.	0.	1.	0.	0.	0.	0.	1.	/
REC CANRDL	0.	0.	0.	1.	0.	0.	0.	0.	1.	/
REC CANRDR	0.	0.	0.	1.	0.	0.	0.	0.	1.	/
REC CANRDL	0.	0.	0.	1.	0.	0.	0.	0.	1.	/

```

BEGIN EXTRACT /
*/  DEFINE MID-SURFACE NODES FOR WING COMPONENTS -- 13 NODES PER SECTION AS
    DEFINED BY THE GEOMETRY DATA.  THE NODES ARE LOCATED SUCH THAT THEY
    COINCIDE WITH THE LONGITUDINAL CONTROL CURVES DEFINED BY THE ENRICH DATA
    RECORD IN THE GEOMETRY DATA SET. /
    COMPONENT WING /
MIDSURFACE NODES IN SECTION 13. 3.0 -1. 55. 3.0 -1. 13. 3.0 20. /
1 TO 13 OF .005 .095 .1 *7 .05 .05 /
MIDSURFACE NODES IN SECTION 13. 4.0 -1. 55. 4.0 -1. 13. 4.0 20. /
14 TO 26 OF .005 .095 .1 *7 .05 .05 /
MIDSURFACE NODES IN SECTION 13. 5.0 -1. 55. 5.0 -1. 13. 5.0 20. /
27 TO 39 OF .005 .095 .1 *7 .05 .05 /
MIDSURFACE NODES IN SECTION 13. 6.0 -1. 55. 6.0 -1. 13. 6.0 20. /
40 TO 52 OF .005 .095 .1 *7 .05 .05 /
MIDSURFACE NODES IN SECTION 13. 8.0 -1. 55. 8.0 -1. 13. 8.0 20. /
53 TO 65 OF .005 .095 .1 *7 .05 .05 /
MIDSURFACE NODES IN SECTION 13. 10.0 -1. 55. 10.0 -1. 13. 10.0 20. /
66 TO 78 OF .005 .095 .1 *7 .05 .05 /
MIDSURFACE NODES IN SECTION 13. 12.0 -1. 55. 12.0 -1. 13. 12.0 20. /
79 TO 91 OF .005 .095 .1 *7 .05 .05 /
MIDSURFACE NODES IN SECTION 13. 14.0 -1. 55. 14.0 -1. 13. 14.0 20. /
92 TO 104 OF .005 .095 .1 *7 .05 .05 /
MIDSURFACE NODES IN SECTION 13. 16.0 -1. 55. 16.0 -1. 13. 16.0 20. /
105 TO 117 OF .005 .095 .1 *7 .05 .05 /
MIDSURFACE NODES IN SECTION 13. 17.6 -1. 55. 17.6 -1. 13. 17.6 20. /
118 TO 130 OF .005 .095 .1 *7 .05 .05 /
MIDSURFACE NODES IN SECTION 13. 17.999 -1. 55. 17.999 -1. 13. 17.999 20. /
131 TO 143 OF .005 .095 .1 *7 .05 .05 /
*/
    COMPONENT WINGL /
MIDSURFACE NODES IN SECTION 13. -3.0 -1. 55. -3.0 -1. 13. -3.0 20. /
201 TO 213 OF .005 .095 .1 *7 .05 .05 /
MIDSURFACE NODES IN SECTION 13. -4.0 -1. 55. -4.0 -1. 13. -4.0 20. /
214 TO 226 OF .005 .095 .1 *7 .05 .05 /
MIDSURFACE NODES IN SECTION 13. -5.0 -1. 55. -5.0 -1. 13. -5.0 20. /
227 TO 239 OF .005 .095 .1 *7 .05 .05 /
MIDSURFACE NODES IN SECTION 13. -6.0 -1. 55. -6.0 -1. 13. -6.0 20. /
240 TO 252 OF .005 .095 .1 *7 .05 .05 /
MIDSURFACE NODES IN SECTION 13. -8.0 -1. 55. -8.0 -1. 13. -8.0 20. /
253 TO 265 OF .005 .095 .1 *7 .05 .05 /
MIDSURFACE NODES IN SECTION 13. -10.0 -1. 55. -10.0 -1. 13. -10.0 20. /
266 TO 278 OF .005 .095 .1 *7 .05 .05 /
MIDSURFACE NODES IN SECTION 13. -12.0 -1. 55. -12.0 -1. 13. -12.0 20. /
279 TO 291 OF .005 .095 .1 *7 .05 .05 /
MIDSURFACE NODES IN SECTION 13. -14.0 -1. 55. -14.0 -1. 13. -14.0 20. /
292 TO 304 OF .005 .095 .1 *7 .05 .05 /
MIDSURFACE NODES IN SECTION 13. -16.0 -1. 55. -16.0 -1. 13. -16.0 20. /
305 TO 317 OF .005 .095 .1 *7 .05 .05 /
MIDSURFACE NODES IN SECTION 13. -17.6 -1. 55. -17.6 -1. 13. -17.6 20. /
318 TO 330 OF .005 .095 .1 *7 .05 .05 /
MIDSURFACE NODES IN SECTION 13. -17.999 -1. 55. -17.999 -1. 13. -17.999 20. /
331 TO 343 OF .005 .095 .1 *7 .05 .05 /
*/
    COMPONENT BODY /
SURFACE NODES IN SECTION 2. -10. -10. 2. 10. -10. 2. -10. 10. /
1001 TO 1037 AT CURVES /
SURFACE NODES IN SECTION 4. -10. -10. 4. 10. -10. 4. -10. 10. /
1038 TO 1074 AT CURVES /
SURFACE NODES IN SECTION 6. -10. -10. 6. 10. -10. 6. -10. 10. /
1075 TO 1111 AT CURVES /
SURFACE NODES IN SECTION 12. -10. -10. 12. 10. -10. 12. -10. 10. /
1112 TO 1148 AT CURVES /
SURFACE NODES IN SECTION 16. -10. -10. 16. 10. -10. 16. -10. 10. /
1149 TO 1185 AT CURVES /
SURFACE NODES IN SECTION 20. -10. -10. 20. 10. -10. 20. -10. 10. /
1186 TO 1222 AT CURVES /
SURFACE NODES IN SECTION 24. -10. -10. 24. 10. -10. 24. -10. 10. /

```

1223 TO 1259 AT CURVES /
 SURFACE NODES IN SECTION 28. -10. -10. 28. 10. -10. 28. -10. 10. /
 1260 TO 1296 AT CURVES /
 SURFACE NODES IN SECTION 32. -10. -10. 32. 10. -10. 32. -10. 10. /
 1297 TO 1333 AT CURVES /
 SURFACE NODES IN SECTION 36. -10. -10. 36. 10. -10. 36. -10. 10. /
 1334 TO 1370 AT CURVES /
 SURFACE NODES IN SECTION 40. -10. -10. 40. 10. -10. 40. -10. 10. /
 1371 TO 1407 AT CURVES /
 SURFACE NODES IN SECTION 48. -10. -10. 48. 10. -10. 48. -10. 10. /
 1408 TO 1444 AT CURVES /
 SURFACE NODES IN SECTION 52. -10. -10. 52. 10. -10. 52. -10. 10. /
 1445 TO 1491 AT CURVES /
 SURFACE NODES IN SECTION 65. -10. -10. 65. 10. -10. 65. -10. 10. /
 1492 TO 1518 AT CURVES /

*/
 */ DEFINE MID-SURFACE NODES FOR FIN COMPONENTS -- 10 NODES PER SECTION.
 THE NODES ARE LOCATED SUCH THAT THEY COINCIDE WITH THE LONGITUDINAL
 CONTROL CURVES DEFINED BY THE ENRICH DATA RECORD IN THE GEOMETRY
 DATA SET. /

COMPONENT FINA /
 MIDSURFACE NODES IN SECTION 50. 2.0 5.0 70. 2.0 5.0 50. 2.0 -5.0 /
 4001 TO 4010 OF .1 * = 7 .2 /
 MIDSURFACE NODES IN SECTION 50. 4.0 5.0 70. 4.0 5.0 50. 4.0 -5.0 /
 4011 TO 4020 OF .1 * = 7 .2 /
 MIDSURFACE NODES IN SECTION 50. 6.0 5.0 70. 6.0 5.0 50. 6.0 -5.0 /
 4021 TO 4030 OF .1 * = 7 .2 /
 MIDSURFACE NODES IN SECTION 50. 8.483 5.0 70. 8.483 5.0 50. 8.483 -5.0 /
 4031 TO 4040 OF .1 * = 7 .2 /
 COMPONENT FINB /
 MIDSURFACE NODES IN SECTION 50. 8.483 5.0 70. 8.483 5.0 50. 8.483 -5.0 /
 4041 TO 4050 OF .1 * = 7 .2 /
 MIDSURFACE NODES IN SECTION 50. 10.18 5.0 70. 10.18 5.0 50. 10.18 -5.0 /
 4051 TO 4060 OF .1 * = 7 .2 /
 COMPONENT FINC /
 MIDSURFACE NODES IN SECTION 50. -4.481 5. 70. -4.481 5. 50. -4.481 -5. /
 4061 TO 4070 OF .1372 .0628 .1 * = 4 .1628 .1372 /
 MIDSURFACE NODES IN SECTION 50. -3.948 5. 70. -3.948 5. 50. -3.948 -5. /
 4071 TO 4080 OF .1372 .0628 .1 * = 4 .1628 .1372 /
 COMPONENT FINE /
 MIDSURFACE NODES IN SECTION 50. -2.455 5. 70. -2.455 5. 50. -2.455 -5. /
 4081 TO 4090 OF .1372 .0628 .1 * = 4 .1628 .1372 /
 COMPONENT FINF /
 MIDSURFACE NODES IN SECTION 50. -2.0 5. 70. -2.0 5. 50. -2.0 -5. /
 4091 TO 4100 OF .1372 .0628 .1 * = 4 .1628 .1372 /

*/
 */ DEFINE MID-SURFACE NODES FOR CANARD COMPONENTS -- 10 NODES PER SECTION.
 THE NODES ARE LOCATED SUCH THAT THEY COINCIDE WITH THE LONGITUDINAL
 CONTROL CURVES DEFINED BY THE ENRICH DATA RECORD IN THE GEOMETRY
 DATA SET. /

COMPONENT CANARD /
 MIDSURFACE NODES IN SECTION 50. 3.0 -1. 70. 3.0 -1. 50. 3.0 1. /
 5001 TO 5010 OF .1 * = 7 .2 /
 MIDSURFACE NODES IN SECTION 50. 6.0 -1. 70. 6.0 -1. 50. 6.0 1. /
 5011 TO 5020 OF .1 * = 7 .2 /
 MIDSURFACE NODES IN SECTION 50. 11.315 -1. 70. 11.315 -1. 50. 11.315 1. /
 5021 TO 5030 OF .1 * = 7 .2 /
 COMPONENT CANARDL /
 MIDSURFACE NODES IN SECTION 50. -3.0 -1. 70. -3.0 -1. 50. -3.0 1. /
 5041 TO 5050 OF .1 * = 7 .2 /
 MIDSURFACE NODES IN SECTION 50. -6.0 -1. 70. -6.0 -1. 50. -6.0 1. /
 5051 TO 5060 OF .1 * = 7 .2 /
 MIDSURFACE NODES IN SECTION 50. -11.315 -1. 70. -11.315 -1. 50. -11.315 1. /
 5061 TO 5070 OF .1 * = 7 .2 /
 COMPONENT CANARDR /
 MIDSURFACE NODES IN SECTION 50. 12.319 -1. 70. 12.319 -1. 50. 12.319 1. /
 5071 TO 5080 OF .1 * = 7 .2 /
 COMPONENT CANARDL /
 MIDSURFACE NODES IN SECTION 50. -12.319 -1. 70. -12.319 -1. 50. -12.319 1. /
 5081 TO 5090 OF .1 * = 7 .2 /
 END EXTRACT /

END NODAL DATA /
*/
*/ DEFINE NODE SUBSETS FOR PRINT AND PLOT DISPLAYS. /
BEGIN SUBSET DEFINITION /
SUBSETS OF NODAL SET 10 /
N10 = ALL /
END SUBSET DEFINITION /
END PROBLEM DATA /

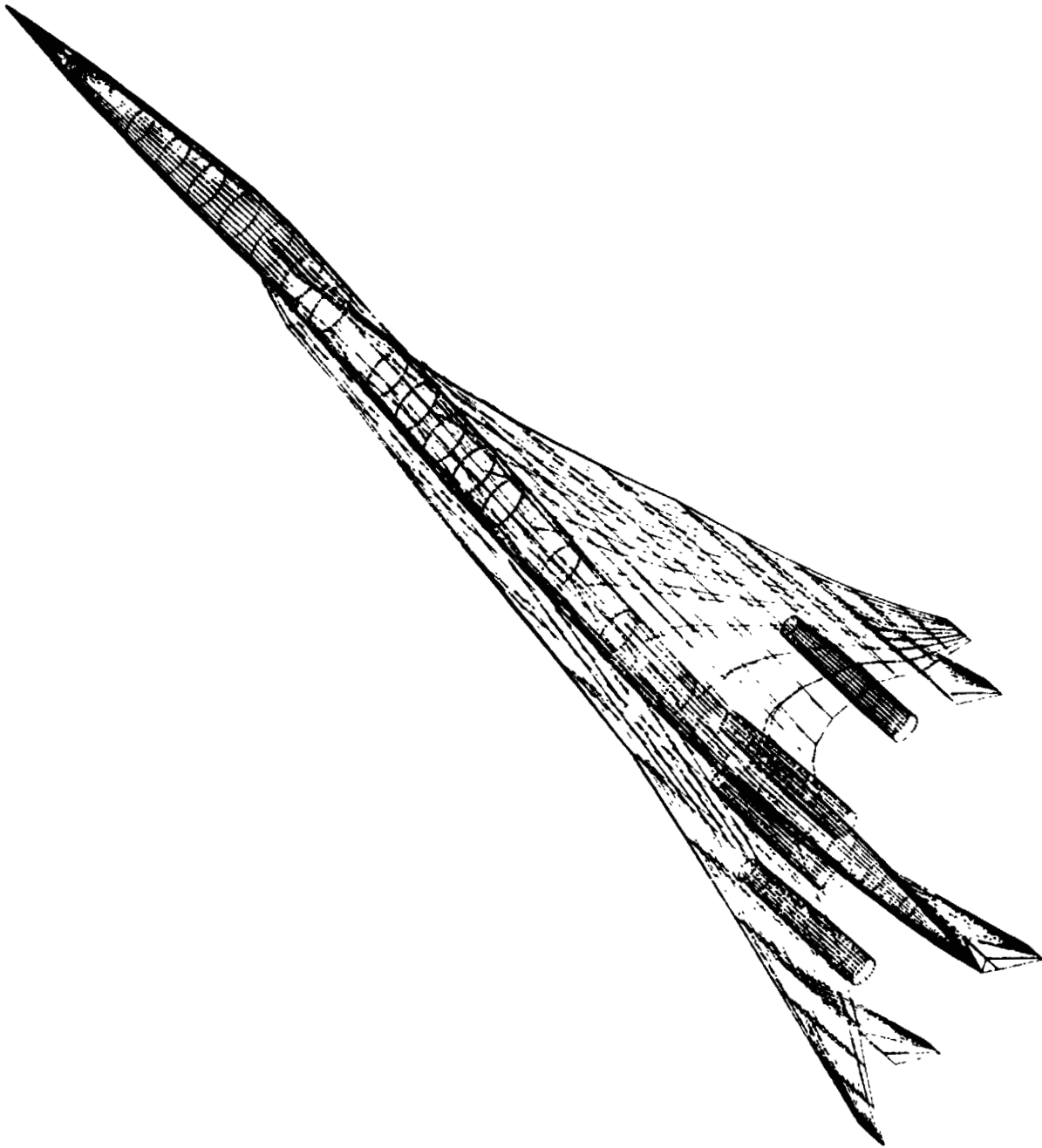


Figure 303-1. SST Configuration

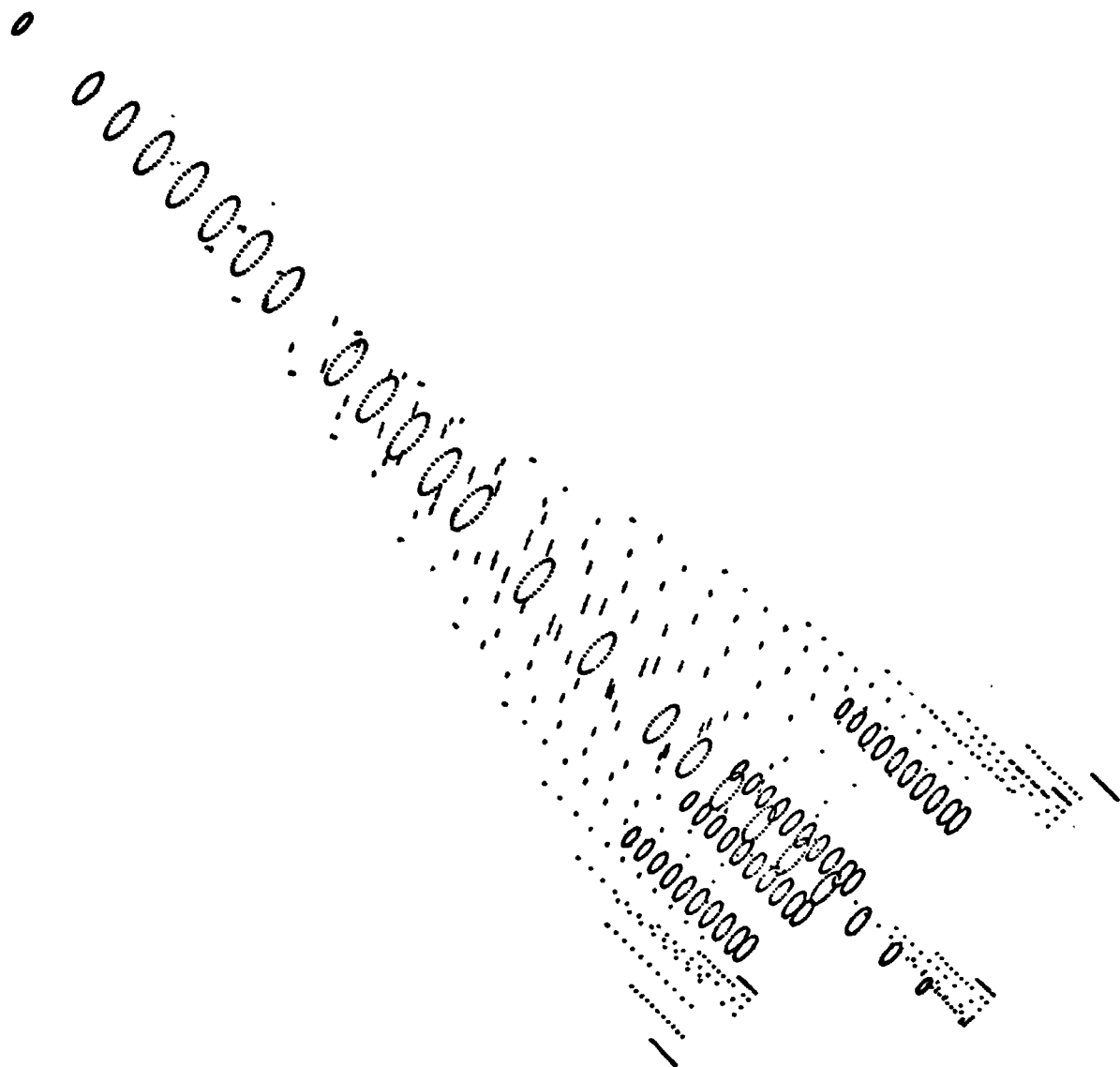


Figure 303-2. ATLAS Nodal Data for SST Aircraft

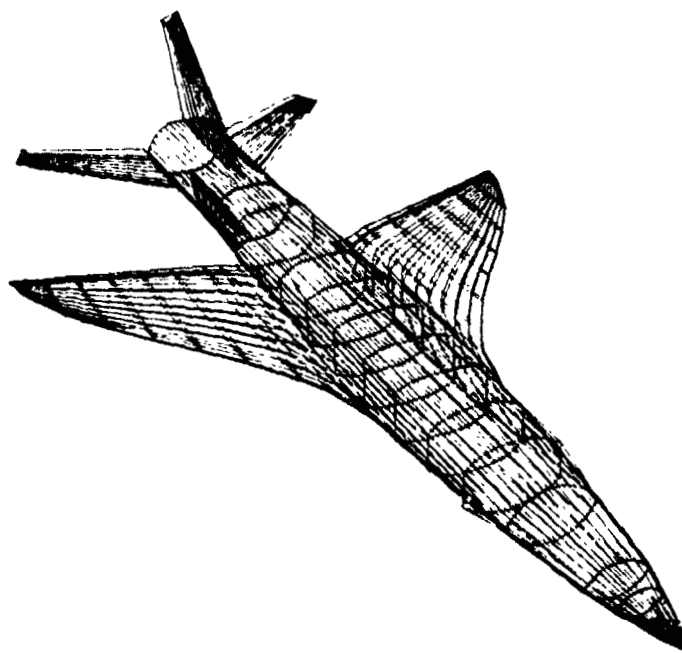
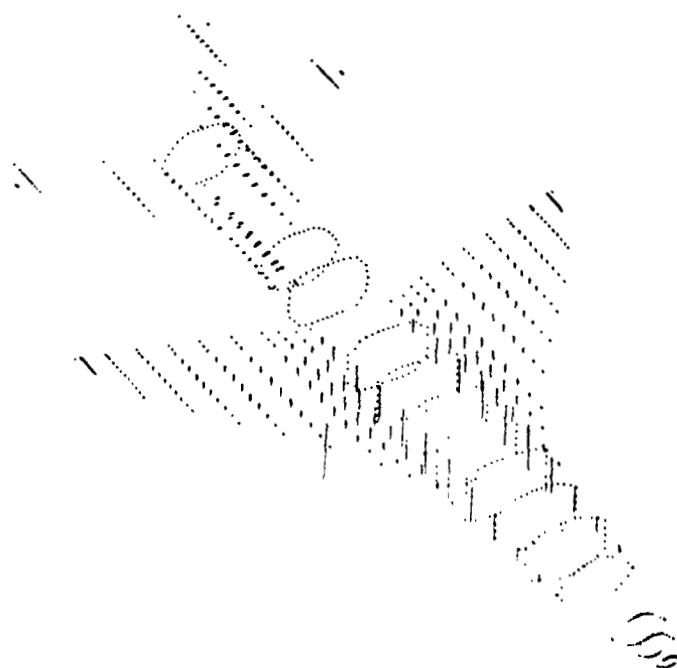


Figure 303-3. Fighter Aircraft Configuration



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OF POOR QUALITY

Figure 303-4. ATLAS Nodal Data for Fighter Aircraft

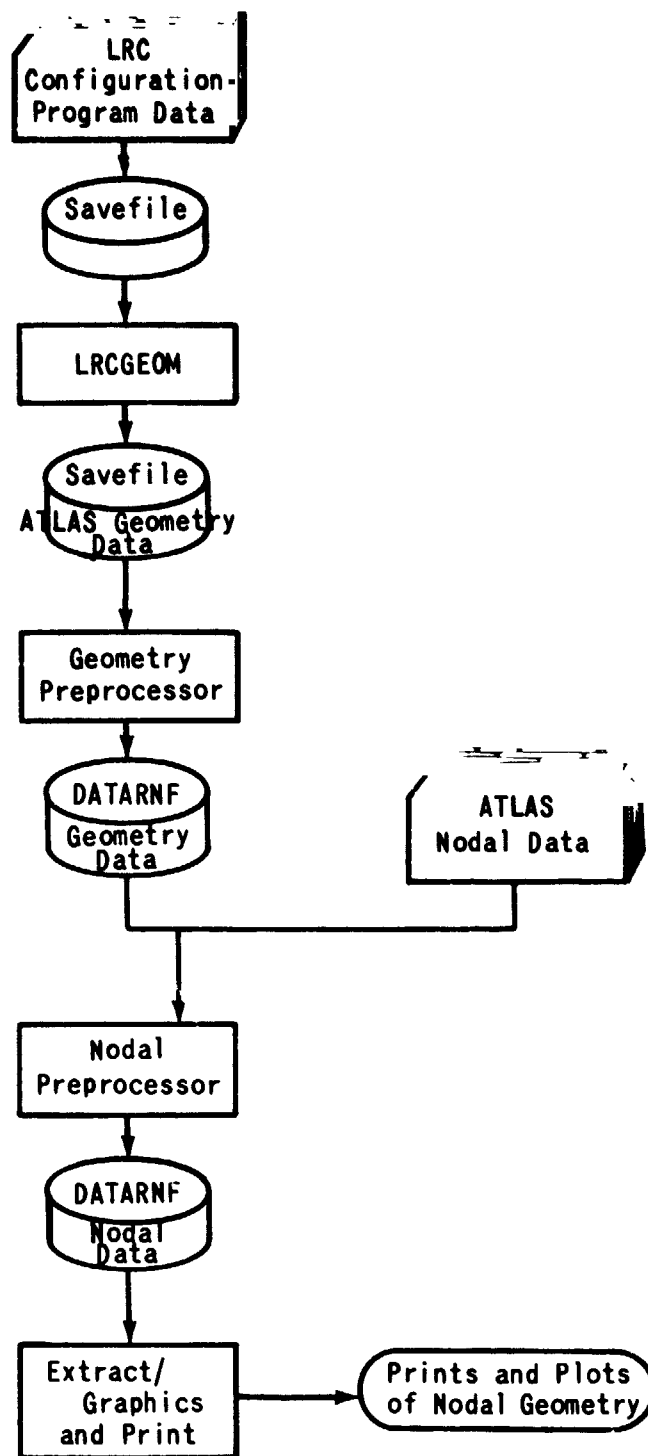


Figure 303-5. Schematic of ATLAS/ LaRC Airplane Configuration Program Interface Demonstration

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